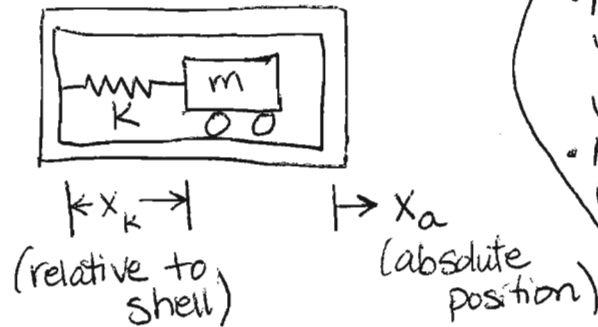


Sensors

- Important to consider both
freq. response & noise characteristics.

Accelerometer (e.g. MEMS)



- Assume x_a is the "system input" we wish to measure.
- Assume sensor output is proportional to a gap (measured capacitively).

Force balance (Newton's 2nd law...)

$$\sum F = m a$$

$$-K x_k = m (\ddot{x}_a + \ddot{x}_k)$$

relative position

total acceleration (absolute + relative)

$$-m \ddot{x}_k - K x_k = m \ddot{x}_a$$

$$-(ms^2 + K) \cdot X_k(s) = (ms^2) \cdot X_a(s)$$

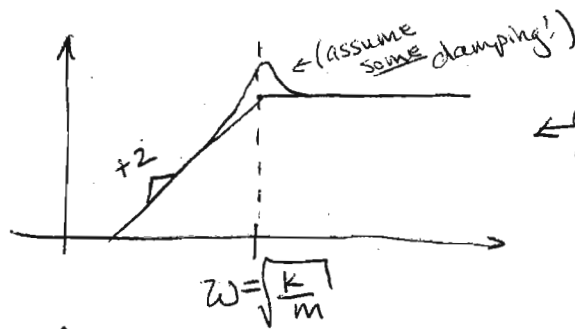
$$\frac{X_k(s)}{X_a(s)} = \frac{-(ms^2)}{(ms^2 + K)}$$

$$V_{\text{sense}} = A_{\text{sense}} \cdot x_k$$

← Sensor output voltage is proportional to relative displacement, x_k

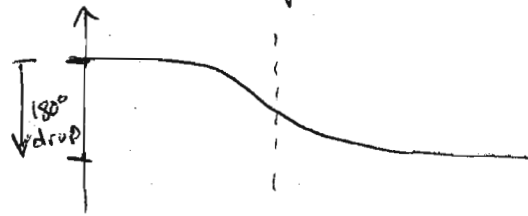
$$\text{So: } \frac{V_{\text{sense}}}{X_a} = A_{\text{sense}} \cdot \frac{x_k}{X_a} = -A \frac{ms^2}{(ms^2 + K)}$$

$$\left| \frac{V_{sense}(s)}{X_a(s)} \right|$$



$$-A \frac{ms^2}{(ms^2+K)}$$

$$\angle \left(\frac{V_s}{X_a} \right)$$



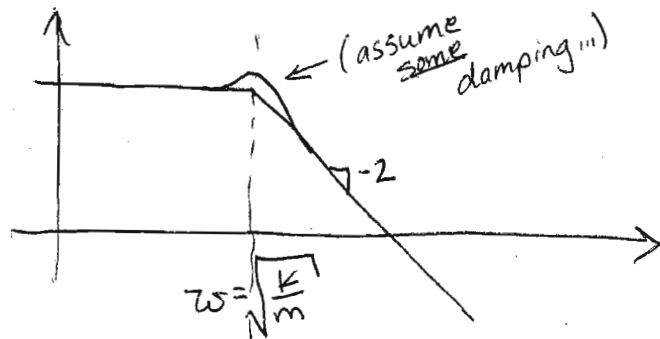
* So, at "high frequencies", we have a nice, flat measurement of POSITION of the outer shell of the accelerometer.

But this is called an "accelerometer", right?

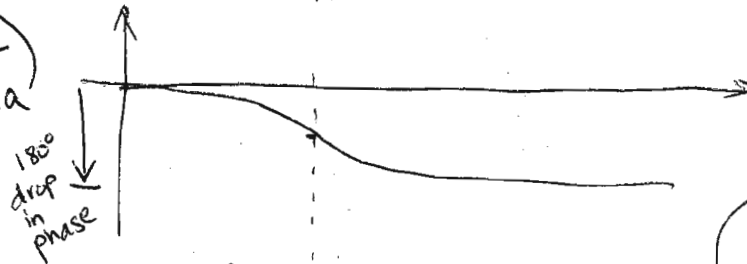
What is the relationship between V_{sense} & \ddot{X}_a ??

$$\frac{V_s(s)}{\ddot{X}_a(s)} = \frac{V_s(s)}{s^2 X_a(s)} = -A \frac{ms^2}{s^2(ms^2+K)} = -A \frac{m}{ms^2+K}$$

$$\left| \frac{V_s}{s^2 X_a} \right|$$



$$\angle \left(\frac{V_s}{s^2 X_a} \right)$$

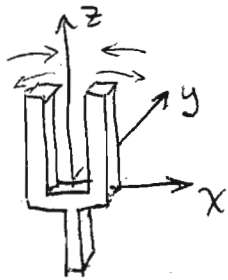


So, at low frequencies, we have a good measurement of ACCELERATION.

Note - I am intentionally being "sloppy" in labeling "phase", b/c sense constant "A" can be > 0 or < 0 ...

Gyro - A gyroscope gives an output proportional to angular velocity. Inertial measurement units (IMUs) typically do something akin to integration to turn this into an estimate of angular position.

(Coriolis effect... $a_c = 2(\Omega \times v)$)

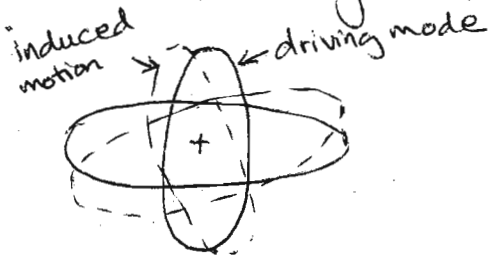


"tuning fork" version

$$F_c = m \cdot a_c$$

← Drive $\pm x$ (local coordinate).
Rotation about \vec{z} is sensed, b/c out-of-plane motion (in \vec{y}) is induced.

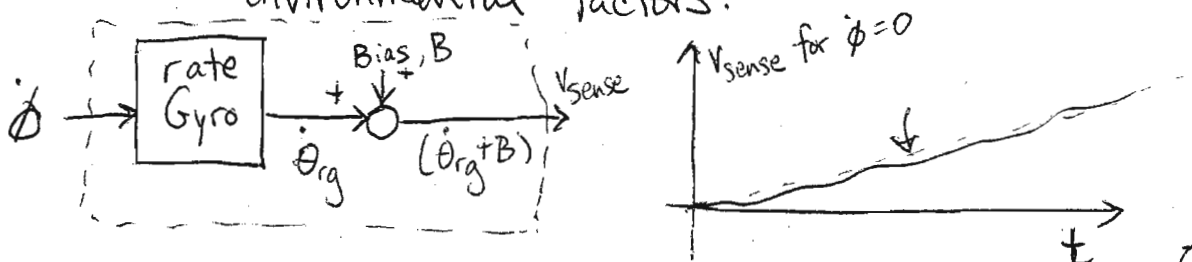
Alternate form: Wineglass mode.



Mode that you hear when you rub the rim of a wineglass.

Drift

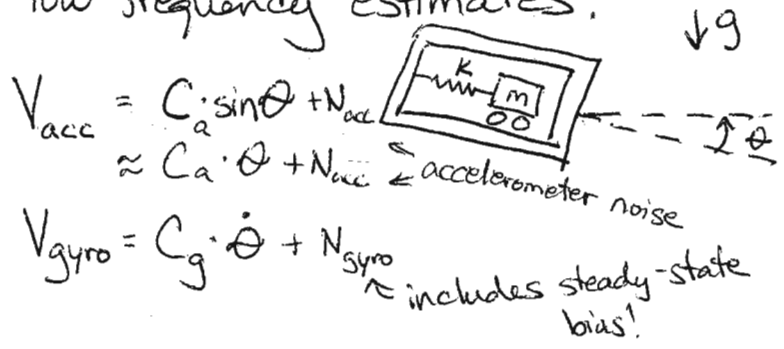
- Gyro sensor will have noise at all frequencies, but the most problematic noise is low frequency, i.e., $\omega \approx 0$. (Steady-state offset.)
- Unfortunately, this offset is (generally) sensitive to temperature and other environmental factors.



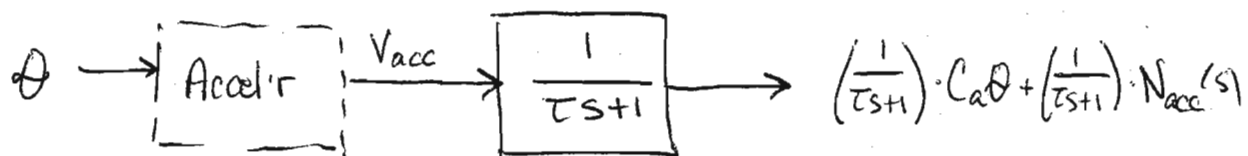
Sensor Fusion: Complementary Filters

Problem - One sensor may work ^{well} over a particular range of frequencies, while another works well over a different range. Can we blend these?

Example - Gyro has drift, so it performs poorly at low frequency estimates of θ (position, via integration),
 - Accelerometer can work as a "filt sensor", but it is only effective for low frequency estimates.



• So, let's use a low-pass filter on V_{acc} :



• What is a good choice of filter for V_{gyro} ?

(For now, assume $C_a=1$, $C_g=1$...)

$$\underbrace{\left(\frac{1}{\tau s+1}\right)}_{\text{Accelerometer filter}} \cdot \theta_{(a)} + \underbrace{(\quad ? \quad)}_{\text{Gyro filter}} \cdot \dot{\theta}_{(g)} = \theta$$

$$\left(\frac{1}{\tau s+1}\right) \cdot \theta + (\quad ? \quad) \cdot s \cdot \theta = \theta \cdot \underbrace{\left(\frac{\tau s+1}{\tau s+1}\right)}_{\text{just "1"}}$$

Answer:

$$(\quad ? \quad) \cdot s \cdot \theta = \left[\frac{\tau s+1}{\tau s+1} - \frac{1}{\tau s+1} \right] \cdot \theta$$

$$(\quad ? \quad) \cdot s = \frac{\tau s}{\tau s+1}$$

$$\boxed{? = \frac{\tau}{\tau s+1}}$$

Higher-order filters work, too:

$$\left(\frac{3s^2+3s+1}{s^3+3s^2+3s+1}\right) \cdot \theta_a + \left(\frac{s^2}{s^3+3s^2+3s+1}\right) \cdot s \cdot \theta_g = \theta \cdot 1$$

• Set filter to attenuate noise of each sensor.

→ Next class: Observers

Kalman Filters

Extended Kalman Filters (EKF)