

# Partial Feedback Linearization <sup>"(PFL)"</sup> (Spong 94)

• For an UNDERACTUATED system, where

$$m < n$$

# actuated DOF  $\uparrow$   $\uparrow$  # DOF, total  
 ("degrees of freedom")

- There remain  $l = n - m$  "passive joints".

Linearize the non-linear EOM at each dt, and use a feedback law to control a subset of joints.

• IF we have a GOOD MODEL of the dynamics,

- and if  $m \geq l$  (more actuated than passive joints)

- and if we can guarantee we can calculate any required matrix inverse or pseudo-inverse ("STRONG INERTIAL COUPLING"),

• THEN,

→ We can "shuffle around" the terms in the equations of motion to solve DIRECTLY for ANY  $m$  of  $n$  DOF'S - not just the so-called "active" joints.

## General Case :

• Nonlinear equations of motion (EOM) may be written as:

$$\begin{array}{l}
 1. \quad \underbrace{M_{11}}_{(l \times l)} \ddot{q}_1 + \underbrace{M_{12}}_{(l \times m)} \ddot{q}_2 + \underbrace{h_1}_{(l \times 1)} + \underbrace{\phi_1}_{(l \times 1)} = \underbrace{0}_{(l \times 1)} \\
 \hline
 2. \quad \underbrace{M_{21}}_{(m \times l)} \ddot{q}_1 + \underbrace{M_{22}}_{(m \times m)} \ddot{q}_2 + \underbrace{h_2}_{(m \times 1)} + \underbrace{\phi_2}_{(m \times 1)} = \underbrace{T}_{(m \times 1)}
 \end{array}$$

$l$  equations for  $l$  "passive" joints

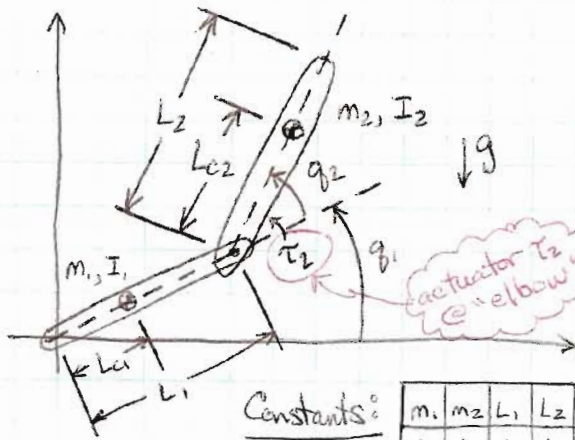
$m$  equations for  $m$  "active" joints

• To control some set,  $m$  of the  $n$  DOF, of joints :

a) Make all matrices have constraints at each dt.  
 b) Move  $m$  joints toward  $m$  desired joint pos.  
 c) Shuffle eqs to solve for  $T$ .

- "Linearize" these non-linear EOM at each "dt" in time (as controller runs).  
 - Plug in current  $q_i$  and  $\dot{q}_i$  values, for all  $i$ .
- Come up with a control law (e.g., simple "PD" proportional plus derivative control) that defines  $m$  of  $n$  desired accelerations:  
 $\ddot{q}_i^{des} \leftarrow$  (for  $m$  DOF'S)  $\leftarrow$  pick  $\ddot{q}_i^{des}$  to get toward desired  $q_i(t)$ ...
- Use matrix algebra to solve for  $m$  elements in  $T$  ("torques") to achieve  $m$  values,  $\ddot{q}_i = \ddot{q}_i^{des}$ .  $\leftarrow$  "Shuffle" EOM, to solve for  $T!$  (P.1)

# ACROBOT Example :



Define some terms:

$$\begin{aligned}
 m_{11} &= m_1 L_{c1}^2 + m_2 (L_1^2 + L_{c2}^2 + 2L_1 L_{c2} \cos(q_2)) + I_1 + I_2 \\
 m_{22} &= m_2 L_{c2}^2 + I_2 \\
 m_{12} &= m_{21} = m_2 (L_{c2}^2 + L_1 L_{c2} \cos(q_2)) + I_2 \\
 h_1 &= -m_2 L_1 L_{c2} \sin(q_2) \dot{q}_2^2 - 2m_2 L_1 L_{c2} \sin(q_2) \dot{q}_2 \dot{q}_1 \\
 h_2 &= m_2 L_1 L_{c2} \sin(q_2) \dot{q}_1^2 \\
 \phi_1 &= (m_1 L_{c1} + m_2 L_1) g \cos(q_1) + m_2 L_{c2} g \cos(q_1 + q_2) \\
 \phi_2 &= m_2 L_{c2} g \cos(q_1 + q_2)
 \end{aligned}$$

Constants:

$m_1$	$m_2$	$L_1$	$L_2$	$L_{c1}$	$L_{c2}$	$I_1$	$I_2$	$g$
1	1	1	1	.5	.5	.2	1.0	9.8

Collocated :  $\tau_2$  set by choosing  $\ddot{q}_2$       Non-collocated :  $\tau_2$  set by choosing  $\ddot{q}_1$ .

collocated: plug in for  $\ddot{q}_1$

$$\begin{aligned}
 1. \quad m_{11} \ddot{q}_1 + m_{12} \ddot{q}_2 + h_1 + \phi_1 &= 0 \\
 2. \quad m_{21} \ddot{q}_1 + m_{22} \ddot{q}_2 + h_2 + \phi_2 &= \tau_2
 \end{aligned}$$

non-collocated: plug in for  $\ddot{q}_2$

A. Rewrite 1. w/  $\ddot{q}_1$  on lefthand side:

$$\ddot{q}_1 = \frac{-1}{m_{11}} (m_{12} \ddot{q}_2 + h_1 + \phi_1)$$

B. Plug this in for  $\ddot{q}_1$  in 2.:

$$m_{21} \left[ \frac{-1}{m_{11}} (m_{12} \ddot{q}_2 + h_1 + \phi_1) \right] + m_{22} \ddot{q}_2 + h_2 + \phi_2 = \tau_2$$

C. Drive  $q_2$  toward some desired  $q_2^{des}$ .

e.g.,  $q_2^{des} = \frac{2\alpha}{\pi} \tan^{-1}(\dot{q}_1)$  (say  $\alpha = \frac{\pi}{2}$ )

D. Control laws (PD) sets  $\ddot{q}_2^{des}$  to move  $q_2$  toward  $q_2^{des}$ :

$$\ddot{q}_2 = v_2 = K_p (q_2^{des} - q_2) - K_D \dot{q}_2 \tag{Eq. 55}$$

E. Plug  $\ddot{q}_2$  from D. into B. to get  $\tau_2$ !!

A. Rewrite 1. w/  $\ddot{q}_2$  on LHS:

$$\ddot{q}_2 = \frac{-1}{m_{12}} (m_{11} \ddot{q}_1 + h_1 + \phi_1)$$

B. Plug this in for  $\ddot{q}_2$  in 2.:

$$m_{21} \ddot{q}_1 + m_{22} \left[ \frac{-1}{m_{12}} (m_{11} \ddot{q}_1 + h_1 + \phi_1) \right] + h_2 + \phi_2 = \tau_2$$

C. Drive  $q_1$  toward some desired  $q_1^{des}$ .

$q_1^{des} = \frac{\pi}{2}$  (1st link to be "upright")

D. Control law (PD) picks a value for  $\ddot{q}_1^{des}$  to drive  $q_1$  toward  $q_1^{des}$ :

$$\ddot{q}_1 = v_1 = K_p (q_1^{des} - q_1) - K_D \dot{q}_1 \tag{Eq. 56}$$

E. Plug  $\ddot{q}_1$  from D. into B. → get  $\tau_2$ !!

General Case ( $m > 1, l > 1$  ... MATRIX equations!)

Collocated

Non-collocated

Both start with the same EOM in matrix form

if collocated

if non-collocated

$$1. M_{11}\ddot{q}_1 + M_{12}\ddot{q}_2 + h_1 + \phi_1 = 0$$

$$2. M_{21}\ddot{q}_1 + M_{22}\ddot{q}_2 + h_2 + \phi_2 = T$$

plug in:

$$\ddot{q}_1 = -M_{11}^{-1}(M_{12}\ddot{q}_2 + h_1 + \phi_1)$$

plug in:

$$\ddot{q}_2 = -M_{12}^\dagger(M_{11}\ddot{q}_1 + h_1 + \phi_1)$$

Where  $M_{12}^\dagger$  is the PSEUDO-INVERSE of the  $(l \times m)$  matrix  $M_{12}$ :

$$M_{12}^\dagger = M_{12}^T (M_{12} M_{12}^T)^{-1}$$

A. Then 2. becomes:

$$-M_{21}M_{11}^{-1}(M_{12}\ddot{q}_2 + h_1 + \phi_1) + M_{22}\ddot{q}_2 + h_2 + \phi_2 = T$$

A. Then 2. becomes:

$$M_{21}\ddot{q}_1 - M_{21}M_{12}^\dagger(M_{11}\ddot{q}_1 + h_1 + \phi_1) + h_2 + \phi_2 = T$$

B. Collecting terms: (collocated case) (Eq. 11)

$$\underbrace{(M_{22} - M_{21}M_{11}^{-1}M_{12})}_{\bar{M}_{22}}\ddot{q}_2 + \underbrace{(h_2 - M_{21}M_{11}^{-1}h_1)}_{\bar{h}_2} + \underbrace{(\phi_2 - M_{21}M_{11}^{-1}\phi_1)}_{\bar{\phi}_2} = T$$

(Eq. 13)  $\ddot{q}_2 = V_2$

(Eq. 33)  $\ddot{q}_1 = V_1$

B. Collecting terms: (non-collocated case) (Eq. 35)

$$\underbrace{(M_{21} - M_{22}M_{12}^\dagger M_{11})}_{\tilde{M}_{21}}\ddot{q}_1 + \underbrace{(h_2 - M_{22}M_{12}^\dagger h_1)}_{\tilde{h}_2} + \underbrace{(\phi_2 - M_{22}M_{12}^\dagger \phi_1)}_{\tilde{\phi}_2} = T$$

C. Write a control law to set  $V_2$ .

C. Write a control law to set  $V_1$ .

(p. 3)