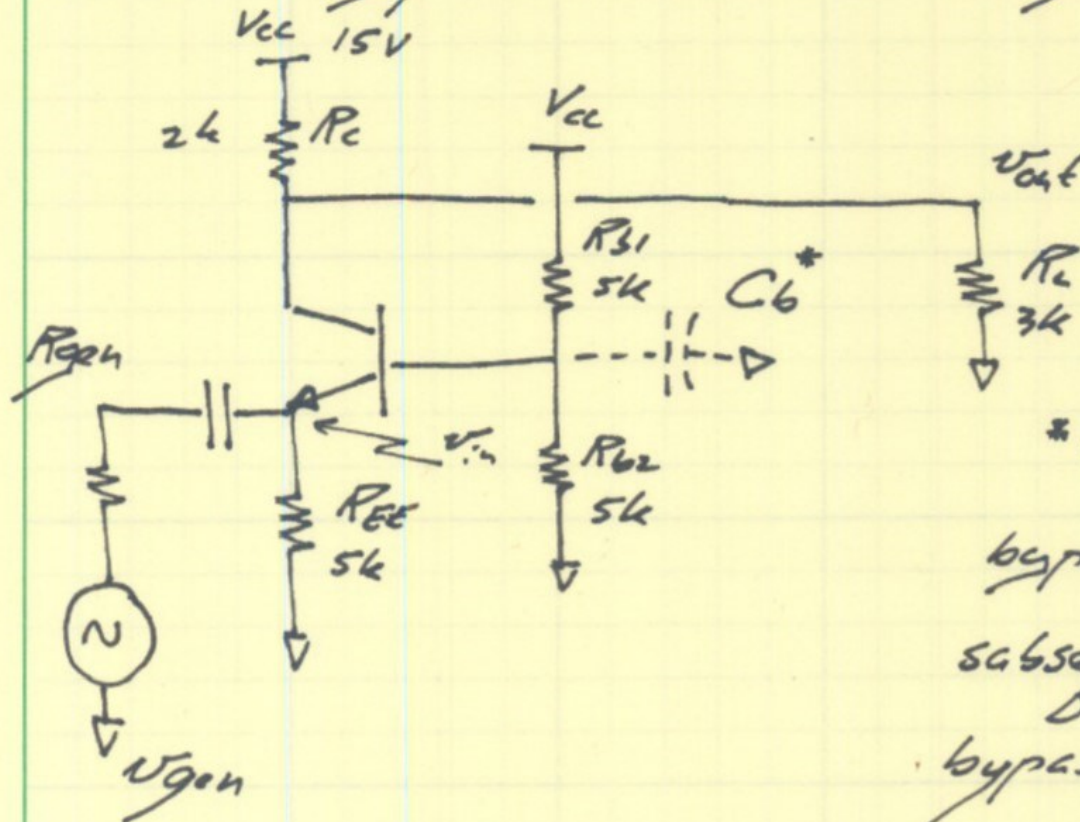


ECE137A, Notes Set 6: Common Gate, Common Base

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Common-base stage

First - analyze common-base stage:



$$\beta = 50$$

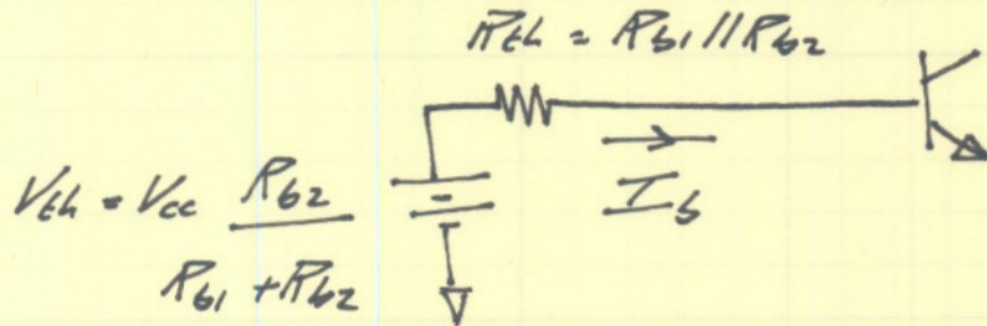
$$V_A = 50V$$

* we will presently not ac bypass the base --- but subsequent analysis shows that bypassing is advisable.

Bias Analysis: Iterative

Assume $\beta \rightarrow \infty \Rightarrow I_B = 0 \Rightarrow V_B = 7.5V \Rightarrow V_E = 6.8V$
 $\Rightarrow I_E = 6.8V / 5k\Omega = 1.36mA$

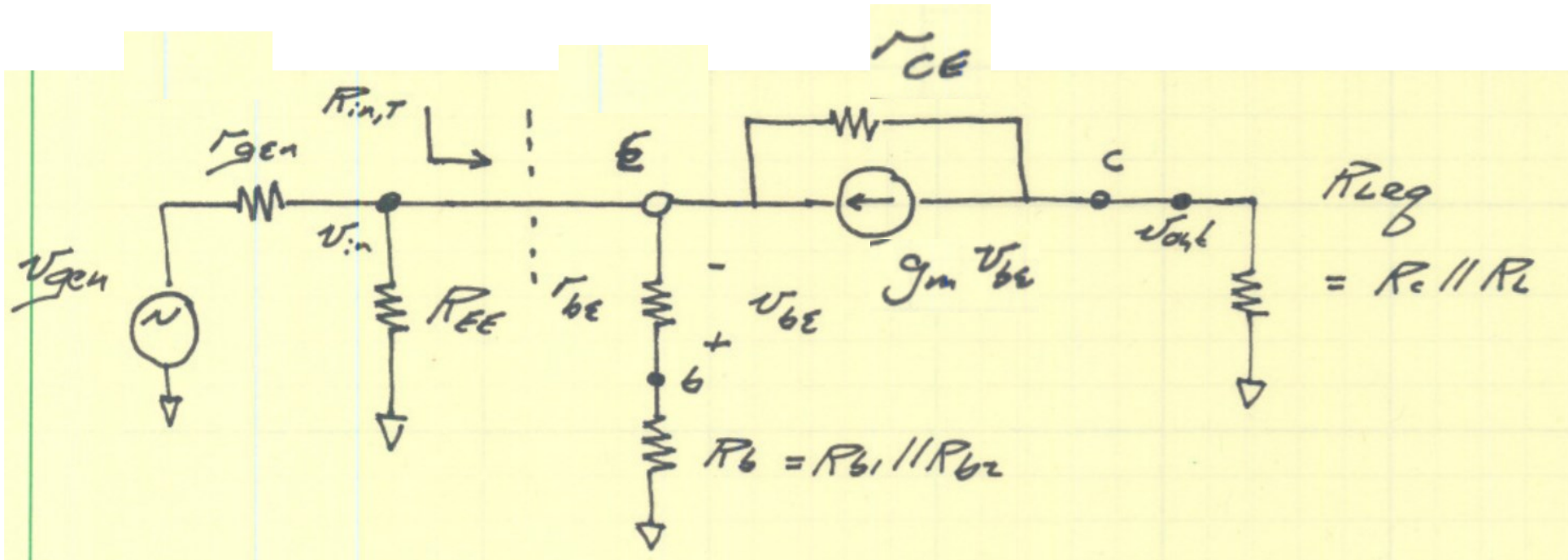
Now assume $\beta = 50 \Rightarrow I_B = I_E / \beta = 27\mu A$



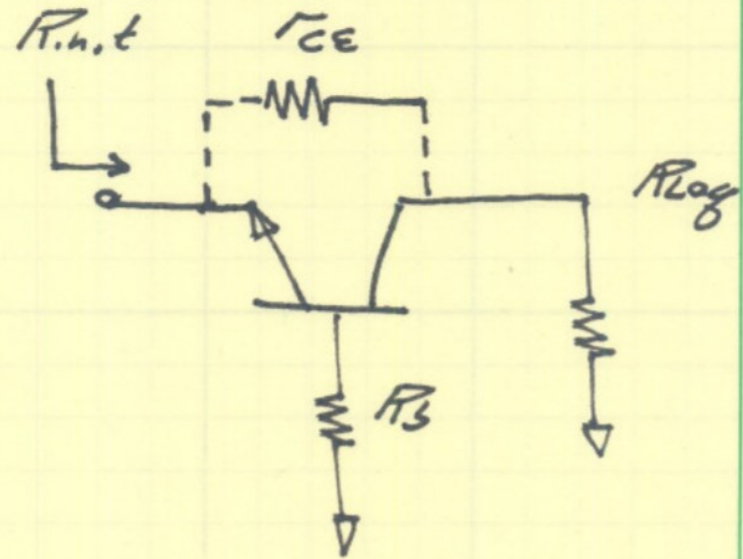
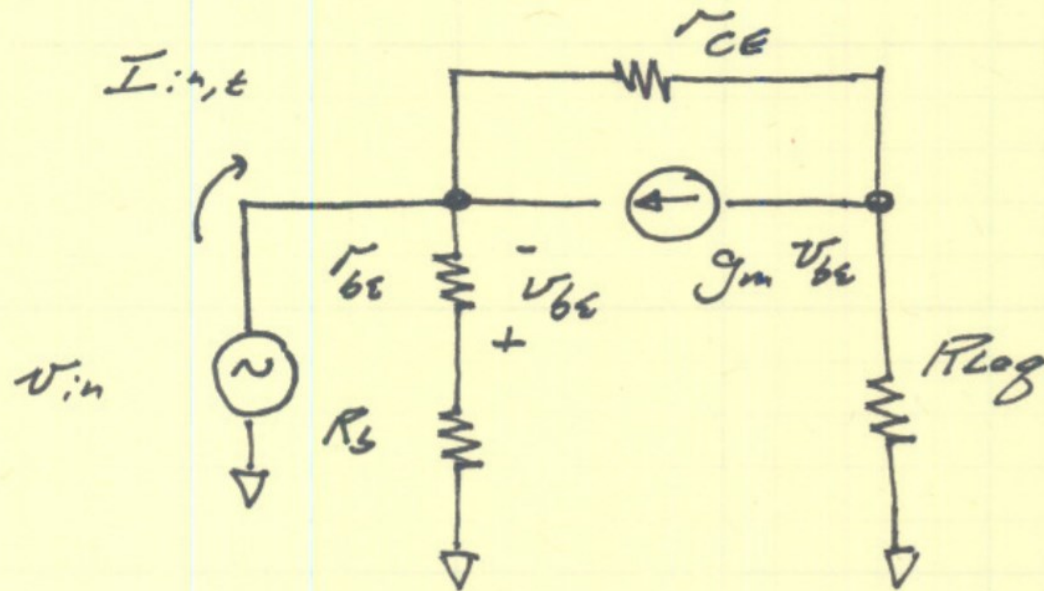
$\Rightarrow V_E = 7.5V - I_B \cdot R_{Th} = 7.5V - 2.5k\Omega \cdot 27\mu A$
 $= 7.5V - 68mV$

a negligible correction
 \rightarrow need not further analyze for
 corrections in I_E .

Nearly exact small-signal analysis



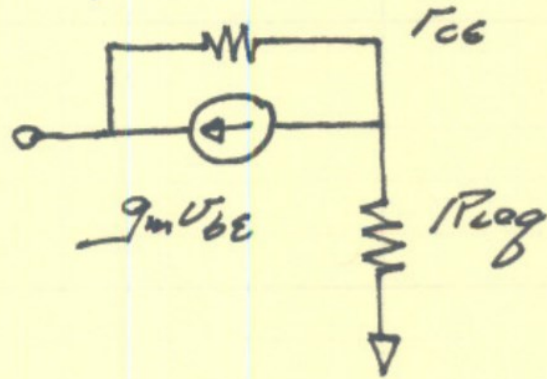
Finding transistor input impedance:



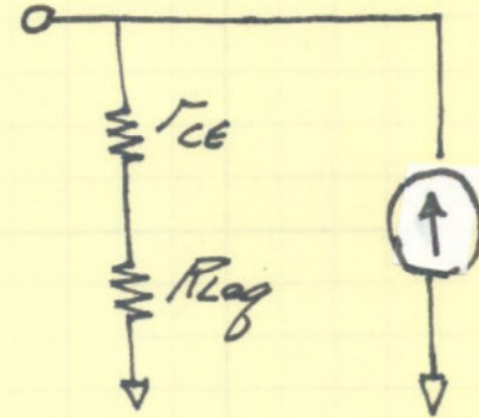
$$v_{in} / I_{in,t} \triangleq R_{in,T}$$

Finding transistor input impedance:

To simplify, and to understand, recognize the current divider in the circuit:



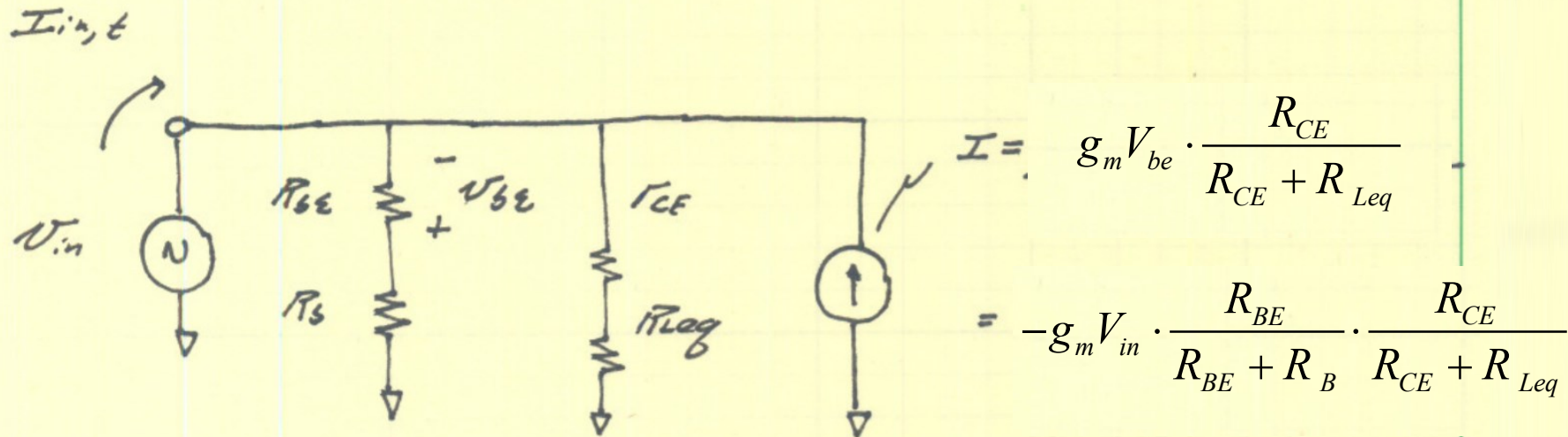
Norton eq. →



$$g_m V_{be} \cdot \frac{R_{CE}}{R_{CE} + R_{Leq}}$$

Finding transistor input impedance:

So we are trying to find R_{in} of the network below:

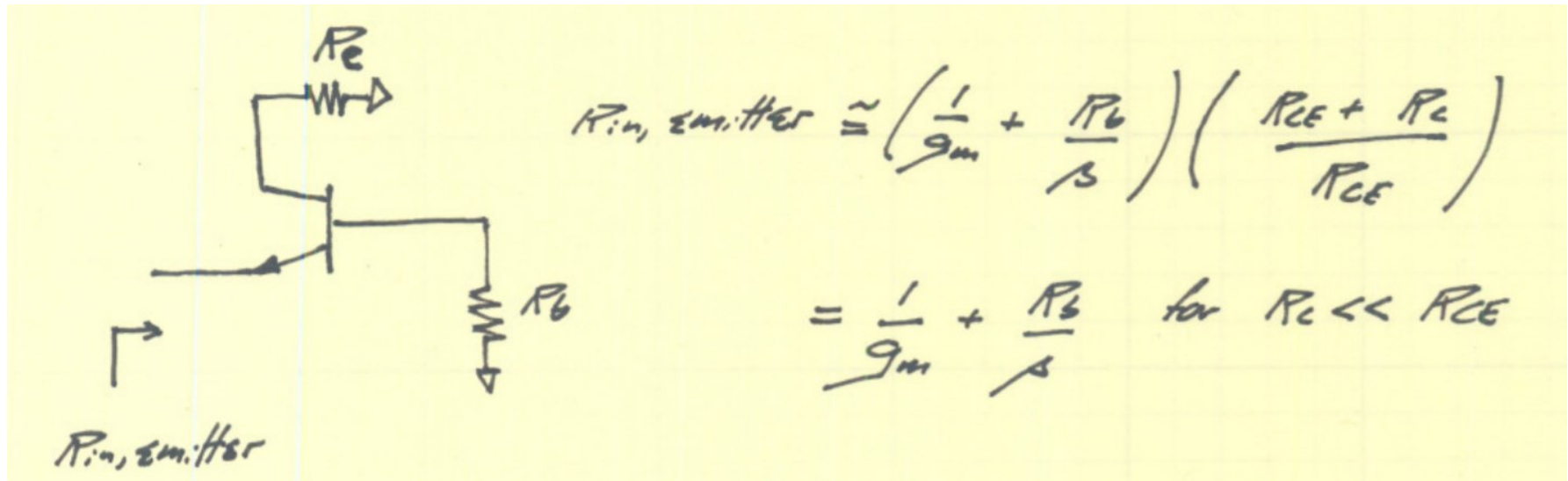
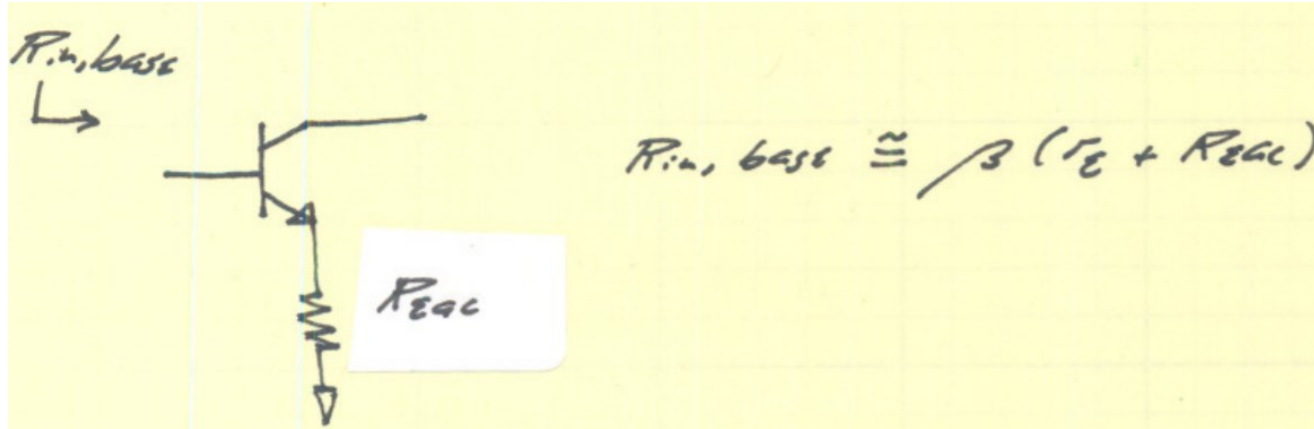


The current in the right-most branch is dominant, so

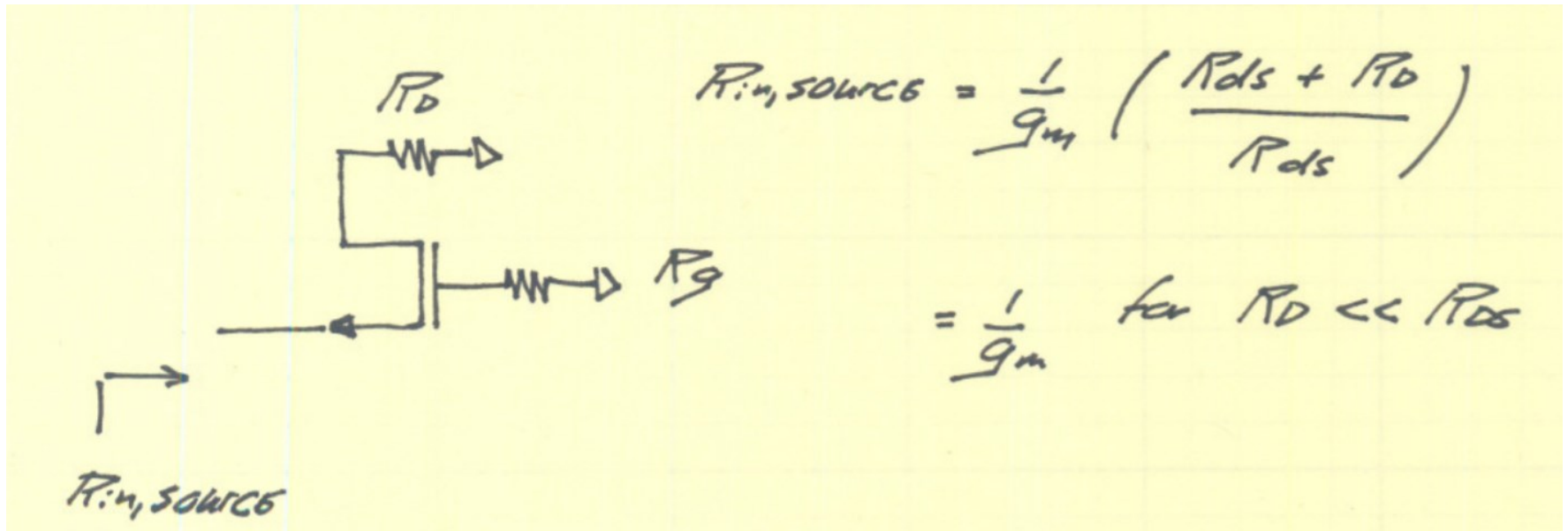
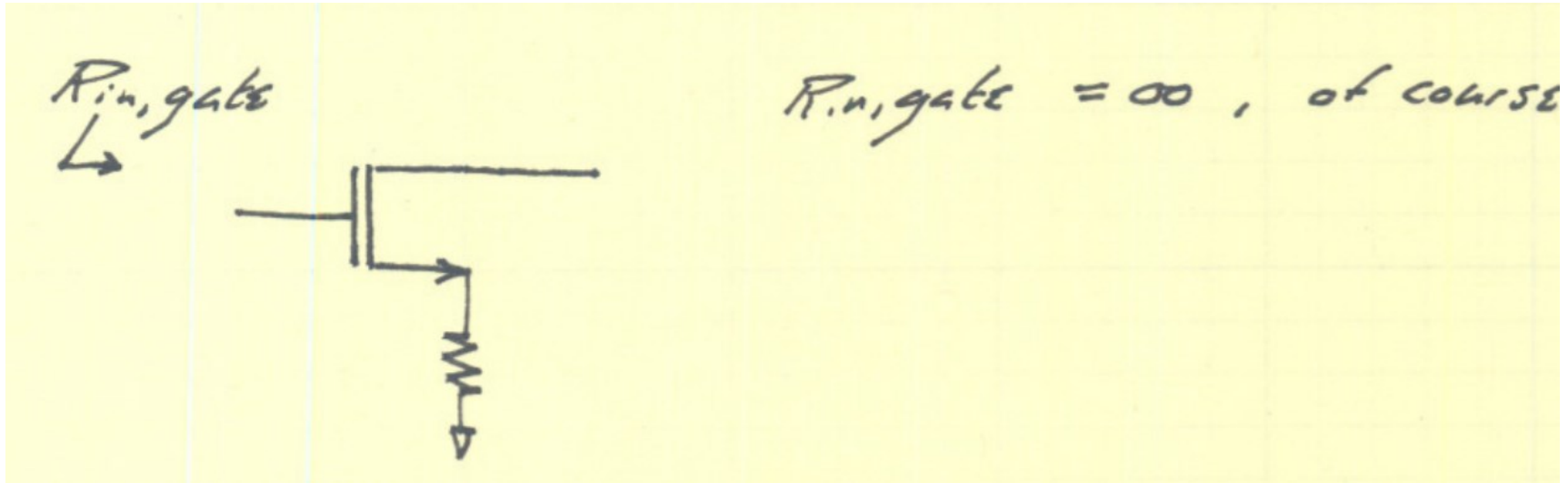
$$R_{in,T} \approx \frac{V_{in}}{I} = \frac{R_{BE} + R_B}{g_m \beta \beta} \frac{R_{log} + r_{CE}}{r_{CE}} = \left(r_E + \frac{R_B}{\beta} \right) \left(\frac{R_{log} + R_{CE}}{R_{CE}} \right)$$

$$R_{in,T} \approx \left(r_E + \frac{R_B}{\beta} \right) \left(\frac{R_{log} + R_{CE}}{R_{CE}} \right) = \left(\frac{1}{g_m} + \frac{R_B}{\beta} \right) \left(\frac{R_{log} + R_{CE}}{R_{CE}} \right)$$

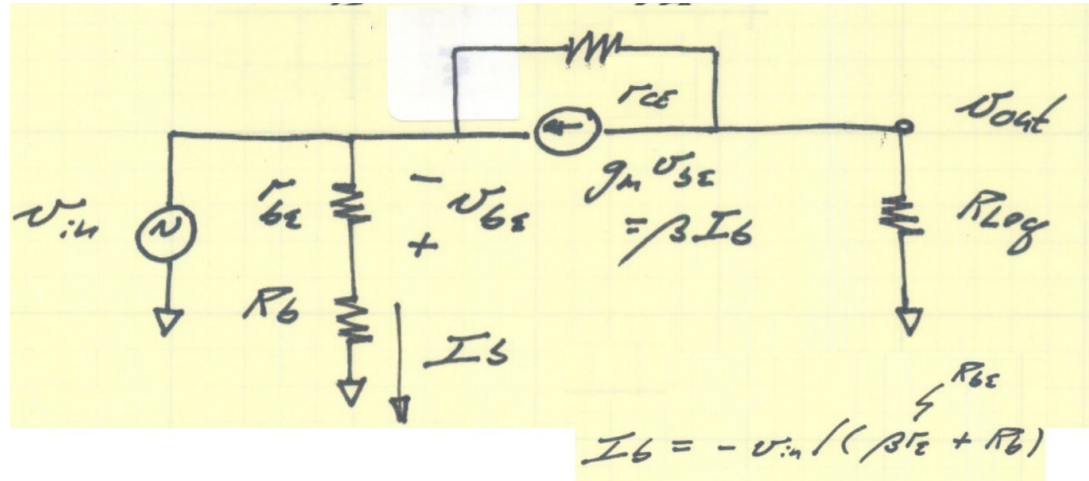
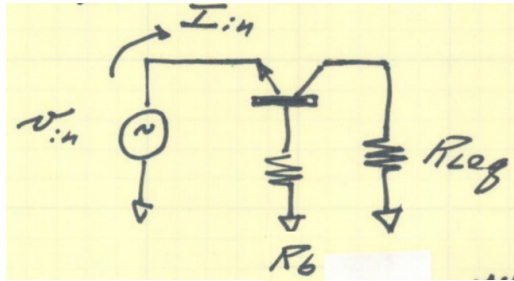
Some pictures:



Some pictures:



Common-base voltage gain



nodal equation at v_{out} :

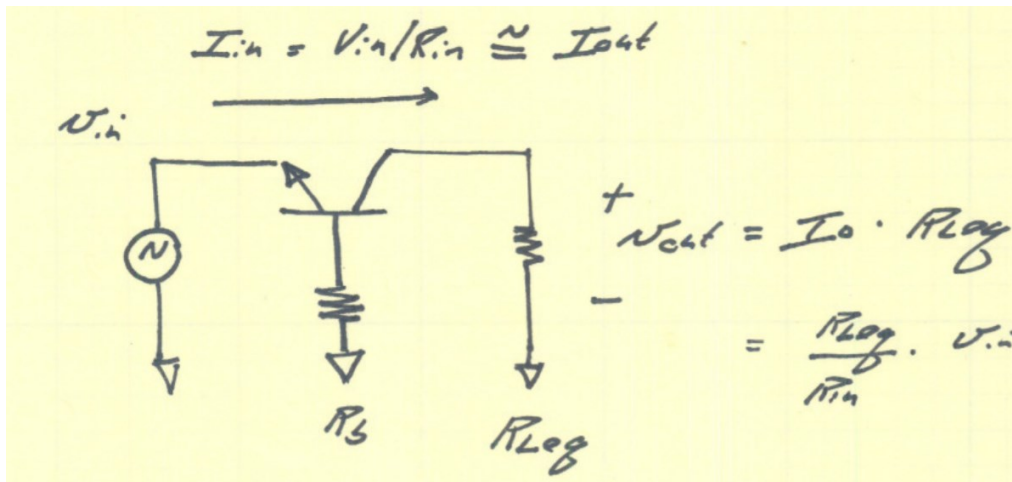
$$0 = v_{out} \left(\frac{1}{R_{Load}} + \frac{1}{r_{CE}} \right) + v_{in} \left(-\frac{1}{r_{CE}} - \frac{\beta}{\beta r_E + R_B} \right)$$

now $r_{CE} \gg r_E + R_B / \beta$ unless R_B is really big...

$$\Rightarrow \frac{v_{out}}{v_{in}} = \frac{1}{r_E + R_B / \beta} \frac{1}{\frac{1}{R_{Load}} + \frac{1}{r_{CE}}}$$

Common-base voltage gain

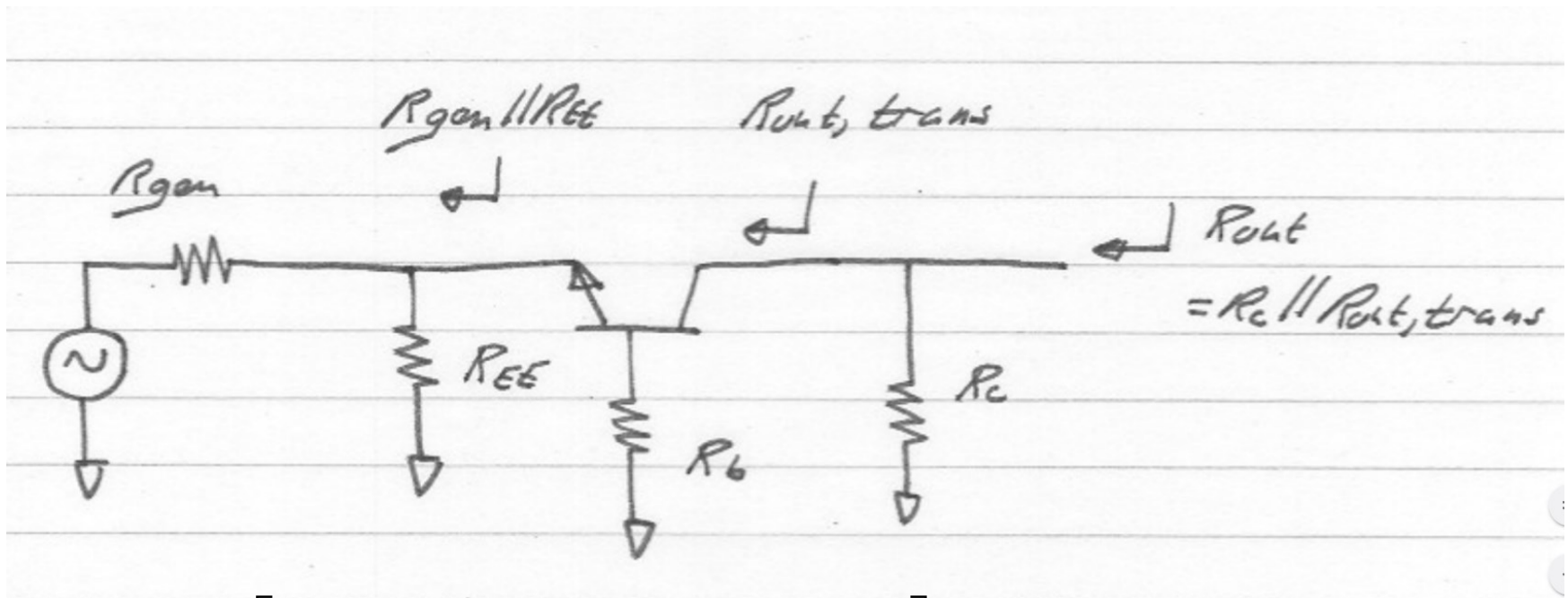
$$\frac{V_{out}}{V_{in}} = \frac{R_{Leq}}{r_e + R_b / \beta} \cdot \frac{R_{ce}}{R_{ce} + R_{Leq}} = \frac{R_{Leq}}{R_{in,emitter}}$$



For the FET, we have the same relationship:

$$\frac{V_{out}}{V_{in}} = \frac{R_{Leq}}{1 / g_m} \cdot \frac{R_{DS}}{R_{DS} + R_{Leq}} = \frac{R_{Leq}}{R_{in,source}}$$

Output impedance: Common-Base



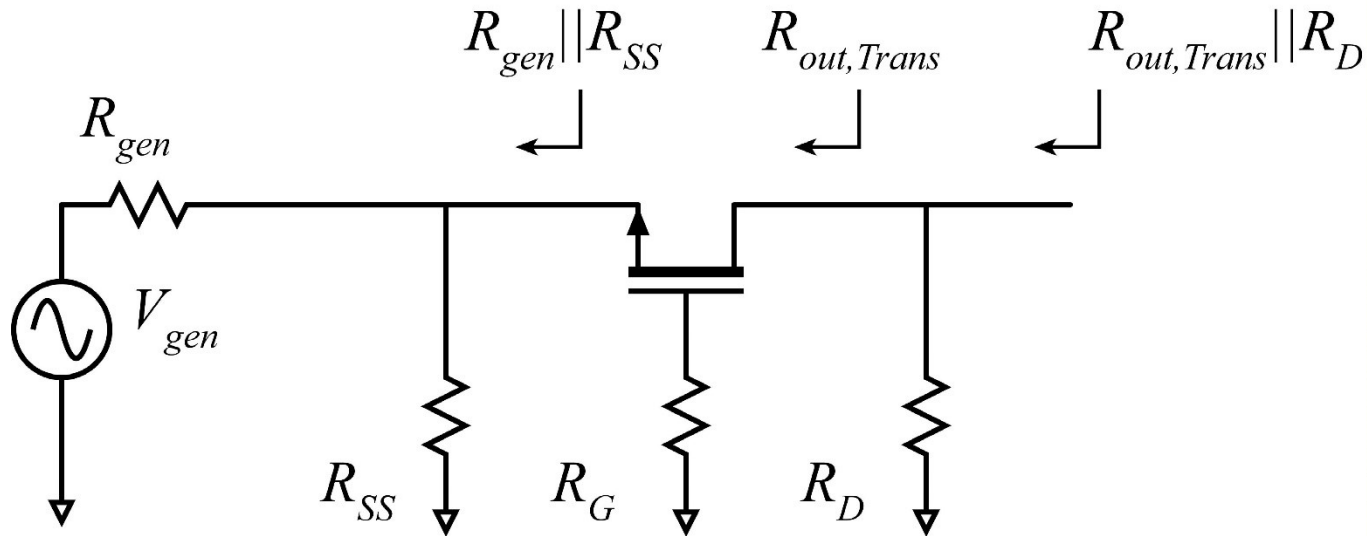
$$R_{out, Trans} = R_{CE} \left[1 + \frac{R_{gen} \parallel R_{EE}}{1/g_m} \frac{R_{be}}{R_{be} + R_b + R_{gen} \parallel R_{EE}} \right] \approx \left[\frac{R_{gen} \parallel R_{EE}}{1/g_m} \right]$$

this is the same analysis as the common-emitter +degeneration output impedance

For the FET this becomes

$$R_{out, Trans} = R_{DS} \left[1 + \frac{R_{gen} \parallel R_{SS}}{1/g_m} \right]$$

Output impedance: Common-Gate



For the FET, the analysis is identical
(except for the absence of R_{be}) and hence:

$$R_{out,Trans} = R_{DS} \left[1 + \frac{R_{gen} \parallel R_{SS}}{1/g_m} \right]$$