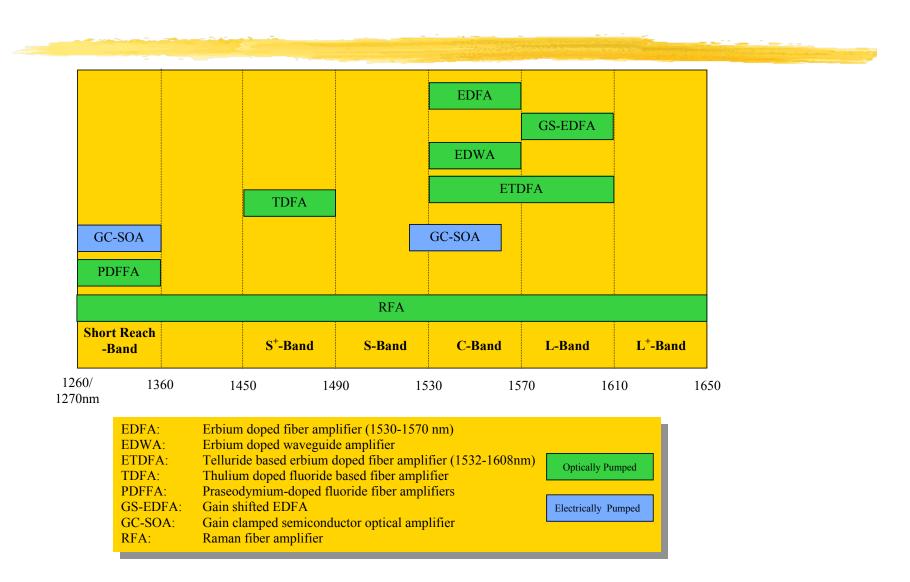


Lecture 8: Intro to Optical Amplifiers

1R Optical Regeneration

- ⇒ Analog amplification
- ⇒ Faithfully reproduces input signal with minimal distortion
- ⇒ Can be used as a linear repeater by periodically boosting optical power
- ⇒ Can be used in nonlinear region as a level clamping amplifier
- ⇒ Single amplifier can be used as a multichannel amplifier, ideally with minimal crosstalk and distortion

Waveband Operation



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OA Figures of Merit and Design Parameters

Figure of Merit	Design Parameter	Impact	
Unsaturated Gain (G ₀)	Pump Power	•	Sets the number of photons available for gain, increase in G_0 with increased pump power but
	Erbium Doped Fiber Length	•	reaches an asymptope Increased G ₀ with increased length for moderate pump power
Gain Flatness	Operation in Saturation	•	Higher F _n at shorter wavelengths Gain sensitivity to channel add/drop
	Erbium Doped Fiber Length	•	Optimal length for pump and signal powers
Noise Figure (F _n)	Co-Propagating pump	•	Lower F _n than counter-Propagating
	Counter-Propagating Pump	•	Higher F _n than co-Propagating
	Erbium Doped Fiber Length	•	F_n increases with increase in fiber length
	Pump Power	•	F _n decreases with increase in pump power
Maximum	Erbium Doped Fiber	•	
amplifier output	Length		
power (P _{out,max})	Pump Power	•	Pout,max increases with increased pump power

1R Optical Regeneration

 \Rightarrow 1R = Optical Analog amplification, without reshaping or retiming

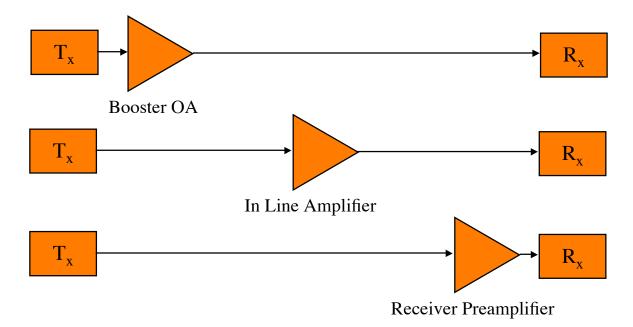
$$E_{out}(t) = G \cdot E_{in}(t) + n(t)$$
Amplifier optical Gain
Amplifier emitted
optical noise

- ⇒ Faithfully reproduces input signal with minimal distortion
- ⇒ Can be used as a linear repeater by periodically boosting optical power
- ⇒ Can be used in nonlinear region as a level clamping amplifier
- ⇒ Available solutions
 - ⇒ Erbium Doped Fiber Amplifiers (EDFA)
 - ⇒ Semiconductor Optical Amplifiers (SOA)

Optical Amplifiers

\Rightarrow Three classes

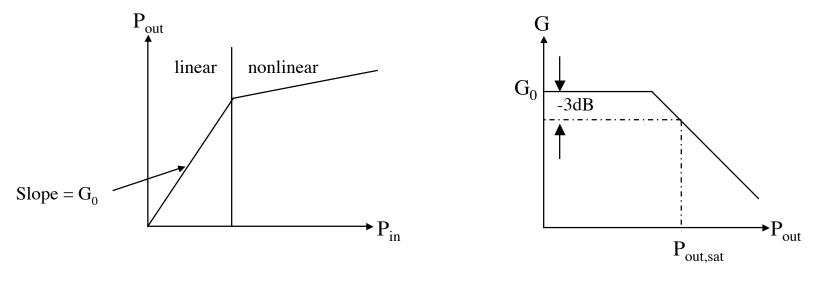
- \Rightarrow Booster (power) amplifiers: Boost power into transmission fiber, low NF, high P_{sat}.
- \Rightarrow In-line amplifiers: Periodically amplify signal due to fiber attenuation, high G, high P_{sat}.
- ⇒ Receiver preamplifiers: Boost power into receiver, low NF, high G.



Optical Amplifiers Gain Characteristics

Define: Unsaturated amplifier gain G_0 as the gain achieved at low signal levels and in the linear amplifier regime .

Define: Output saturation power as the output power needed to decrease the amplifier gain by a factor of 2.



Region I: Linear Region II: Nonlinear (Saturated)

$$G_0 = \frac{P_{out}}{P_{in}} \qquad \qquad G = G_0 \exp\left(-\frac{G-1}{G}\frac{P_{out}}{P_S}\right)$$

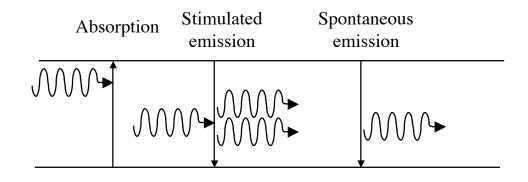
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Optical Amplifier Physics

\Rightarrow An atomic system with two energy levels can

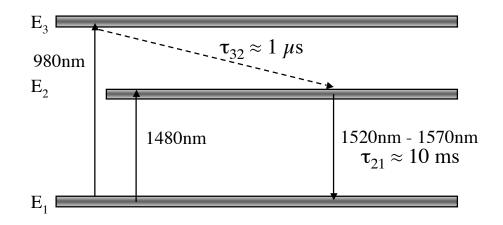
- ⇒ absorb light
- ⇒ amplify light
- \Rightarrow spontaneously emit light



Stimulated and spontaneous emission are achieved by pumping the amplifier electrically or optically

Erbium Doped Fiber Amplifier (EDFAs)

Energy levels for Er+ ions in silica glass



Two pumping options:

- <u>980 nm pump</u>: Complete population inversion -> Low noise figure
- <u>1480 nm pump</u>: Low population inversion -> high quantum efficiency in converting pump photons to signal photons

EDFA Gain Spectrum

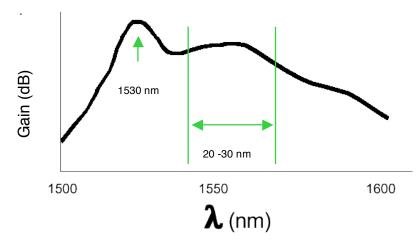
⇒ The gain coefficient for a single atomic transition in the unsaturated regime is given by the peak gain g_0 and the dipole relaxation time T_2 as

$$g(\omega) = \frac{g_0}{1 + (\omega - \omega_0)^2 T_2^2}$$

⇒ Averaging the gain over the distribution of atomic transition frequencies yields the effective gain

$$g_{eff}(\omega) = \int_{-\infty}^{\infty} g(\omega, \omega_0) f(\omega_0) d\omega_0$$

 \Rightarrow An illustration of the effective gain is given below. Note the presence of a gain peak around 1530nm and a semi-flat gain region with optical bandwidth 20-30nm.



EDFA Theory Basics

⇒ Using a simple two-level model for the EDFA assumes that ASE and excited-state absorption are negligible. Also, this model assumes the top excited energy level empties instantly (negligible excited state lifetime).

⇒The population densities of states E_1 and E_2 are given by N_1 and N_2 , with the cross section emission and absorption $\sigma_p^a, \sigma_p^e, \sigma_s^a, \sigma_s^e$ for the pump and signal photon flux ϕ_p and ϕ_s . T_1 is about 10ms for EDFAs.

$$\frac{\partial N_2}{\partial t} = \left(\sigma_p^a N_1 - \sigma_p^e N_2\right)\phi_p + \left(\sigma_s^a N_1 - \sigma_s^e N_2\right)\phi_s - \frac{N_2}{T_1}\frac{\delta y}{\delta x}$$
$$\frac{\partial N_1}{\partial t} = \left(\sigma_p^e N_2 - \sigma_p^a N_1\right)\phi_p + \left(\sigma_s^e N_2 - \sigma_s^a N_1\right)\phi_s + \frac{N_2}{T_1}$$

⇒ If we ignore ASE, the evolution of the pump and signal powers along the fiber in direction z can be approximated by taking into account the fiber loss at signal and pump wavelengths (α , α ')

$$\frac{\partial P_s}{\partial z} = \Gamma_s \left(\sigma_s^e N_2 - \sigma_s^a N_1 \right) P_s - \alpha P_s$$

$$\pm \frac{\partial P_p}{\partial z} = \Gamma_p \left(\sigma_p^e N_2 - \sigma_p^a N_1 \right) P_p - \alpha' P_p$$

EDFA Theory Basics

⇒ For short amplifiers (10-20m), optical loss can be ignored ($\alpha = \alpha' = 0$). Let $N_1 + N_2 = N_{total}$, and a_d be the cross-sectional area of the doped portion of the fiber core. The steady state solution for the rate equations reduces to

$$N_{2}(z) = -\frac{T_{1}}{a_{d}hv_{s}}\frac{\delta P_{s}}{\delta z} \pm \frac{T_{1}}{a_{d}hv_{p}}\frac{\delta P_{p}}{\delta z}$$
$$a_{d} = \Gamma_{s}a_{s} = \Gamma_{p}a_{p}$$

 \Rightarrow Substituting this equation into the power evolution equations and integrating over the length of fiber, the gain can be computed by taking the ratio of output to input power

$$G = \Gamma_s \exp\left[\int_0^L \sigma_s^e N_2 - \sigma_s^a N_1 dz\right]$$

EDFA Basics

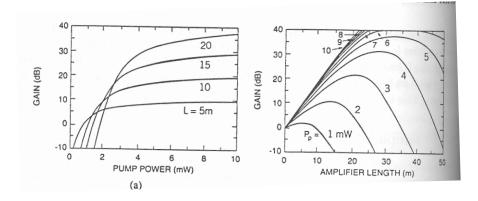
 \Rightarrow From the figure below we observe that

 \Rightarrow For a given amplifier length the gain initially increases with pump power then saturates

 \Rightarrow For a given pump power, the amplifier gain becomes maximum at optimum

L, then rolls off sharply as the pump photons have all been absorbed.

 \Rightarrow Both L and P_p must be optimized for a particular amplifier design.



EDFA pumps

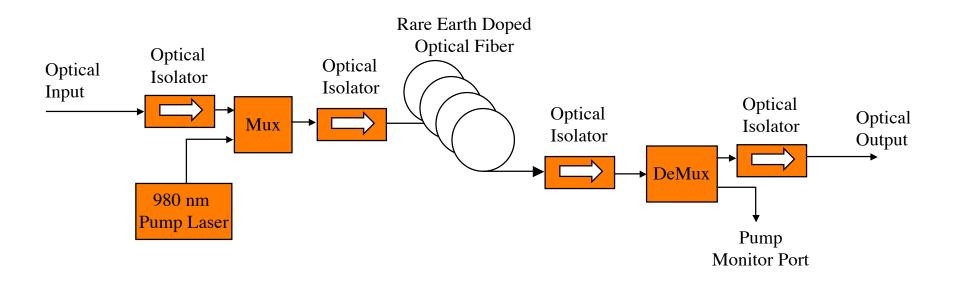
- ⇒ 1480 nm pumping: it was the choice for most of the first commercial solutions
 - ⇒ Mainly due to the fact that 1480 nm laser were more resilient and commercially available at high output power (which is usually in the order of 200-400 mW)
 - ⇒ Generally less expensive
 - ⇒ From a pure transmission point of view, they have low performance in terms of noise figure (see later)
- \Rightarrow 980 nm pumping:
 - ⇒ Today laser technology has reach a high reliability even at 980 nm
 - ⇒ Most current commercial EDFAs use this solution, sometimes together with 1480 nm

Typical Pump Source Characteristics

Performance parameter/wavelength	980 nm	1480 nm
Minimum noise figure	<4 dB	5.5 dB
Optical conversion power efficiency	35%	50%
Diode laser quantum efficiency	0.92 W/A @ 240 mW	0.36 W/A @ 200 mW
Module wall-plug efficiency	39% W/W	13% W/W
1999 rated module power	200 mW	180 mW
State-of-the-art module reliability	110 FIT	65 FIT
Mean time to failure	>2×10 ⁶ hours @ 150 mW	>5×10 ⁶ hours @ 120 mW
-3dB Er absorption band in silica	976 to 984 nm	> ~1450 nm

Rare Earth Fiber Amplifiers

Rare Earth Doped Fiber Amplifier: Single pump, single stage geometry



EDFA Characteristics

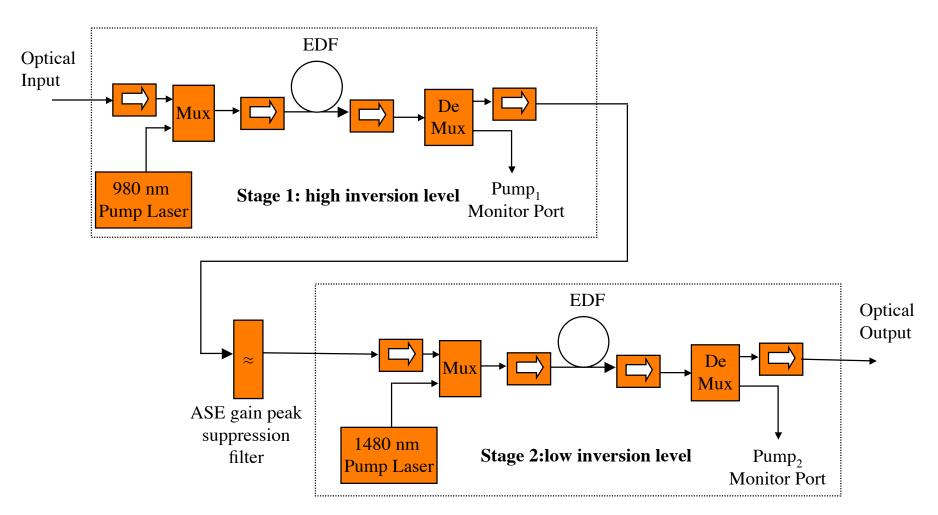
\Rightarrow Gain:

- \Rightarrow Higher gain requires high
- \Rightarrow High Output Power:
 - \Rightarrow Requires high P_{out sat} which requires high optical pump power and high inversion

\Rightarrow Gain Flatness

- \Rightarrow Is a function of inversion level.
- \Rightarrow Typically 40%-60% inversion leads to broadest gain with lowest ripple
- ⇒ Gain Bandwidth:
 - \Rightarrow Can be enhanced using optical filtering and composite gain media
- \Rightarrow Noise Figure:
 - \Rightarrow High population inversion level
- ⇒ Transient Behavior:
 - \Rightarrow Can be suppressed using optical gain clamping or dynamic gain control feedback

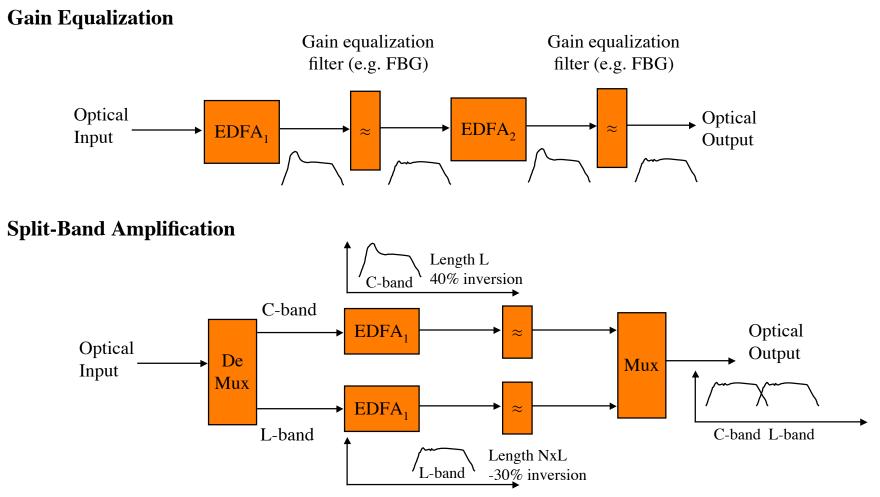
Two-Stage EDFA Optical Amplifier



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Wideband EDFAs



ASE noise in EDFA

 \Rightarrow The output ASE noise is:

$$P_{ASE}^{out} \cong 2n_{sp}h\nu(G-1)\Delta B$$

 \Rightarrow where:

- \Rightarrow $n_{sp} = (N_2 N_1)/N_2$ is the spontaneous emission factor, mainly dependent on the degree of inversion
- $\Rightarrow h$ is the Plank constant
- $\Rightarrow v$ is the central optical frequency
- \Rightarrow G is the EDFA gain
- $\Rightarrow \Delta B$ is the bandwidth over which the noise is measured
- \Rightarrow The <u>noise figure</u> of the EDFA is defined as: $F = 2n_{sn}$
- \Rightarrow The optimal value for an EDFA is *F*=3 dB
 - \Rightarrow Typical values are from 4 to 5 dB

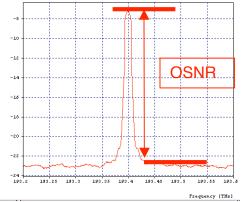
ASE noise in EDFA -II

 \Rightarrow The output ASE noise on a 0.1 nm bandwidth is approx. given by:

$$P_{ASE}^{out} \cong -58dBm + F_{EDFA} + G_{EDFA}$$

- ⇒ The ASE noise is one of the factor that sets the ultimate limits of optically amplified systems
 - ⇒ The optical signal-to-noise ratio (OSNR) cannot go below a given level to have acceptable BER at the receiver
 - \Rightarrow Given an input signal power P_{in}

$$OSNR\Big|_{dB} \cong P_{signal}^{in} + 58dBm - F_{EDFA}$$



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EDFA features

- ⇒ In a WDM environment, the crosstalk among channels generated by EDFA is very low
 - \Rightarrow This is one of the main reason for the EDFA success
 - \Rightarrow Physically, this is related to the (slow, ms) time constant of the saturation process in EDFA
 - \Rightarrow A comb of tens of channels can be amplified by a single EDFA with negligible crosstalk
- Still, in some important situation, transient effects in EDFA may be \Rightarrow relevant

