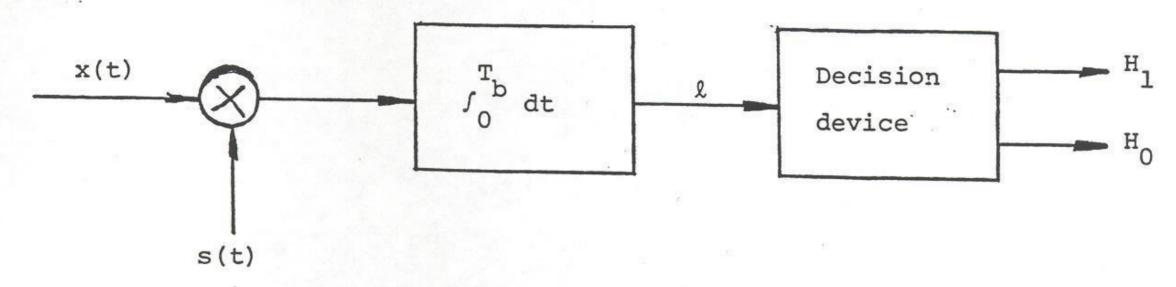
# (a) ASK with coherent reception



Denoting the presence of symbol 1 or symbol 0 by hypothesis  $H_1$  or  $H_0$ , respectively, we may write

$$H_1$$
:  $x(t) = s(t) + w(t)$ 

$$H_0$$
:  $x(t) = w(t)$ 

where  $s(t) = A_c cos(2\pi f_c t)$ , with  $A_c = \sqrt{2E_b/T_b}$ . Therefore,

$$l = \int_{0}^{T_{b}} x(t) s(t) dt$$

If  $l > E_b/2$ , the receiver decides in favor of symbol 1. If  $l < E_b/2$ , it decides in favor of symbol 0.

The conditional probability density functions of the random variable L, whose value

is denoted by &, are defined by

$$f_{L|0}(\ell|0) = \frac{1}{\sqrt{\pi N_0 E_b}} \exp(-\frac{\ell^2}{N_0 E_b})$$

$$f_{L|1}(\ell|1) = \frac{1}{\sqrt{\pi N_0 E_b}} \exp[-\frac{(\ell - E_b)^2}{N_0 E_b}]$$

The average probability of error is therefore,

$$P_{e} = P_{o} \int_{E_{b}/2}^{\infty} f_{L10}(l_{1}|0)d_{l_{1}} + P_{1} \int_{-\infty}^{E_{b}/2} f_{L11}(l_{1}|1)dl$$

$$= \frac{1}{2} \int_{E_{b}/2}^{\infty} \frac{1}{\sqrt{\pi N_{0}E_{b}}} \exp(-\frac{l_{2}^{2}}{N_{0}E_{b}})dl_{1} + \frac{1}{2} \int_{-\infty}^{E_{b}/2} \frac{1}{\sqrt{\pi N_{0}E_{b}}} \exp[-\frac{(l_{2}-E_{b})^{2}}{N_{0}E_{b}}]dl_{1}$$

$$= \frac{1}{\sqrt{\pi N_{0}E_{b}}} \int_{E_{b}/2}^{\infty} \exp(-\frac{l_{2}^{2}}{N_{0}E_{b}})dl_{1}$$

$$= \frac{1}{2} \operatorname{erfc}(\frac{1}{2} \sqrt{E_{b}/N_{0}})$$

The transmitted binary PSK signal is defined by

$$s(t) = \begin{cases} \sqrt{E_b} \phi(t), & 0 \le t \le T_b, & \text{symbol 1} \\ -\sqrt{E_b} \phi(t), & 0 \le t \le T_b, & \text{symbol 0} \end{cases}$$

where the basis function  $\phi(t)$  is defined by

$$\phi(t) = \sqrt{\frac{2}{T_b}} \cos(2\pi f_c t)$$

The locally generated basis function in the receiver is

$$\begin{split} \phi_{\rm rec}(t) &= \sqrt{\frac{2}{T_b}} \cos(2\pi f_c t + \varphi) \\ &= \sqrt{\frac{2}{T_b}} [\cos(2\pi f_c t) \cos \varphi - \sin(2\pi f_c t) \sin \varphi] \end{split}$$

where  $\phi$  is the phase error. The correlator output is given by

$$y = \int_0^{T_b} x(t) \varphi_{\rm rec}(t) dt$$

where

$$x(t) = s_k(t) + w(t),$$
  $k = 1, 2$ 

Assuming that  $f_c$  is an integer multiple of  $1/T_b$ , and recognizing that  $\sin(2\pi f_c t)$  is orthogonal to  $\cos(2\pi f_c t)$  over the interval  $0 \le t \le T_b$ , we get

$$y = \pm \sqrt{E_b} \cos \varphi + W$$

when the plus sign corresponds to symbol 1 and the minus sign corresponds to symbol 0, and W is a zero-mean Gaussian variable of variance  $N_0/2$ . Accordingly, the average probability of error of the binary PSK system with phase error  $\varphi$  is given by

$$P_e = \frac{1}{2} \operatorname{erfc} \left( \sqrt{\frac{E_b \cos^2 \varphi}{N_0}} \right)$$

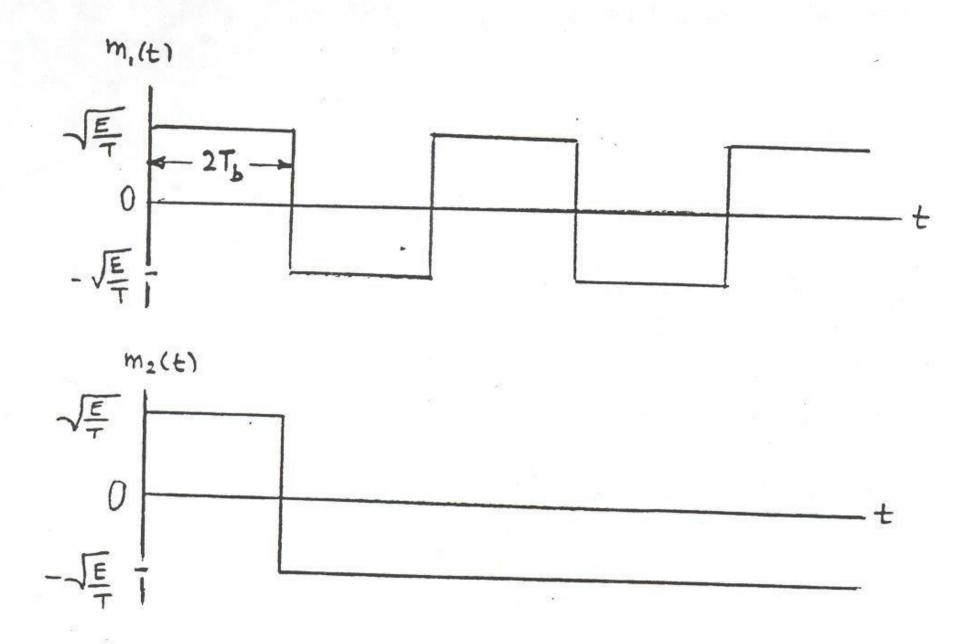
When  $\varphi = 0$ , this formula reduces to that for the standard PSK system equipped with perfect phase recovery. At the other extreme, when  $\varphi = \pm 90^{\circ}$ ,  $P_e$  attains its worst value of unity.

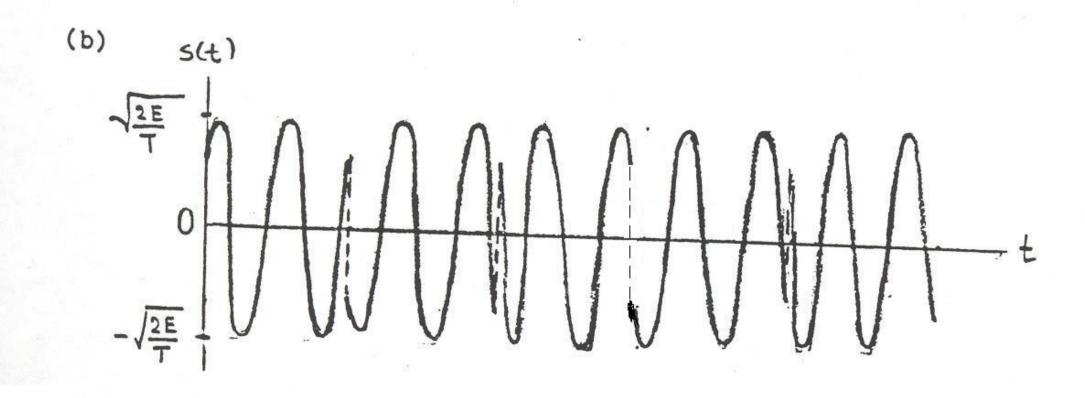
a) The QPSK wave can be expressed as

$$s(t) = m_1(t) \cos(2\pi f_c t) + m_2(t) \sin(2\pi f_c t)$$
.

Dividing the binary wave into dibits and finding  $m_1(t)$  and  $m_2(t)$  for each dibit:

dibit	11	00	10	00	10
m <sub>1</sub> (t)	√E/T	- √E/T	√E/T	- √E/T	√E/T
m <sub>2</sub> (t)	$\sqrt{E/T}$	- √E/T	$-\sqrt{E/T}$	$-\sqrt{E/T}$	- √E/T





The transmission bandwidth of 256-QAM signal is

$$B = \frac{2R_b}{\log_2 M}$$

where  $R_b$  is the bit rate given by  $1/T_b$  and M = 256. Thus

$$B_{256} = \frac{2(1/T_b)}{\log_2 256} = \frac{2}{8T_b} = \frac{1}{4T_b}$$

The transmission bandwidth of 64-QAM is

$$B_{64} = \frac{2(1/T_b)}{\log_2 64} = \frac{2}{6T_b} = \frac{1}{3T_b}$$

Hence, the bandwidth advantage of 256-QAM over 64-QAM is

$$-\frac{1}{4T_b} + \frac{1}{3T_b} = \frac{1}{12T_b}$$

The average energy of 256-QAM signal is

$$E_{256} = \frac{2(M-1)E_0}{3} = \frac{2(256-1)E_0}{3}$$
$$= 170E_0$$

where  $E_0$  is the energy of the signal with the lowest amplitude. For the 64-QAM signal, we have

$$E_{64} = \frac{2(63)}{3}E_0 = 42E_0$$

Therefore, the increase in average signal energy resulting from the use of 256-QAM over 64-QAM, expressed in dBs, is

$$10\log_{10} \left(\frac{170E_0}{42E_0}\right) \approx 10\log_{10}(4)$$
= 6 dB

The probability of symbol error for 16-QAM is given by

$$P_e = 2\left(1 - \frac{1}{\sqrt{M}}\right) \operatorname{erfc}\left(\sqrt{\frac{3E_{av}}{2(M-1)N_0}}\right)$$

Setting  $P_e = 10^{-3}$ , we get

$$10^{-3} = 2\left(1 - \frac{1}{4}\right) \operatorname{erfc}\left(\sqrt{\frac{3E_{av}}{30N_0}}\right)$$

Solving this equation for  $E_{av}/N_0$ ,

$$\frac{E_{\text{av}}}{N_0} = 58$$
$$= 17.6 \text{dB}$$

The probability of symbol error for 16-PSK is given by

$$P_e = \operatorname{erfc}\left(\sqrt{\frac{E}{N_0}}\sin(\pi/M)\right)$$

Setting  $P_e = 10^{-3}$ , we get

$$10^{-3} = \operatorname{erfc}\left(\sqrt{\frac{E}{N_0}}\sin(\pi/16)\right)$$

Solving this equation for  $E/N_0$ , we get

$$\frac{E}{N_0} = 142 = 21.5 \text{dB}$$

Hence, on the average, the 16-PSK demands 21.5 - 17.6 = 3.9 dB more symbol energy than the 16-QAM for  $P_e = 10^{-3}$ .

Thus the 16-QAM requires about 4 dB less in signal energy than the 16-PSK for a fixed  $N_0$  and  $P_e$  =  $10^{-3}$ , However, for this advantage of the 16-QAM over the 16-PSK to be realized, the channel must be linear.