

7.2:

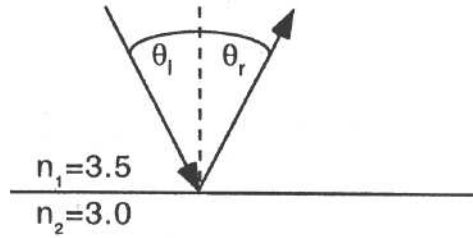


Figure 7.2. Reflection from dielectric interface

## a) TE polarization

$$r = 1 e^{j60^\circ}$$

$$\phi^{TE} = 2 \tan^{-1} \left( \frac{\gamma_{tx}}{k_{ix}} \right) = 60^\circ = \frac{\pi}{3} \quad (7.11)$$

$$\frac{\gamma_{tx}}{k_{ix}} = 0.577 = \frac{1}{\sqrt{3}}$$

$$\frac{\sqrt{\beta^2 - k_x^2}}{n_1 \cos \theta_i} = \frac{\sqrt{n_1^2 \sin^2 \theta_i - n_2^2}}{n_1 \cos \theta_i} = \frac{1}{\sqrt{3}}$$

$$n_1^2 \sin^2 \theta_i - n_2^2 = \frac{n_1^2}{3} \cos^2 \theta_i$$

$$n_1^2 - n_1^2 \cos^2 \theta_i - n_2^2 = \frac{n_1^2}{3} \cos^2 \theta_i$$

$$\frac{4}{3} n_1^2 \cos^2 \theta_i = n_1^2 - n_2^2$$

$$\cos \theta_i = \sqrt{\frac{3(n_1^2 - n_2^2)}{4n_1^2}}$$

$$\theta_i = \cos^{-1} \left( \sqrt{\frac{3(n_1^2 - n_2^2)}{4n_1^2}} \right)$$

$$\theta_i = \cos^{-1}(0.446)$$

$$\theta_i = 63.5^\circ$$

## b) TM polarization

$$\phi^{TM} = 2 \tan^{-1} \left( \frac{n_1^2 \gamma_{tx}}{n_2^2 k_{ix}} \right) = 60^\circ = \frac{\pi}{3} \quad (\text{p. 305})$$

$$\frac{n_1^2 \sqrt{n_1^2 \sin^2 \theta_i - n_2^2}}{n_2^2 n_1 \cos \theta_i} = \frac{1}{\sqrt{3}}$$

$$\theta_i = \cos^{-1} \left( \sqrt{\frac{n_1^2 - n_2^2}{n_1^2 + \frac{n_2^2}{3n_1^2}}} \right)$$

$$\theta_i = 61.7^\circ$$

7.4:

As described by Fig. 7.13, modes occur at resonances of the layer structure. The resonances can be found by using the transmission matrices of chapter 3 (see Table 3.3).

Assuming lossless material, the propagation matrices are given by

$$T_p = \begin{bmatrix} e^{j\beta_t L_t} & 0 \\ 0 & e^{-j\beta_t L_t} \end{bmatrix}$$

where

$$\beta_t = k_x = \sqrt{k_0^2 - k_z^2} = \frac{2\pi}{\lambda_0} \sqrt{n^2 - \bar{n}^2}$$

$L_t$  = distance of propagation (i.e. thickness of layer).

The reflection matrices are given by

$$T_{r_{12}} = \frac{1}{t_{12}} \begin{bmatrix} 1 & r_{12} \\ r_{12} & 1 \end{bmatrix}$$

$$r_{12} = \frac{n_1 - n_2}{n_1 + n_2}$$

$$t_{12} = \sqrt{1 - r_{12}^2}$$

The reflection values shown in Fig. 7.13,

$$r_A = r_B = \frac{T_{21}}{T_{11}}$$

$$T = T_{p0} T_{r_{01}} T_{p1} T_{r_{12}} T_{p2} T_{r_{21}} T_{p1} T_{r_{12}}$$

Modes of the waveguide structure occur for

$$r_A^2 = 1$$

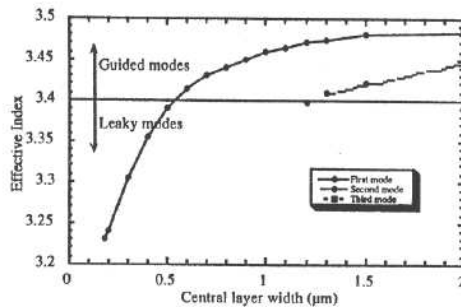


Figure 7.4. Effective index vs. central layer thickness

7.5:

For perfectly reflecting boundaries placed at  $30\mu\text{m}$ ,  $r = -1$ . From Table 1.1,  $n(\text{GaAs at } 1.0\mu\text{m}) = 3.52$  and  $n(\text{Al}_2\text{Ga}_8\text{As at } 1.0\mu\text{m}) = 3.39$ . This layer structure is shown in Fig. 7.11.

Solve for guided modes:

Guided modes can be solved for as done in Appendix 3. Using Eq. A3.12 and Fig. A3.2, we find that

$$V = \frac{2\pi}{1.0\mu\text{m}}(0.3\mu\text{m})\sqrt{3.52^2 - 3.39^2} = 1.79$$

So there is one guided mode.

$$b = 0.36$$

$$\bar{n} = \sqrt{3.39^2 + (0.36)(3.52^2 - 3.39^2)} = 3.437$$

$$\beta(m=1) = \frac{2\pi}{1.0\mu\text{m}}3.437 = 21.598$$

Solve for radiation modes:

$$k = \sqrt{k_x^2 + \beta^2}$$

$$k_x = \sqrt{k^2 - \beta^2} = \frac{2\pi}{\lambda}\sqrt{n^2 - \bar{n}^2}$$

In order to satisfy the characteristic equation (round trip gain = 1), we have

$$r_1 e^{k_1 x d_1} e^{k_2 x d_2} e^{k_3 x d_3} r_2 e^{k_1 x d_1} e^{k_2 x d_2} e^{k_3 x d_3} = 1$$

$$r_1 = r_2 = -1$$

$$d_1 = d_3 = 30\mu\text{m}$$

$$d_2 = 0.3\mu\text{m}$$

$$k_1 = k_3 = \frac{2\pi}{1.0\mu\text{m}}\sqrt{3.39^2 - \bar{n}^2}$$

$$k_2 = \frac{2\pi}{1.0\mu\text{m}}\sqrt{3.52^2 - \bar{n}^2}$$

The phase of the characteristic equation can be simplified to

$$m \frac{\lambda}{2} = (30\mu\text{m})\sqrt{3.39^2 - \bar{n}^2} + (0.3\mu\text{m})\sqrt{3.52^2 - \bar{n}^2} + (30\mu\text{m})\sqrt{3.39^2 - \bar{n}^2} \quad \text{for } m \geq 2$$

Solve for  $\beta$  using perturbation theory described in Chapter 6.

Simplify this expression by replacing the waveguide region with the same width of cladding material. This simplifies the expression for  $\beta$  significantly and allows us to write a closed form solution for  $\beta$ .

$$m \frac{\lambda}{2} \approx (60.3\mu\text{m}) \frac{\lambda}{2\pi} \sqrt{\left(\frac{2\pi n_1}{\lambda}\right)^2 - \beta^2}$$

$$\beta(m) \approx \sqrt{\left(\frac{2\pi n_1}{\lambda}\right)^2 - \left(\frac{m\pi}{60\mu\text{m}}\right)^2}$$

The perturbation due to the waveguide can then be added to the value of  $\beta$  for each mode:

$$\Delta\beta = \frac{\int \Delta\epsilon k_0^2 |U|^2 dA}{2\beta \int |U|^2 dA} \quad (6.9)$$

For odd numbered modes,

$$U(x) = A \cos(k_{x1m}x)$$

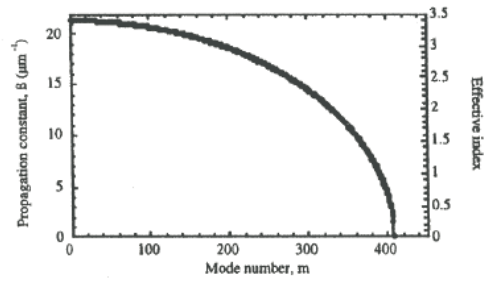
where A is a normalization coefficient and  $k_{x1m}$  is the value of the x component of the k vector for mode number m:  $k_{x1m} = \sqrt{k_1^2 - \beta_m^2}$

Similarly, for even numbered modes,

$$U(x) = A \sin(k_{x1m}x)$$

The index perturbation is  $\Delta\epsilon = 3.52^2 - 3.39^2 = 0.90$

$$k_0 = \frac{2\pi}{1.0\mu\text{m}} = 6.28\mu\text{m}^{-1}$$

Figure 7.5.  $\beta$  and  $\bar{n}$  vs. radiation mode number

Note: If better accuracy is desired, the values of  $\beta$  can be solved for numerically or graphically using the transcendental equations described by Eq. 7.26.