

ECE ECE145A (undergrad) and ECE218A (graduate)

Mid-Term Exam. November 8, 2011

Do not open exam until instructed to.

Open notes, open books, etc

You have 1 hr and 15 minutes.

Use any and all reasonable approximations (5% accuracy is fine.) , ***AFTER STATING THEM.***

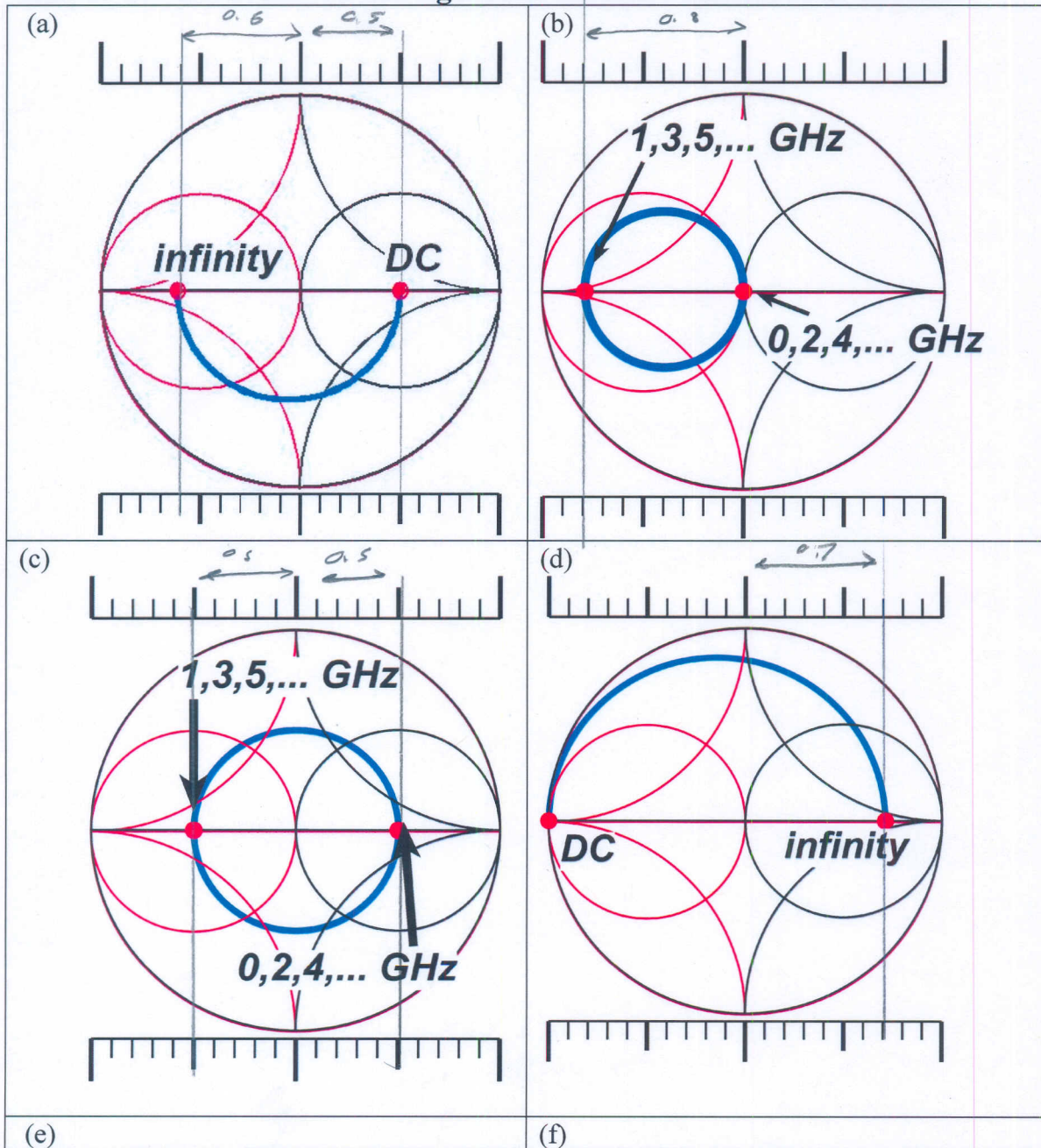
Problem	Points Received	Points Possible
1		20
2a		10
2b		10
2c		10
3a		15
3b		10
4		25
total		100

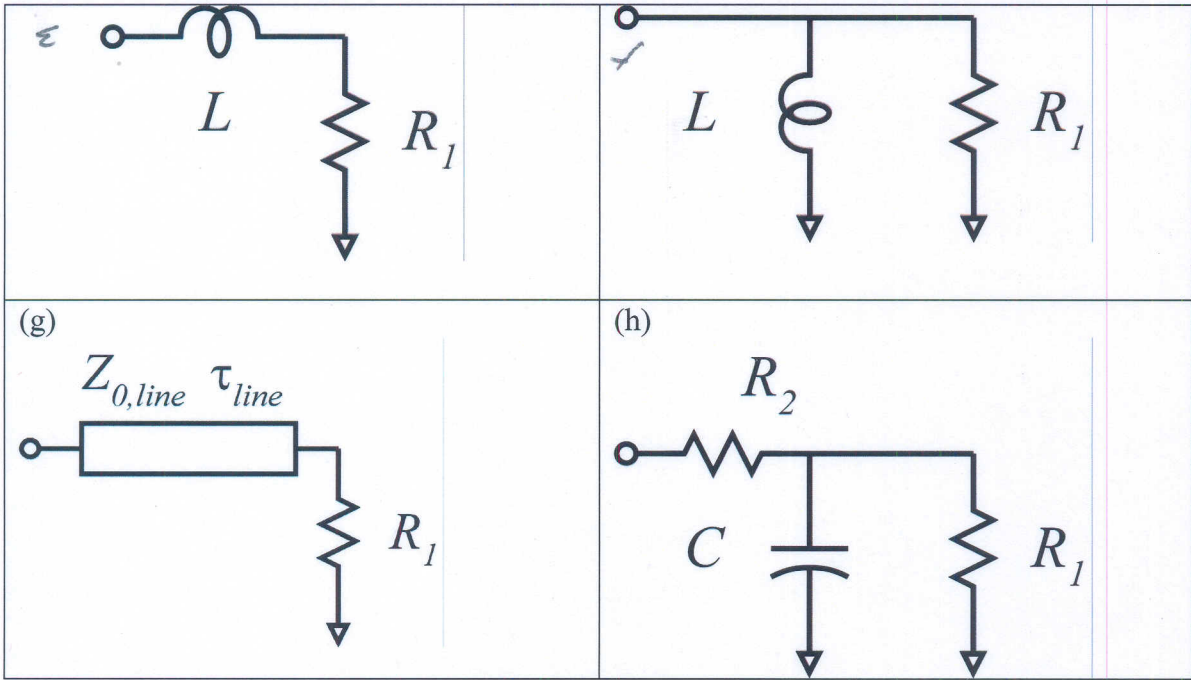
Name: Selatin.

Problem 1, 20 points

The Smith Chart and Frequency-Dependent Impedances.

HINT: use the scales on the figures to measure distances as needed.





a) \textcircled{a} DC, $\Gamma_L = 0.5 \rightarrow R_L = 50\Omega \frac{1+0.5}{1-0.5} = 150\Omega$
 \textcircled{b} $f \rightarrow \infty$, $\Gamma_L = -0.6 \rightarrow R_L = 50\Omega \frac{1-0.6}{1+0.6} = 12.5\Omega$
 \rightarrow circuit H with $R_2 = 12.5\Omega$, $R_1 = 150 - 12.5\Omega = 137.5\Omega$

b) \textcircled{a} DC, 2, 4... GHz, $Z_{in} = 50\Omega$
 \textcircled{b} 1, 3, ... GHz $Z_{in} = 50\Omega \frac{1-0.8}{1+0.8} = 5.55\Omega$
 \rightarrow Quarter-wave line $Z_{in} Z_{load} = Z_{line}^2 = 50\Omega \cdot (5.55\Omega)$
 $\rightarrow Z_{load} = 16.66\Omega$
 $\lambda_{10} = \lambda/4 @ 10\text{GHz} \rightarrow T = 1/4 \text{ ns}$

c) \textcircled{a} DC, 2, 4 GHz, $Z_{in} = 50\Omega \frac{1+0.5}{1-0.5} = 150\Omega$
 \textcircled{b} 1, 3, 5... GHz $Z_{in} = 50\Omega \frac{1-0.5}{1+0.5} = 16.6\Omega$
 \rightarrow Quarter wave line $Z_{in} Z_{load} = Z_{line}^2 =$
 $Z_{line} = (150\Omega \cdot 16.6\Omega)^{1/2} = 50\Omega$
 50Ω line, $1/4$ ns long, loaded by 150Ω

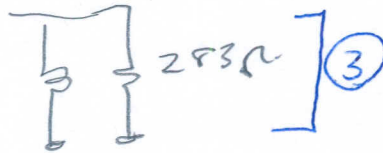
Match each Smith Chart with each circuit, and give all resistor values, and all transmission line delays and characteristic impedances. The charts all use 50 Ohm normalization:

- Smith chart (a). Circuit= H. Component values= $R_1 = 137.5\Omega, R_2 = 12.5\Omega$
 Smith chart (b). Circuit= G. Component values= $R_1 = 50\Omega, Z_{char} = 16.7\Omega, \tau = 4ns$
 Smith chart (c). Circuit= G. Component values= $R_1 = 150\Omega, Z_{in} = 50\Omega, \tau = 4ns$
 Smith chart (d). Circuit= f. Component values= $R_1 = 283\Omega$

(d) impedance is zero @ dc, is

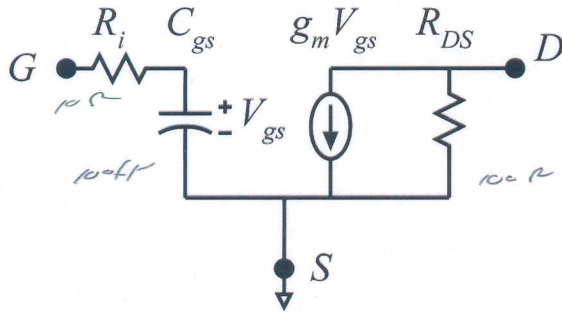
$$\frac{50\Omega(1+0.7)}{(1-0.7)} = 283\Omega$$

②
 @ $f \rightarrow \infty$.



Problem 2, 40 points

Elementary impedance matching network design.



To the left is the equivalent circuit of a FET. The Transconductance is 100 mS, $R_i=10$ Ohms, $C_{gs}=100$ fF, $R_{DS}=100$ Ohms

Part (a), 15 points.

Using the impedance-admittance charts that have been passed out, design a lumped-element matching network to match the input impedance to 50 Ohms at 10 GHz. Use a series inductor and a shunt capacitor. Give the circuit diagram and the element values.

$$100 \text{ fF} \rightarrow Z = j\omega L = 160 \Omega \rightarrow Z/Z_0 = 3.2$$

$$10 \Omega \rightarrow Z/Z_0 = 10/50 = 0.2$$

$$Z = 10 \Omega - j160 \Omega$$

$$Z/Z_0 = 0.2 - j3.2 = \Gamma_A + j\Gamma_A = \frac{1}{A}$$

at point "B", $\frac{1}{\Gamma_B} = 0.2 + j0.4 = \Gamma_B + j\Gamma_B$

$$\Delta Y = Y_B - Y_A = 0.4 - (-3.2) = +3.6$$

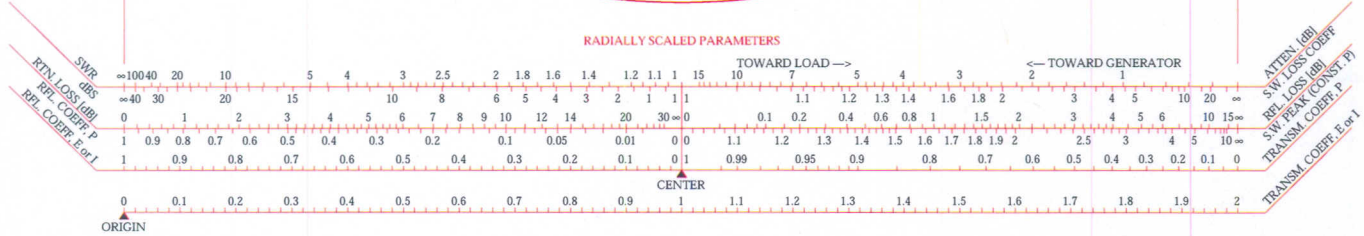
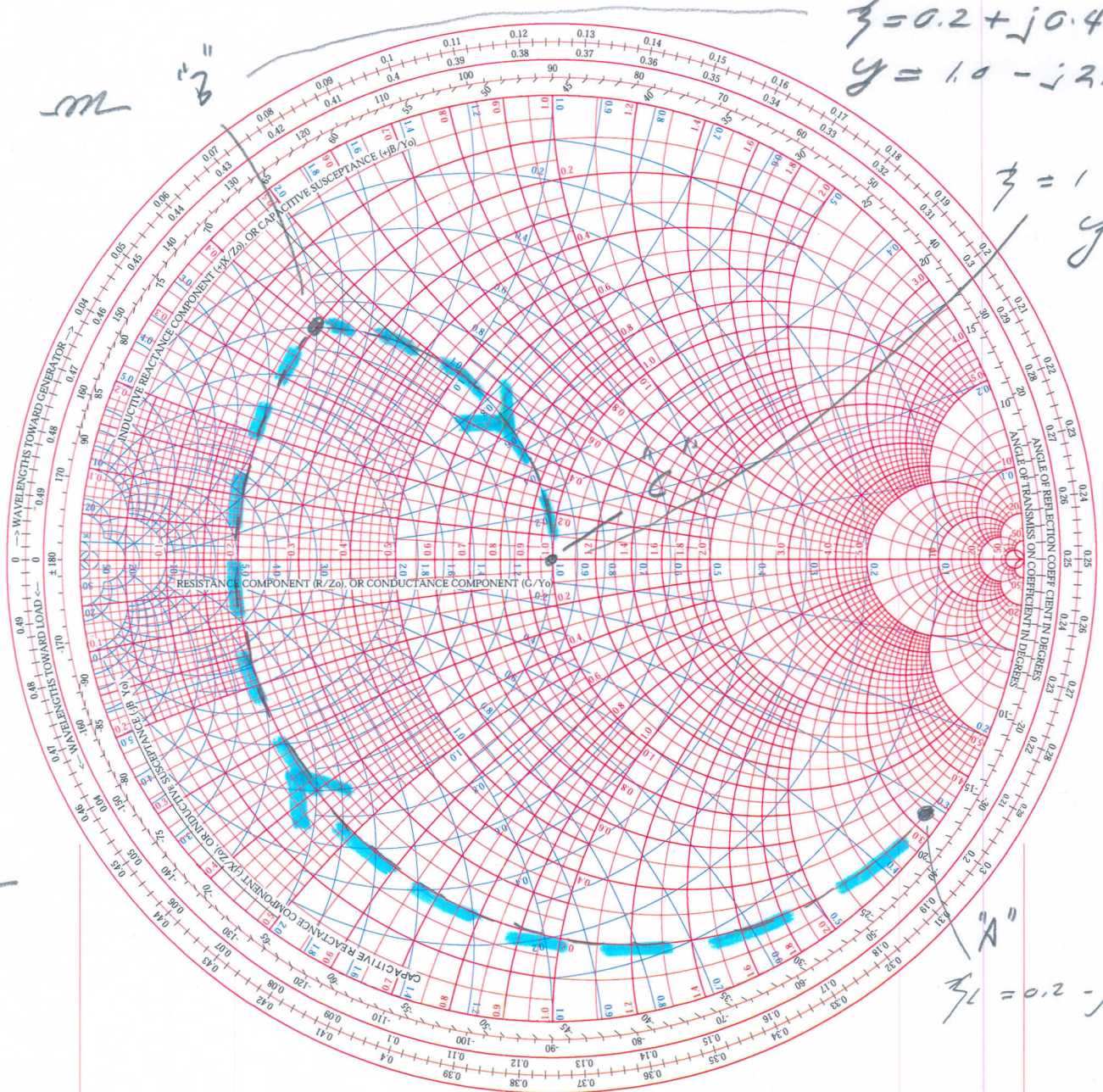
$$\Delta X = \Delta Y \cdot Z_0 = \Delta Y \cdot 50 \Omega = 3.6 \cdot 50 \Omega = 180 \Omega$$

$$\Delta X = \omega L = 180 \Omega \rightarrow L = 180 \Omega / 2\pi f = 2.86 \text{ nH}$$

$\textcircled{2}$ [
 $\textcircled{1}$ point "B", $Y_B = 1 - j2.0$
 $\textcircled{2}$ point "C", $Y_C = 1 - j0$
 $\Delta Y = +2.0 \cdot j$
 $\Delta B = 2.0$
 $\Delta B = 2.0 / 50 \Omega = 0.0405$
 $= \omega C$
 $\rightarrow C = \frac{0.0405}{2\pi f} = 0.64 \text{ pF}$

NAME <i>Solution</i>	TITLE <i>problem 2a</i>	DWG. NO.
SMITH CHART FORM ZY-01-N	Microwave Circuit Design - EE523 - Fall 2000	DATE

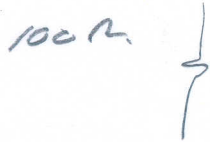
NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES



Part (b), 15 points.

Using the impedance-admittance charts that have been passed out, design a lumped-element matching network to match the output impedance to 50 Ohms at 10 GHz. Use a shunt inductor and a series capacitor. Give the circuit diagram and the element values.

- point A on smith chart - the Z_{out} -



$$\frac{Z}{Z_0} = \frac{100 \Omega}{50 \Omega} = 2.0$$

$$y = 0.5 + j0 = g_a + jb_a$$

- point B on smith chart -

$$\textcircled{2} \left[y_B = 0.5 - j0.5 = g_b + jb_b \right]$$

$$\textcircled{2} \left[\Delta b = b_b - b_a = -0.5 \right]$$

$$\textcircled{2} \left[\Delta B = \Delta b / Z_0 = -0.5 / 50 \Omega = -0.0105 = -10 \text{ mS} \right]$$

$$\textcircled{2} \left[\Delta B = -1 / \omega L \rightarrow L = \frac{-1}{\omega \Delta B} = \frac{-1}{2\pi f \Delta B} = \underline{\underline{1.59 \text{ nH}}} \right]$$

$$\frac{Z}{Z_0} = 1 + j1 = r_b + jx_b$$

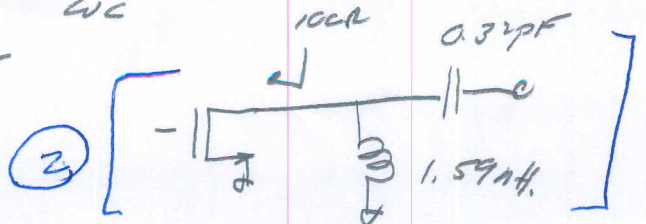
- point C on smith chart

$$\textcircled{2} \left[z_c = 1 + j0 = r_c + jx_c \right]$$

$$\textcircled{2} \left[\Delta x = x_c - x_b = -1.0 \right]$$

$$\textcircled{2} \left[\Delta X = \Delta x \cdot Z_0 = -50 \Omega = \frac{-1}{\omega C} \right]$$

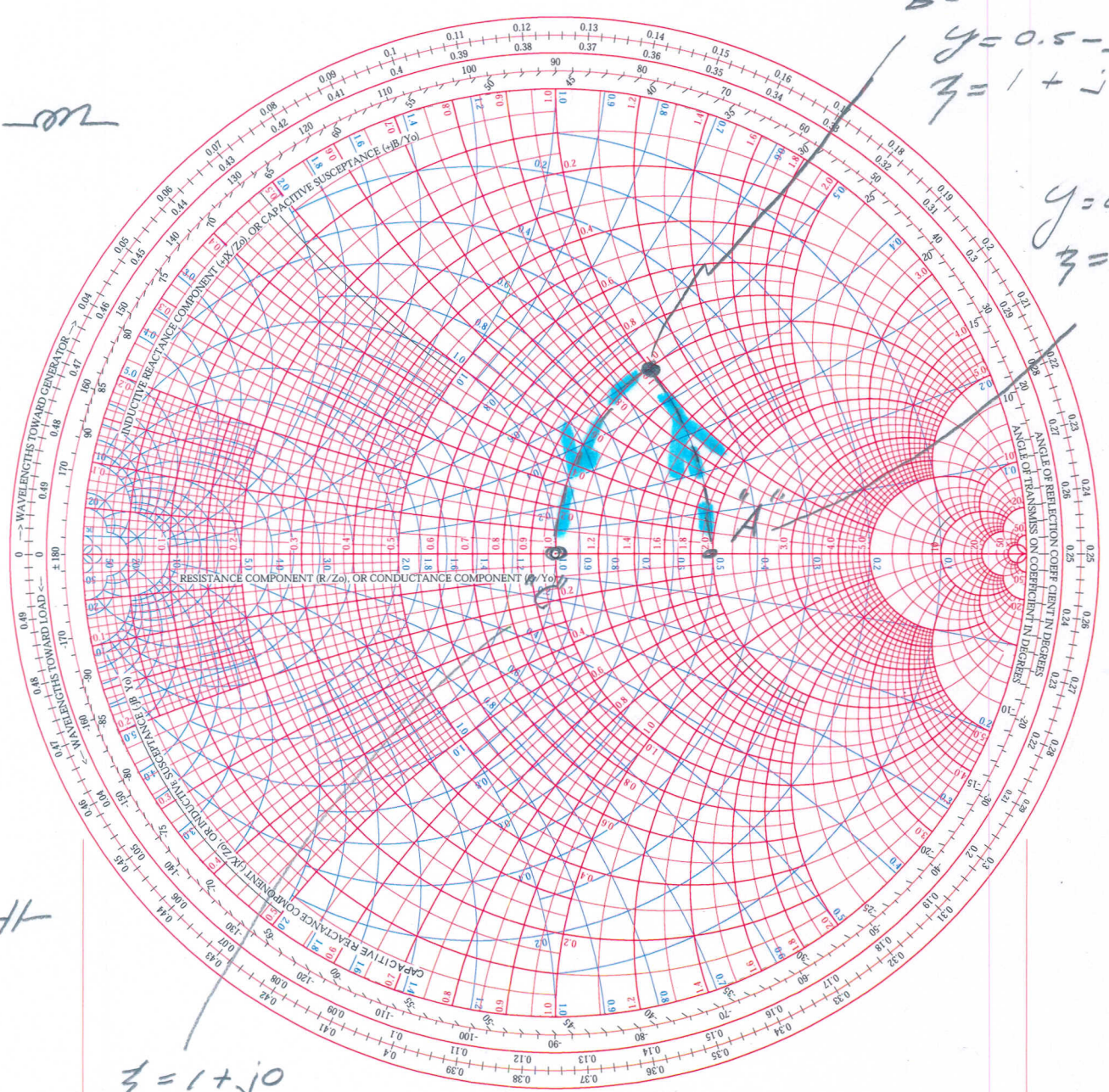
$$\textcircled{2} \left[\rightarrow C = \frac{1}{2\pi f \cdot 50 \Omega} = 0.32 \text{ pF} \right]$$



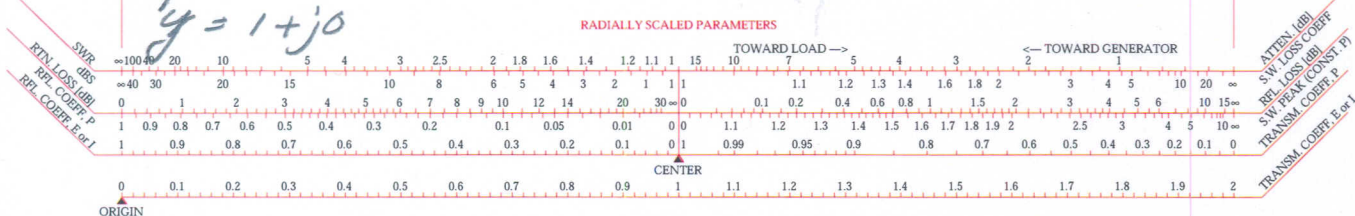
NAME <i>Solatia</i>	TITLE <i>Proble 25</i>	DWG. NO.
SMITH CHART FORM ZY-01-N	Microwave Circuit Design - EE523 - Fall 2000	DATE

NORMALIZED IMPEDANCE AND ADMITTANCE COORDINATES

"B"
 $y = 0.5 - j0.5$
 $Z = 1 + j1$
 $y = 0.5 + j0$
 $Z = 2.0 + j0$

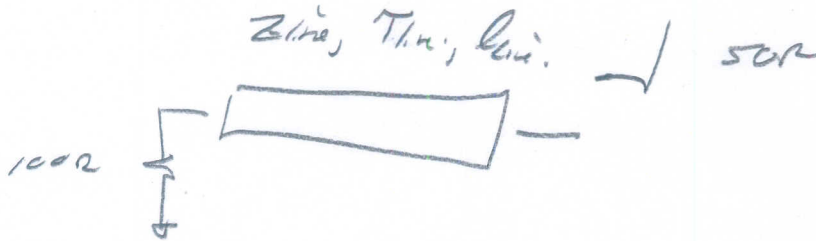


$Z = 1 + j0$
 $y = 1 + j0$



Part (c), 10 points

Now instead design a quarter-wave line to match the load to 50 Ohms. Find the required line impedance and the physical length.



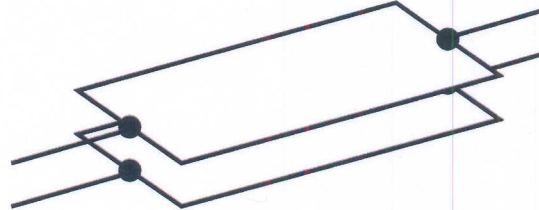
$$Z_{line} = \sqrt{50 \Omega \cdot 100 \Omega} = \underline{70.7 \Omega} \quad (5)$$

$\lambda/4 @ 10 \text{ GHz}$

$$T_{line} = \frac{1}{4} \text{ ns} \quad (5)$$

Problem 3, 25 points*Transmission-lines and lumped elements*Part a: 5 points

A transmission line has plates of $300 \mu\text{m}$ width and $100 \mu\text{m}$ separation. The line is 1 cm long. The region between the plates has a dielectric constant of 2.0 . Neglect the fringing fields at the edges of the plates.



Find the following:

characteristic impedance: 89 Ω
 propagation velocity: $2.12 \cdot 10^8 \text{ m/s}$
 propagation delay: 47.1 ps
 total inductance: 4.2 nH
 total capacitance: 0.53 pF

$$Z_0 = \frac{\sqrt{\frac{\mu_0}{\epsilon_0}}}{\sqrt{\epsilon_r}} \cdot \frac{H}{W} = \frac{377 \Omega}{\sqrt{2}} \cdot \frac{100 \mu\text{m}}{300 \mu\text{m}} = 89 \Omega \quad] \textcircled{1}$$

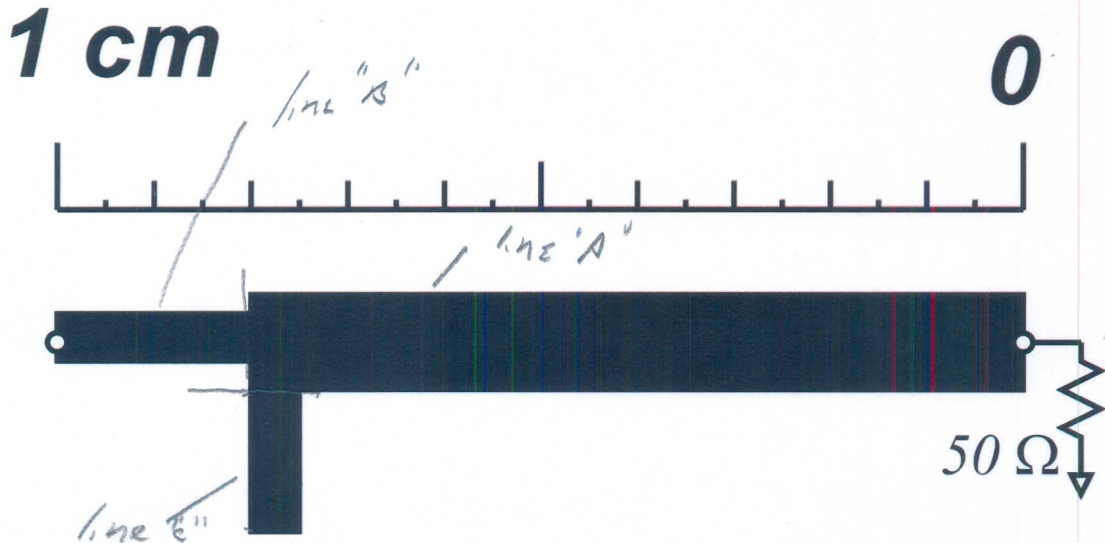
$$v = \frac{c}{\sqrt{\epsilon_r}} = \frac{c}{\sqrt{2}} = 2.12 \cdot 10^8 \text{ m/s} \quad] \textcircled{1}$$

$$\tau = l/v = 1 \text{ cm}/v = 47.1 \text{ ps} \quad] \textcircled{1}$$

$$L = Z_0 \tau = 89 \Omega \cdot 47.1 \text{ ps} = 4.2 \text{ nH} \quad] \textcircled{1}$$

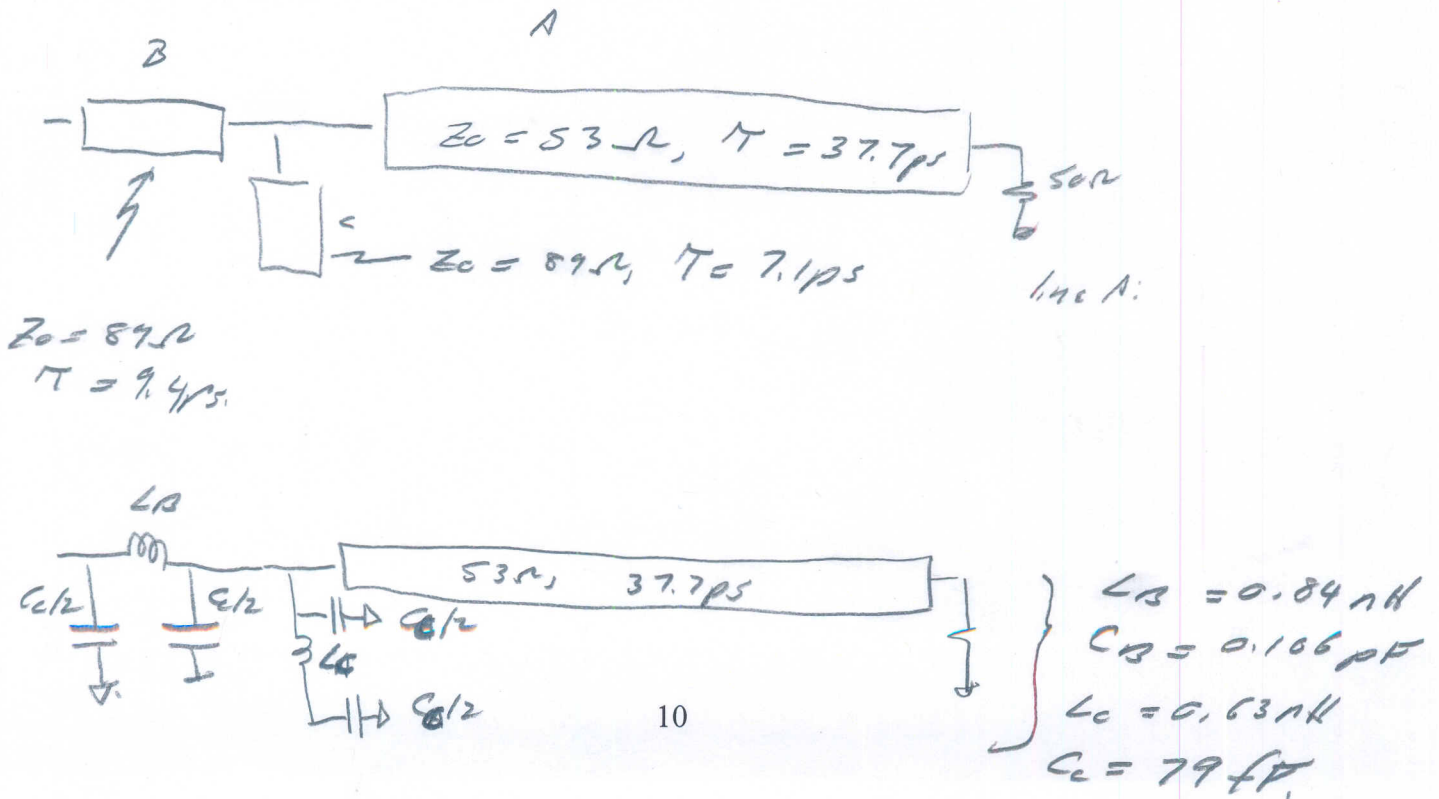
$$C = \tau/Z_0 = 0.53 \text{ pF} \quad] \textcircled{1}$$

part b, 10 points



Above is an accurate scale drawing of a microstrip circuit. The dots represent the connection points. The circuit board is 0.25 mm thick and has a dielectric constant of 2.0. To approximately model fringing fields, the effective conductor width is taken as the physical conductor width plus the board thickness.

First, draw a transmission-line equivalent circuit for the circuit, giving all characteristic impedances and line propagation delays. **Second**, assuming a signal frequency of 5 GHz, draw a second circuit diagram in which you replace line sections shorter than an eight-wavelength with T or Pi-section models, giving the computed values of all LC elements of these sections.



line "A" - width 1 mm, length 8 mm

$$\textcircled{1} \left[Z_0 = \frac{377 \Omega}{\sqrt{27}} \cdot \frac{0.25 \text{ mm}}{1 \text{ mm} + 0.25 \text{ mm}} = 53.3 \Omega \right]$$

$$\textcircled{1} \left[v = \frac{c}{\sqrt{\epsilon_r}} = 2.12 \cdot 10^8 \text{ m/s} \right]$$

$$\textcircled{1} \left[T = \frac{8 \text{ mm}}{v} = 37.7 \text{ ps} \right] \quad \# \text{ wavelengths} = f \cdot T = 0.1885 = \frac{1}{5.3}$$

line "B" length 2 mm width 1/2 mm

$$\textcircled{1} \left[Z_0 = \frac{377 \Omega}{\sqrt{27}} \cdot \frac{0.25 \text{ mm}}{0.5 \text{ mm} + 0.25 \text{ mm}} = 89 \Omega \right]$$

$$\left[v = 2.12 \cdot 10^8 \text{ m/s} \right]$$

$$\textcircled{1} \left[T = \frac{2 \text{ mm}}{v} = 9.4 \text{ ps} \right] \quad \# \text{ wavelength} = f \cdot T = 0.047 = \frac{1}{21}$$

line c length 1.5 mm width 1/2 mm

$$\frac{1}{2} \left[Z_0 = 89 \Omega \right]$$

$$\frac{1}{2} \left[v = 2.12 \cdot 10^8 \text{ m/s} \right]$$

$$\textcircled{1} \left[T = \frac{1.5 \text{ mm}}{v} = 7.07 \text{ ps} \right] \quad \# \text{ wavelengths} = f \cdot T = 0.035 = \frac{1}{28}$$

TT-sections: lines B & c are $< \lambda/8$ $\textcircled{1}$

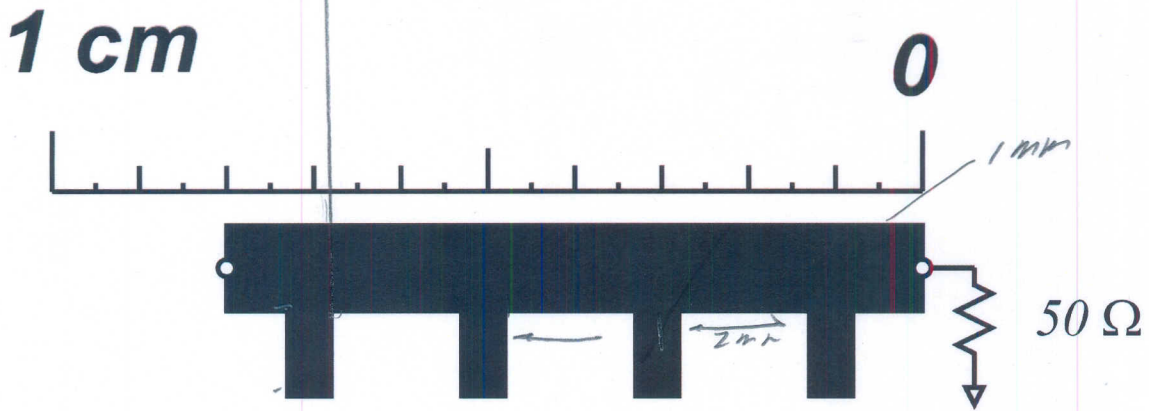
$$\text{line B} \rightarrow L_B = Z_0 T = 0.84 \text{ nH} \quad \left. \right]^{1/2}$$

$$C_B = T/Z_0 = 0.106 \text{ pF} \quad \left. \right]^{1/2}$$

$$\text{line c} \rightarrow L_c = Z_0 T = 0.63 \text{ nH} \quad \left. \right]^{1/2}$$

$$C_c = T/Z_0 = 79 \text{ fF} \quad \left. \right]^{1/2}$$

part c, 10 points

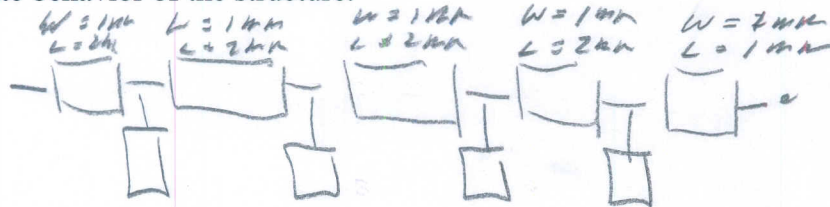


We now repeat the problem for the structure above.

First draw an equivalent circuit using transmission-line sections for all elements, giving all line impedances and delays.

Second draw a transmission line circuit where all elements are replaced by LC *PI-sections*., giving the values of all L's and C's.

Third, neglecting the *inductances* of the *shunt line elements*, please comment on the approximate behavior of the structure.

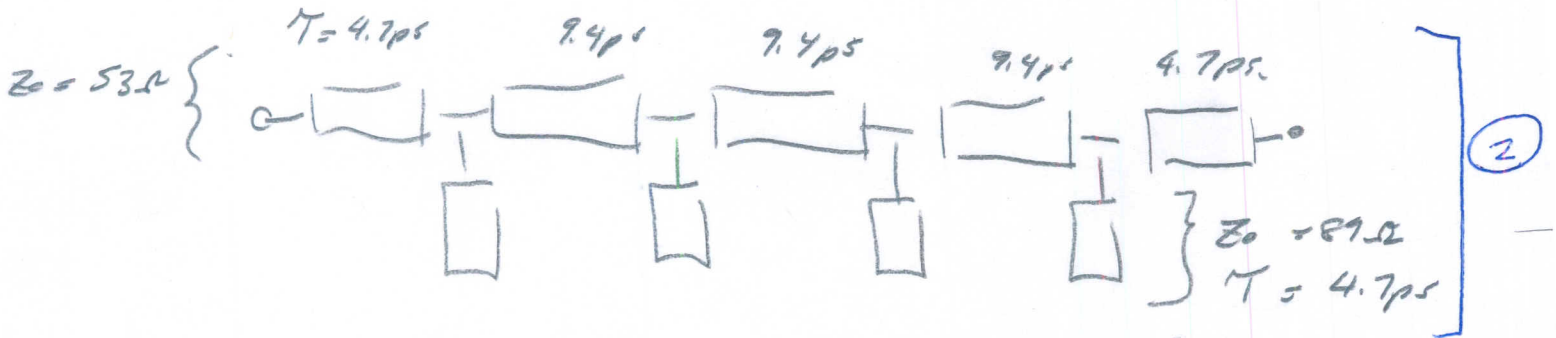


Series lines: $1\text{mm wide} \rightarrow 53\Omega, 2.12 \cdot 10^{-11}\text{m/s.}]^{1/2}$
 lengths = $1, 2\text{mm}, \rightarrow \tau = 4.7\text{ps}, 9.4\text{ps}]^{1/2}$

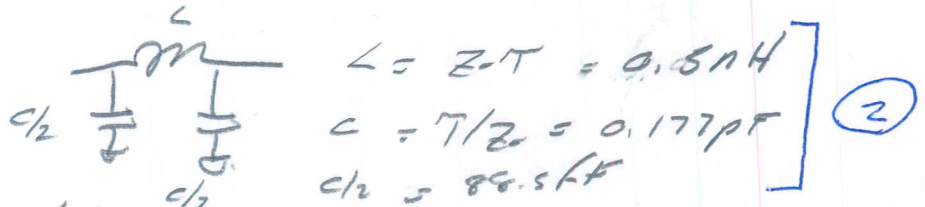
Stubs
 $1/2\text{mm wide} \rightarrow Z_0 = 89\Omega]^{1/2}$
 $1\text{mm long} \rightarrow \tau = 1\text{mm}/v = 4.7\text{ps.}]^{1/2}$

111.

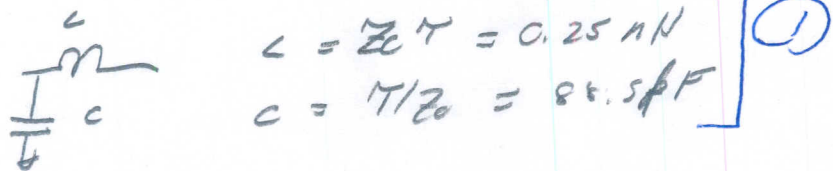
Transmission-line model:



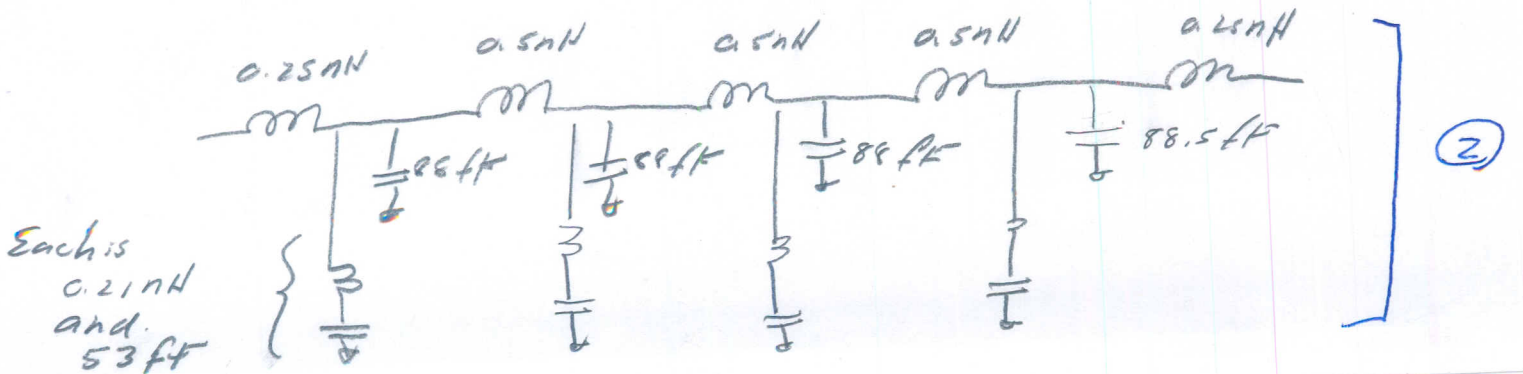
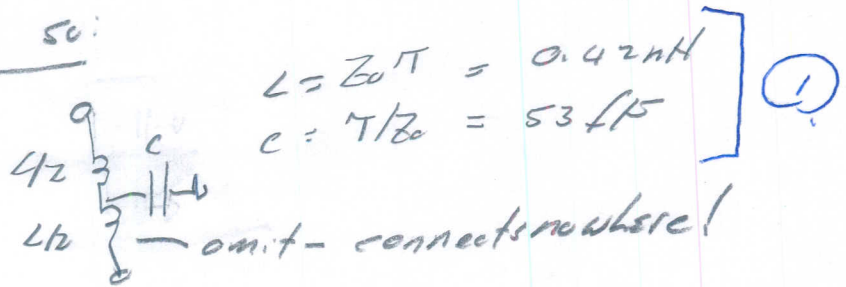
Model longer series lines su:



Model shorter lines su:

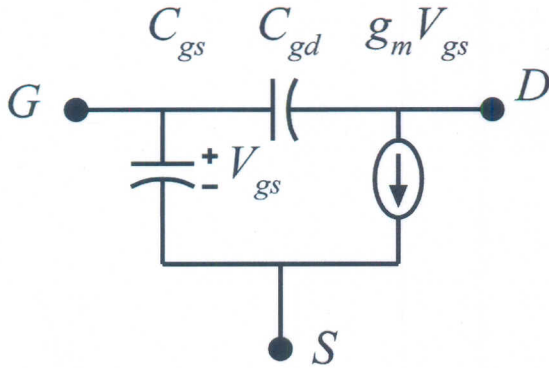


Model stubs like su:



If we remove the series inductance of
the short section, we have an
L-C ladder network - an LC low-pass
filter.

Problem 4, 15 points
resistive feedback amplifiers



A FET has a transconductance of 0.3 mS per micron of gate width.
 $f_t = g_m / (2\pi(C_{gs} + C_{gd}))$ is 100 GHz, and C_{gd} is 20% of C_{gs} .

Design a resistive feedback amplifier with 12 dB gain S21 for a 50 Ohm system using this FET. Draw the circuit diagram with all element values and determine the following:

FET width = 333 μ m
 transconductance = 100 mS
 $C_{gs} =$ 127 fF
 $C_{dg} =$ 32 fF

amplifier 3-dB bandwidth (from nodal analysis or the time constant method).

20.2 GHz

① [12 dB \rightarrow $A_v = -4$

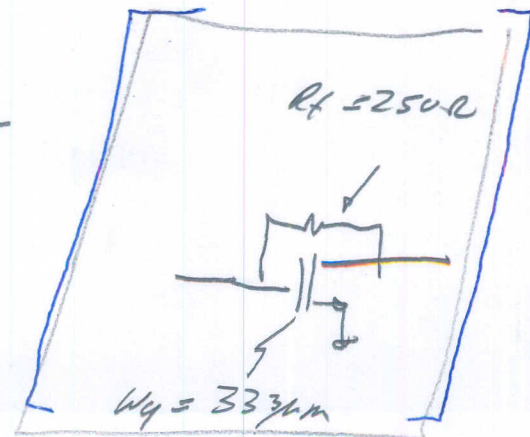
② [$g_m = \frac{1-A}{Z_0} = \frac{1-(-4)}{50} = \frac{5}{50} = 100 \text{ mS}$

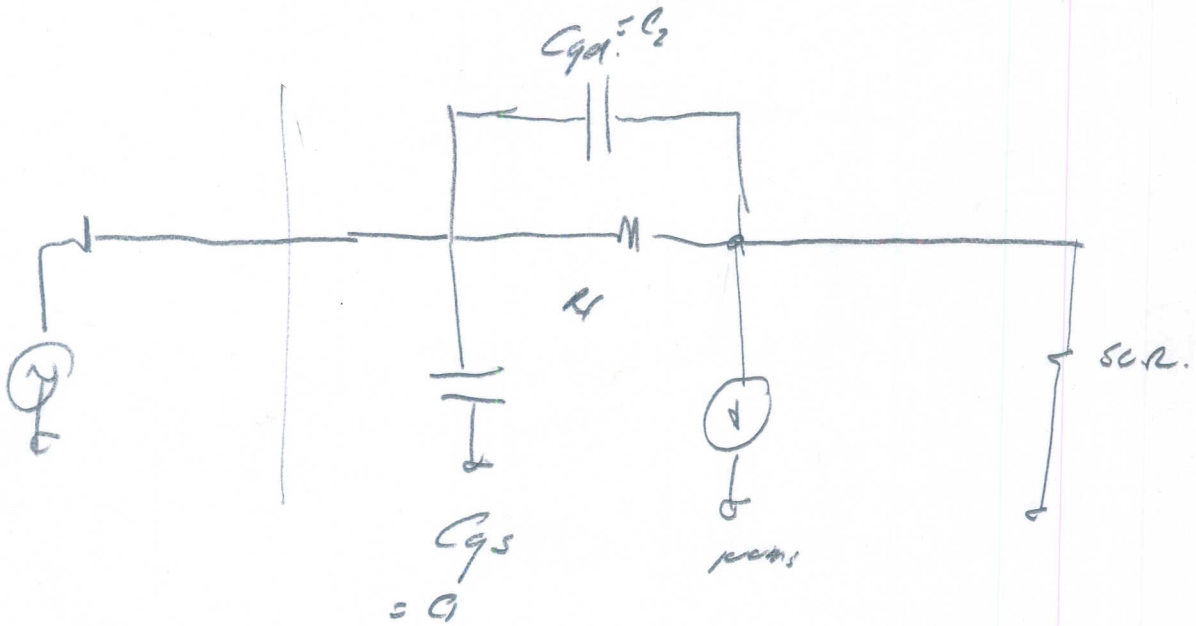
① [$W_g = \frac{g_m}{(g_m/W_g)} = \frac{100 \text{ mS}}{0.3 \text{ mS}/\mu\text{m}} = \underline{\underline{333 \mu\text{m}}}$ \rightarrow many fingers!

② [$C_{gs} = 0.8 \cdot \frac{g_m}{2\pi f_t} = 0.127 \text{ pF}$

② [$C_{gd} = 0.2 \cdot \frac{g_m}{2\pi f_t} = 0.032 \text{ pF} = 32 \text{ fF}$

① [$R_f = Z_0(1-A) = 50 \Omega(5) = 250 \Omega$





Time constant by MTC:

③ [due to C_{gs} : $\tau = R_{in}^0 \cdot C_{gs} = 50 \Omega // 50 \Omega \cdot C_{gs}$
 $= 25 \Omega \cdot C_{gs} = 3.2 \text{ ps}$]

C_{gd} time constant is much more tricky, and the answer will be treated as extra credit —

If we remove R_L , then resistance seen by C_{gd} is:

$$R_{22}^0 = \frac{50 \Omega}{\beta + 1} [1 + \beta R_L] + R_L = 50 \Omega [1 + 100 \cdot 50 \Omega] + 50 \Omega = 350 \Omega$$

If we then replace out with R_L , then

$$R_{22}^0 = 350 \Omega // R_L = 350 \Omega // 250 \Omega = 146 \Omega$$

$$\tau = 146 \Omega \cdot 32 \text{ fF} = 4.66 \text{ ps}$$

② [$\tau_1 = 4.66 \text{ ps} + 3.2 \text{ ps} = 7.86 \text{ ps}$] → ① [$f_{3dB} = 1 / (2\pi \tau_1) = 20.26 \text{ GHz}$]

Start 4 pts.