

Final Exam, ECE 137A

Wednesday March 18, 2015 7:30-10:30 PM

Name: Solution a

Closed Book Exam: Class Crib-Sheet and 3 pages (6 surfaces) of student notes permitted
 Do not open this exam until instructed to do so. Use any and all reasonable approximations (5% accuracy), *after stating & justifying them.*

Show your work:

Full credit will not be given for correct answers if supporting work is missing.

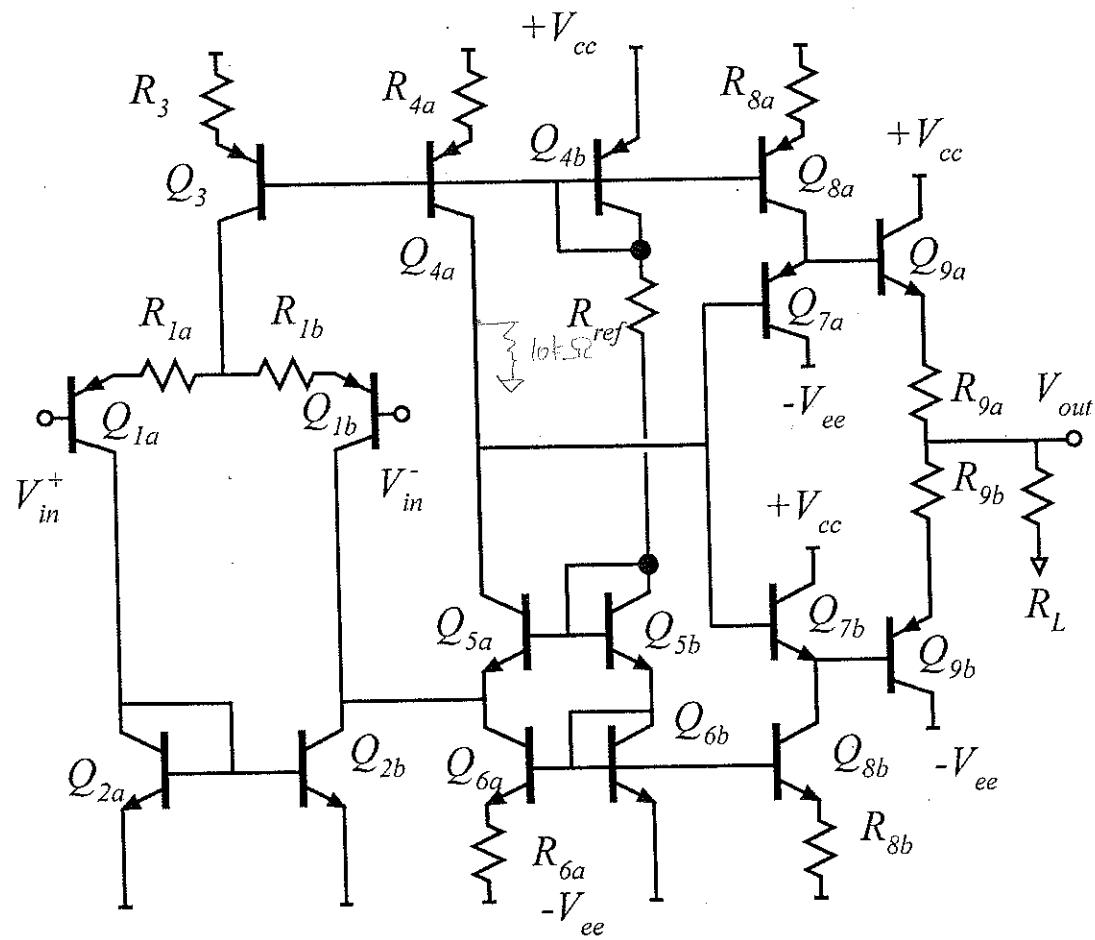
Good luck

Time function	LaPlace Transform
$\delta(t)$ impulse	1
$U(t)$ unit step-function	$1/s$
$e^{-\alpha t}U(t)$	$\frac{1}{s + \alpha}$
$e^{-\alpha t} \cos(\omega_d t)U(t)$	$\frac{s + \alpha}{(s + \alpha)^2 + \omega_d^2}$
$e^{-\alpha t} \sin(\omega_d t)U(t)$	$\frac{\omega_d}{(s + \alpha)^2 + \omega_d^2}$

Part	Points Received	Points Possible	Part	Points Received	Points Possible
1a		5	2c		15
1b		6	2d		10
1c		4	3a		7
1d		10	3b		8
1e		10	3c		7
2a		10	3d		8
2b		10			
total		100			

Problem 1, 35 points

This is an NOT an Op-Amp: Analyze under the assumption that the differential and common mode input voltages are at zero volts



All the transistors have the same (matched) I_S , have $\beta = 100$, and $V_A = \infty$ Volts.

$V_{CE(sat)} = 0.5V$. V_{be} is roughly 0.7 V, but use $V_{be} = (kT/q) \ln(I_E/I_S)$ when necessary and appropriate. The supplies are +2 Volts and -2 Volts.

Q1ab,2ab,4a,5a,6a are to be biased at $250 \mu\text{A}$ collector current.

Q4B,5B,6B are to be biased at 1 mA collector current.

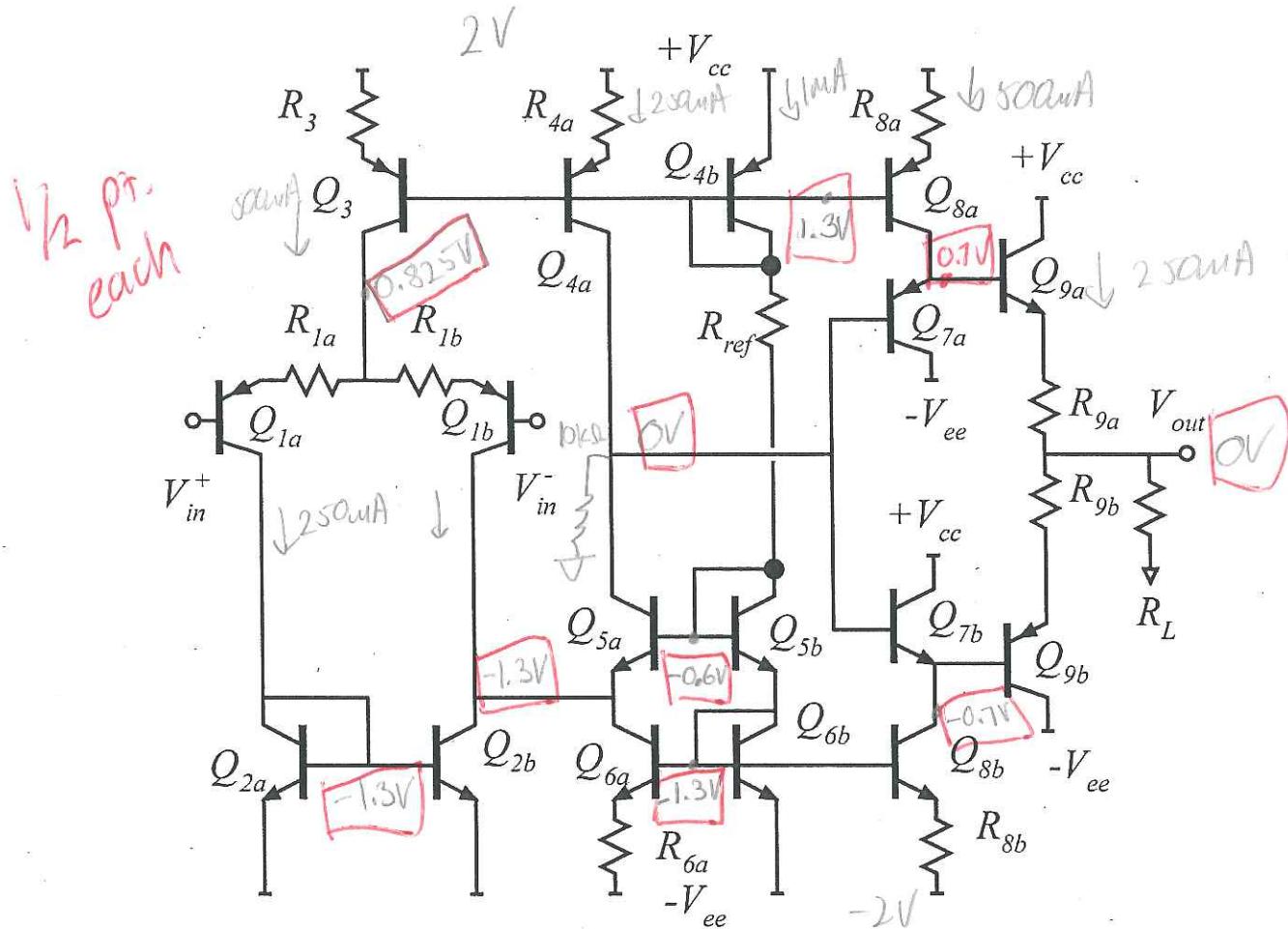
Q8ab are to be biased at $500 \mu\text{A}$ collector current.

Q9ab are to be biased at $250 \mu\text{A}$ collector current.

$$R_L = 250\Omega \quad R1a=R1b=500 \text{ Ohms}$$

Part a, 5 points

DC bias---to simplify ,assume $\beta = \infty$ for the DC analysis only.



On the circuit diagram above, label the DC voltages at ALL nodes, the DC currents through ALL resistors, and the DC collector currents of all transistors.

$$\textcircled{1} [V_{be6b} - V_{be6a} = \frac{kT}{q} \ln \left[\frac{1\text{mA}}{250\mu\text{A}} \right] = 36\text{mV} \rightarrow R_{6a} = \frac{36\text{mV}}{250\mu\text{A}} = 144\Omega]$$

$$\textcircled{1} [V_{be6b} - V_{be8b} = \frac{kT}{q} \ln \left[\frac{1\text{mA}}{500\mu\text{A}} \right] = 18\text{mV} \rightarrow R_{8b} = \frac{18\text{mV}}{500\mu\text{A}} = 36\Omega]$$

$$\textcircled{1} [V_{be7b} - V_{be9b} = \frac{kT}{q} \ln \left[\frac{500\mu\text{A}}{250\mu\text{A}} \right] = 18\text{mV} \rightarrow R_{ab} = \frac{18\text{mV}}{250\mu\text{A}} = 72\Omega]$$

by same arguments, $R_{6a} = 36\Omega$, $R_{9a} = 72\Omega$

$$\textcircled{1} \quad V_{be4b} - V_{be4a} = \frac{kT}{q} \ln \left[\frac{I_{mA}}{250\mu A} \right] = 36\text{mV} \rightarrow R_{4a} = \frac{36\text{mV}}{250\mu A} = \boxed{144\Omega}$$

$$\textcircled{1} \quad V_{be4b} - V_{be3} = \frac{kT}{q} \ln \left[\frac{I_{mA}}{500\mu A} \right] = 18\text{mV} \rightarrow R_3 = \frac{18\text{mV}}{500\mu A} = \boxed{36\Omega}$$

$$\textcircled{1} \quad R_{ref} = \frac{1.3V - (-0.6V)}{1\text{mA}} = \boxed{1900\Omega}$$

Part b, 6 points

DC bias:

Find the value of all resistors.

$$R3 = \underline{26\Omega} \quad R4ba = \underline{44\Omega} \quad R6a = \underline{44\Omega} \quad Rref = \underline{1.4k\Omega} \quad R8a = \underline{36\Omega} \quad R8b = \underline{36\Omega}$$
$$R9a = \underline{77\Omega} \quad R9b = \underline{77\Omega}$$

Part c, 4 points

Find the transconductance of the transistors below:

$$gm_{1a} = \underline{9.61MS} \quad gm_{1b} = \underline{9.61MS} \quad gm_{5a} = \underline{9.61MS} \quad gm_{7a} = \underline{19.2MS}$$

$$gm_{7b} = \underline{19.2MS} \quad gm_{9a} = \underline{9.61MS} \quad gm_{9b} = \underline{9.61MS}$$

① $\boxed{Q_{1a,b}: I_c = 250\mu A, \frac{1}{gm} = 104\Omega \rightarrow 9.61MS}$

① $\boxed{Q_{5a}: I_c = 250\mu A, \frac{1}{gm} = 104\Omega \rightarrow 9.61MS}$

① $\boxed{Q_{7a,b}: I_c = 500\mu A, \frac{1}{gm} = 52\Omega \rightarrow 19.23MS}$

① $\boxed{Q_{9a,b}: I_c = 250\mu A, \frac{1}{gm} = 104\Omega \rightarrow 9.61MS}$

Part d, 10 points.

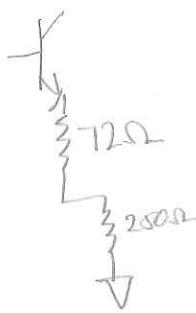
Find the following, using the actual value of β , i.e. $\beta=100$

	Voltage Gain	Input impedance
Transistor combination Q2a,2b,1a,1b	0.172	70.8k Ω
Q5a	0.567	104.52 Ω
Q7a or 7b	1.0	4.26M Ω
Q9a or 9b	0.587	42.6k Ω
Overall differential Vout/Vin	0.66	70.8k Ω

1 pt.
each

* Push-pull \rightarrow analyze with one off and one on.

Q9a:



Voltage Divider gain:

$$\frac{250}{250+72} = 0.776$$

Emitter-Follower gain:

$$R_{L,q} = 250\Omega + 72\Omega = 322\Omega$$

$$A_v = \frac{322\Omega}{322\Omega + 109\Omega} = 0.756$$

$$\text{Overall: } (0.776)(0.756) = 0.587$$

$$R_{iqa} = \beta(104\Omega + 72\Omega + 250\Omega) = 42.6k\Omega$$

Q_{7b}: $R_{eqb} = R_{inab} = 42.6\text{k}\Omega$ (neglect $R_{h,ce,8b}$)

$$\frac{1}{g_m7b} = 52\Omega$$

$$Av = \frac{R_{eq}}{R_{eq} + \frac{1}{g_m}} = 1.0$$

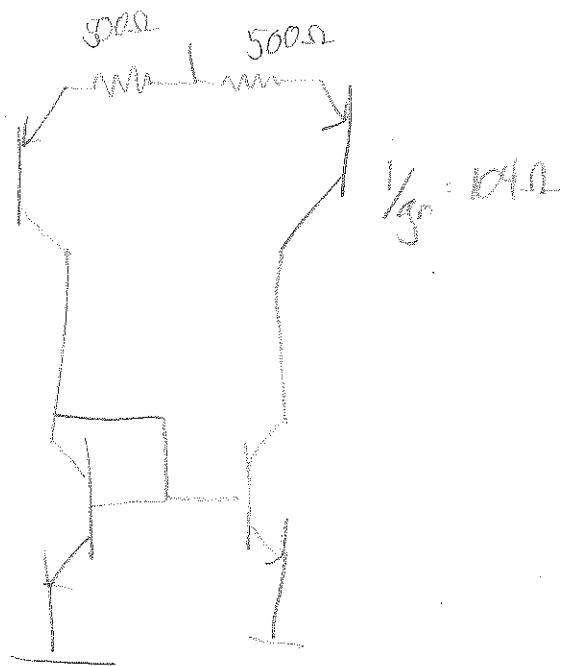
$$R_{in7b} = \beta [42.6\text{k}\Omega] = 4.26\text{M}\Omega$$

Q_{5a}: $R_{eq5a} = 10\text{k}\Omega \parallel R_{in7a} \approx 10\text{k}\Omega$

Impedance presented to base of Q_{5a} is that of diodes Q_{5b} & Q_{6b}, each 26Ω or a total of $52\Omega = R_{base}$

$$R_{in5a} = \frac{1}{g_m5a} + \frac{R_{base5a}}{\beta} = 104\Omega + \frac{52\Omega}{100} = 104.52\Omega$$

$$Av_{5a} = \frac{10\text{k}\Omega}{104.52\Omega} = 95.6755$$



$$\text{Overall transconductance} = \frac{I}{g_{m1a} + R_{in}} = (604\Omega)^{-1}$$

$$\text{gain} = \frac{104\Omega}{604\Omega} = [0.172]$$

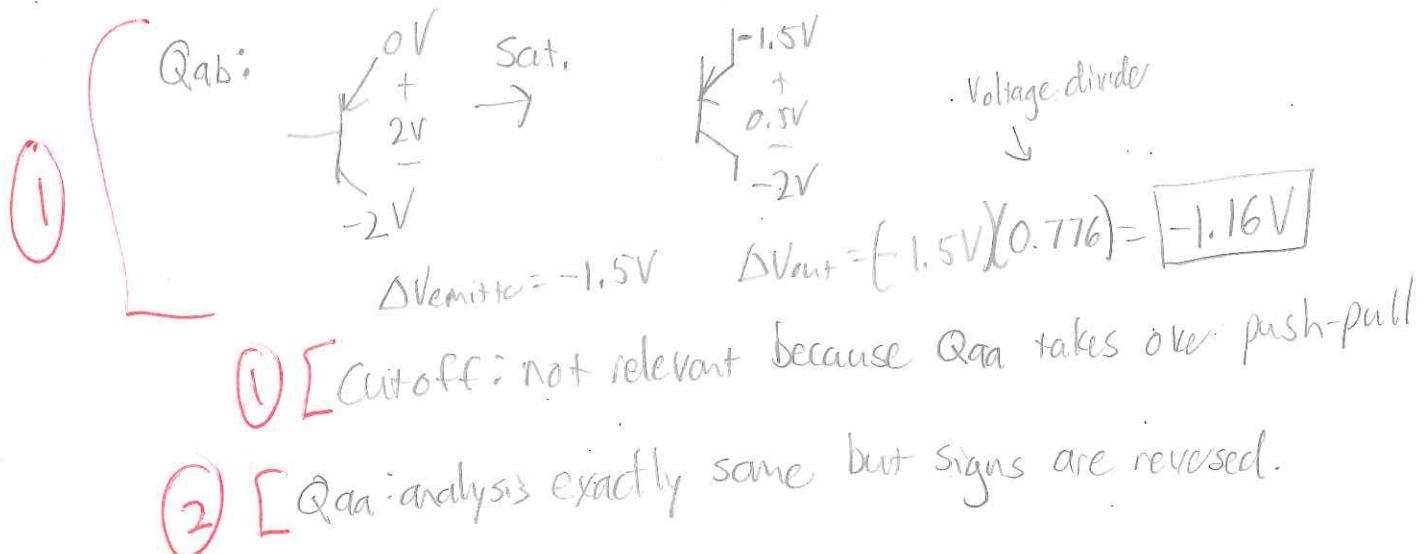
input impedance per side is $\beta[604\Omega + 104] = [10.8k\Omega]$

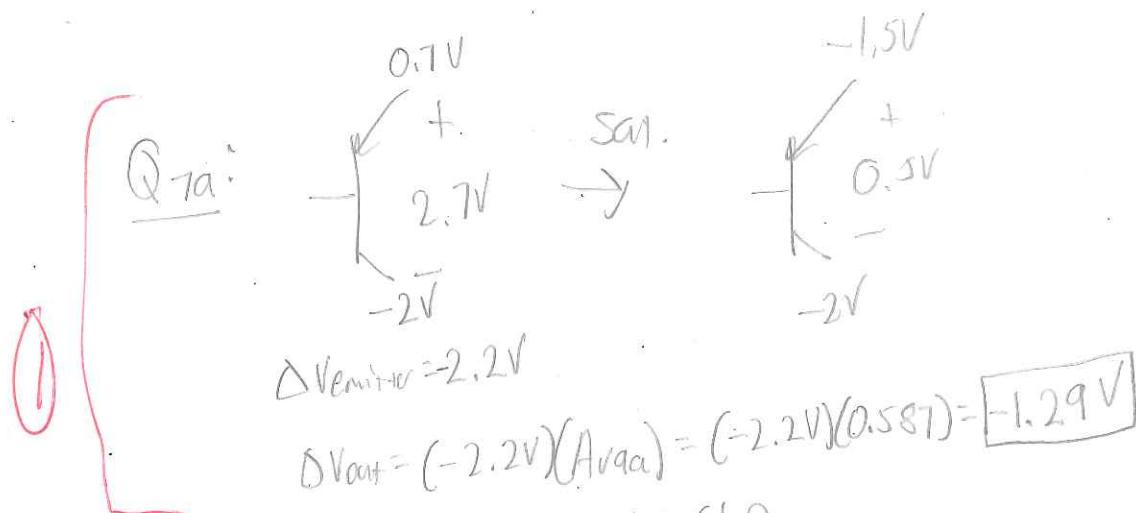
Part e, 10 points

Maximum peak-peak output voltage (*show all your work*)

	magnitude and sign of maximum output signal swing due to <i>cutoff</i>	magnitude and sign of maximum output signal swing due to <i>saturation</i>
Transistor Q4a	+0.88V	Not Relevant
Transistor Q5a	-0.47V	+1.47V
Transistor Q7a	+12.5V	-1.29V
Transistor Q7b	-12.5V	+1.29V
Transistor Q9a	Not Relevant	+1.16V
Transistor Q9b	Not Relevant	-1.16V

Be warned: In some cases a limit is not relevant at all. Mark those answers "not relevant". But, give a 1-sentence statement below as to why it is not relevant. Q7ab and Q9ab form a push pull stage, so be careful about your answers here.





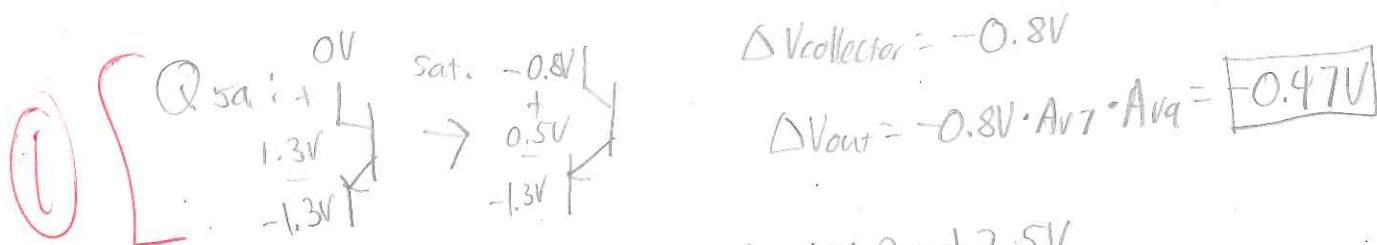
cutoff: $R_{L,\text{eq}} = R_{\text{load}} = 42.6k\Omega$

$$I_{c,q} = 0.5mA$$

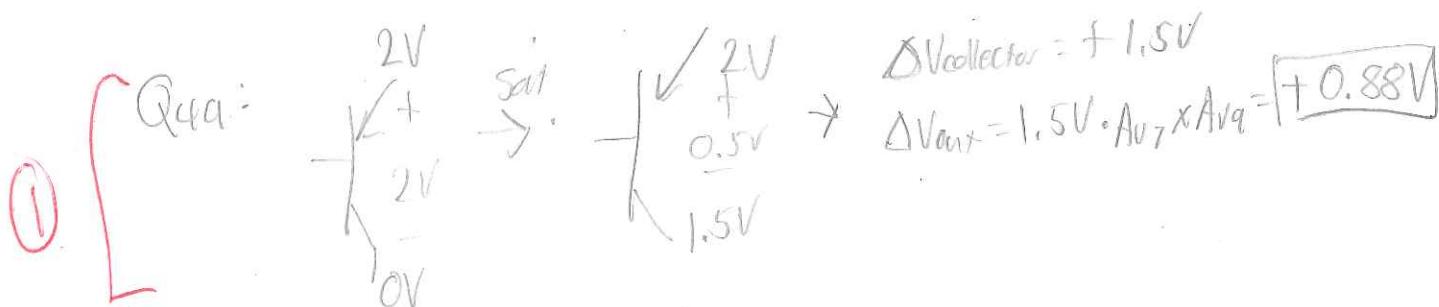
$$\Delta V_{\text{emitter}} = +21.3V$$

$$\Delta V_{\text{out}} = 21.3V \times A_{vqa} = 12.5V \text{ (irrelevant)}$$

$\textcircled{1} \left\{ \begin{array}{l} Q_{7b}: \\ \text{mirror-symmetric w/ } Q_{7a}, \text{ so answers the same} \\ \text{w/ sign reversed} \end{array} \right.$

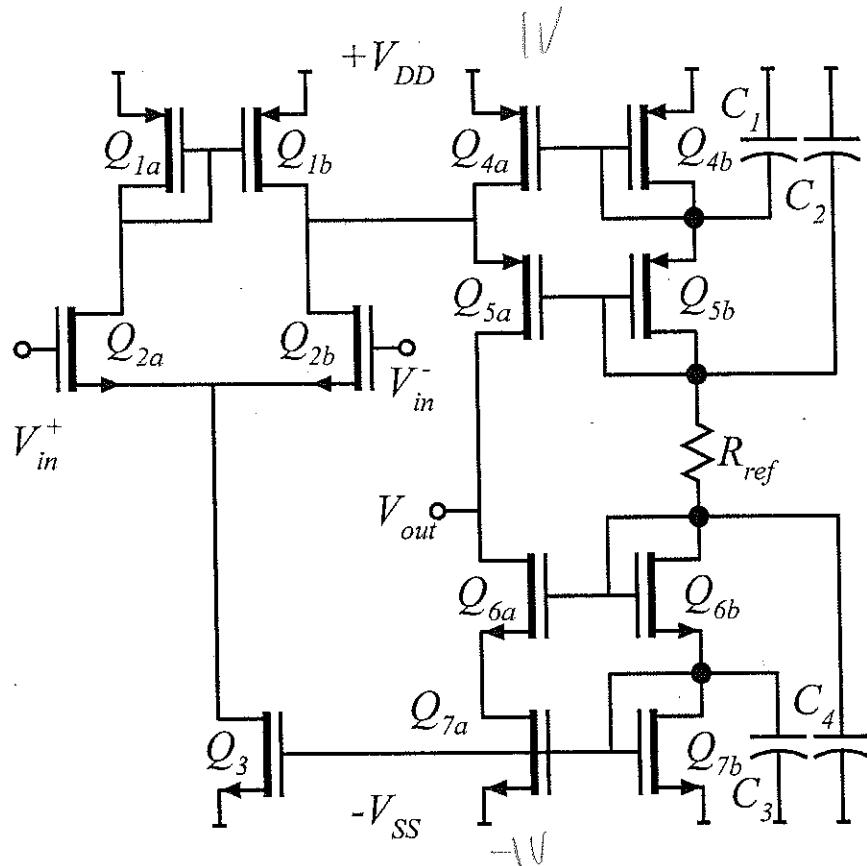


cutoff: $\Delta V_{\text{collector}} = 250mA \cdot 10k\Omega = +2.5V$

$$\Delta V_{\text{out}} = +2.5V \cdot A_{v7} \cdot A_{vd} = +1.47V$$


Problem 2, 35 points

This is an Op-Amp---analyze the bias under the assumption that DC output voltage is zero volts, that the positive input V_{i+} is zero volts, and that we must determine the DC value of the negative input voltage (V_{i-}) necessary to obtain this.



The NMOSFETs and the PMOSFETS have a 0.20 V threshold, a 22nm gate length, $300 \text{ cm}^2/\text{Vs}$ mobility, a 10^7 cm/s saturation drift velocity, and $1/\lambda=3$ Volts. The gate oxide thickness is 1.0nm and the dielectric constant is 3.8. This gives

$$\mu c_{\text{ox}} W_g / 2L_g = 15 \text{ mA/V}^2 \cdot (W_g / 1\mu\text{m}) \text{ and}$$

$$v_{\text{sat}} c_{\text{ox}} W_g = 3.36 \text{ mA/V} \cdot (W_g / 1\mu\text{m}) \quad (\text{both are a bit unrealistic for a real technology}).$$

$$\text{and } v_{\text{sat}} L_g / \mu = 0.113 \text{ V}$$

$$V_{DD} = +1 \text{ V}, \quad -V_{SS} = -1 \text{ V},$$

Part a, 10 points

DC bias.

Approximation: ignore the term $(1 + \lambda V_{DS})$ in DC bias analysis.

Analyze the bias under the assumption that DC output voltage is zero volts, that the positive input V_{i+} is zero volts, and that we must determine the DC value of the negative input voltage (V_{i-}) necessary to obtain this.

Q1ab,2ab are to be biased at $50 \mu\text{A}$ drain current.

Q4ab,5ab,6ab,7ab are to be biased at $200 \mu\text{A}$ drain current

All transistors are to operate with $|V_{gs}| = 0.30\text{V}$.

Find the gate widths of all transistors.

Find:

$$Wg1a = \underline{\quad} \quad Wg1b = \underline{\quad} \quad Wg2a = \underline{\quad} \quad Wg2b = \underline{\quad} \quad Wg3 = \underline{\quad}$$

$$Wg4a = \underline{\quad} \quad Wg4b = \underline{\quad} \quad Wg5a = \underline{\quad} \quad Wg5b = \underline{\quad}$$

$$Wg6a = \underline{\quad} \quad Wg6b = \underline{\quad} \quad Wg7a = \underline{\quad} \quad Wg7b = \underline{\quad}$$

$$R_{ref} = \underline{\quad}$$

$$\textcircled{2} \quad \left\{ \begin{array}{l} V_{gs} = 0.3\text{V} \\ \text{so } V_{gs} - V_{th} = 0.1\text{V} \end{array} \right. \quad \frac{V_{sat} L_g}{cm} \text{ so mobility limited}$$

$$\textcircled{2} \quad \left[I_d = \left[\frac{15\text{mA}}{V^2} \right] \left[\frac{W_g}{L_{um}} \right] (V_{gs} - V_{th})^2 \right]$$

$$\textcircled{2} \quad \left[I_d = 150\mu\text{A} \cdot \left(\frac{W_g}{L_{um}} \right) \rightarrow W_g = 1\text{mm} \cdot \frac{I_d}{150\mu\text{A}} \right]$$

$$\textcircled{1.33} \quad \left\{ Q_{1a,2a,1b,2b}: I_d = 50\mu\text{A} \rightarrow W_g = 0.333\text{mm} \right.$$

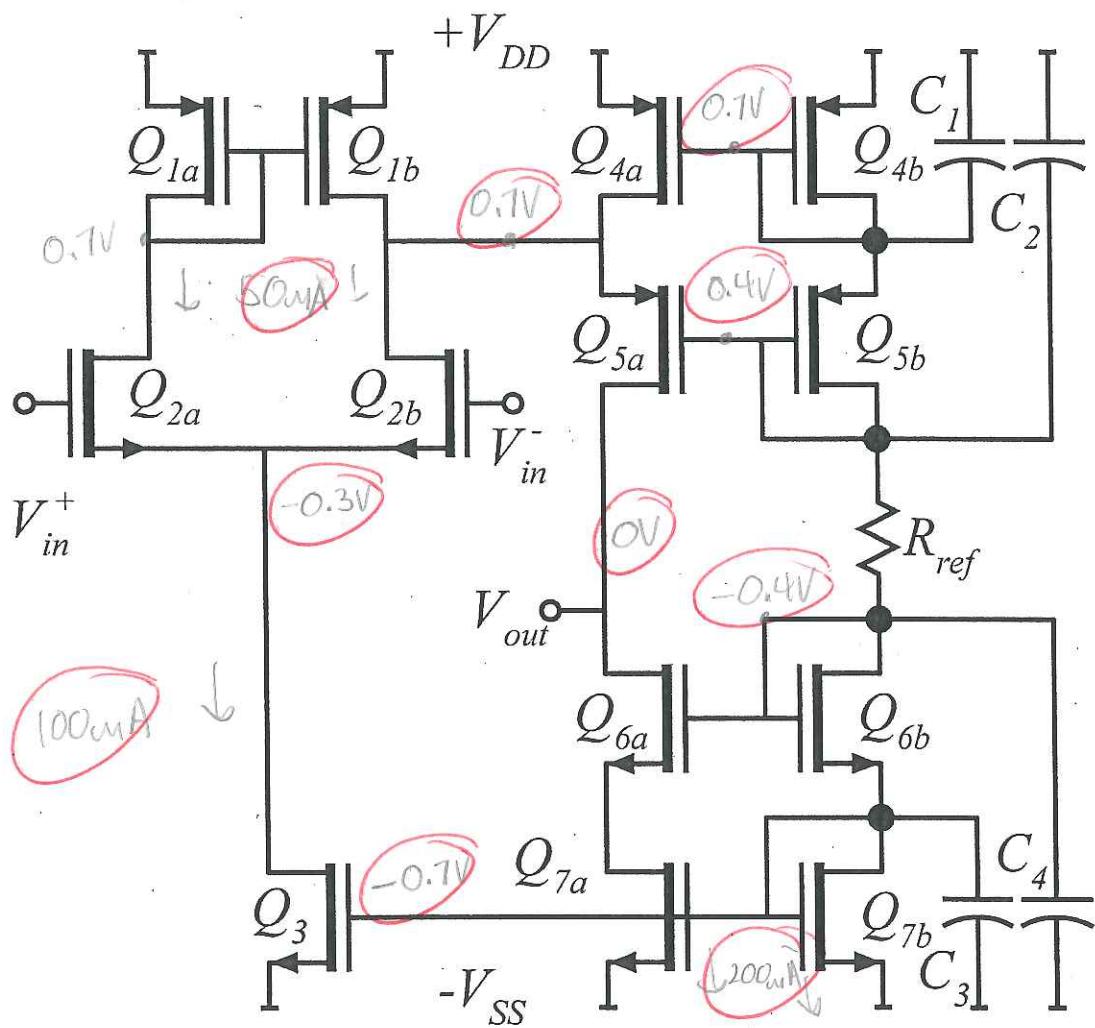
$$\textcircled{1.33} \quad \left\{ Q_3: I_d = 100\mu\text{A} \rightarrow W_g = 0.666\text{mm} \right.$$

$$\textcircled{1.33} \quad \left\{ Q_{4ab,5ab,6ab,7ab}: I_d = 200\mu\text{A} \rightarrow W_g = 1.33\text{mm} \right.$$

Part b, 10 points

DC bias

1 pt each



On the circuit diagram above, label the DC voltages at ALL nodes the drain currents of ALL transistors, and the gate widths of ALL transistors

Part c, 15 points.

You will now compute the op-amp differential gain. *You must consider the $(1 + \lambda V_{DS})$ term in the FET IV characteristics when you do this.*

The capacitors C1-C4 are all zero Ohms AC impedance. (They would not be present in a real design; they are added here to simplify the exam).

Find the following

	Voltage Gain	Input impedance
Transistor combination Q2a,2b,1a,1b	10.22	∞
Q5a	59	15.5 k Ω
Overall differential Vout/Vin	603	∞

(Alternative---if you very skilled, you might be able to compute the combined gain of Q2a,2b,1a,1b and Q5a, all together, in a single step using Norton or Thevenin methods. If you do so, first, don't ask for hints on how to do this and, second, do please also calculate the input impedance of Q5a.)

$$\text{Since } I_D = \frac{15\text{mA}}{\sqrt{2}} (V_{gs} - V_{th})^2 \frac{W_g}{L_{um}}, g_m = \frac{30\text{mA}}{\sqrt{2}} (V_{gs} - V_{th}) \left(\frac{W_g}{L_{um}} \right)$$

$$g_m = 3\text{mS} \cdot \frac{W_g}{L_{um}}$$

$$\text{Q1ab,2ab : } g_m = 1\text{mS}$$

$$\text{Q3 : } g_m = 2\text{mS}$$

$$\text{Q4ab,5ab,6ab,7ab : } g_m = 4\text{mS}$$

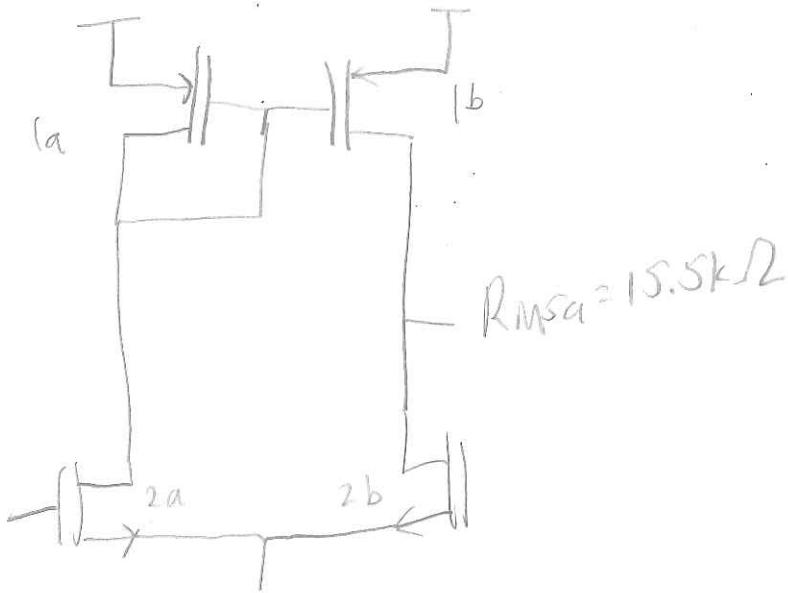
$$\text{① } R_{DS} = \frac{1}{I_D}, \text{ so } R_{DS5a,6a} = \frac{3\text{V}}{200\text{mA}} = 15\text{k}\Omega$$

$$\text{② } R_{out,drain6a} = R_{ds6a}(1 + g_{m6a} R_{ds7a}) = 915\text{k}\Omega$$

$$\text{③ } R_{L_{eq}} = R_{out,drain6a} = 915\text{k}\Omega$$

$$\text{④ } R_{in5a} = \frac{1}{g_{m5a}} \left(\frac{R_{eq} + R_{DS}}{R_{DS}} \right) = 15.5\text{k}\Omega$$

$$\text{⑤ } A_{v5a} = \frac{R_{eq}}{R_{in5a}} = 59$$



$Q_{1ab}, 2ab$

$$\textcircled{1} \quad \sum g_{ms} = 1 \text{ ms}$$

$$\textcircled{1} \quad \sum R_{DS} \approx \frac{3V}{50 \text{ mA}} = 60 \text{ k}\Omega$$

$$\textcircled{2} \quad \text{Stage transconductance} = g_{m1ab} = 1 \text{ ms}$$

$$\textcircled{1} \quad R_{L,eq} = R_{MSa} \parallel R_{DS1b} \parallel R_{DS1a} = 15.5 \text{ k}\Omega \parallel 60 \text{ k}\Omega \parallel 60 \text{ k}\Omega = \\ = \boxed{10.22 \text{ k}\Omega}$$

$$\textcircled{2} \quad \text{gain} = 1 \text{ ms} \cdot 10.22 \text{ k}\Omega = 10.22$$

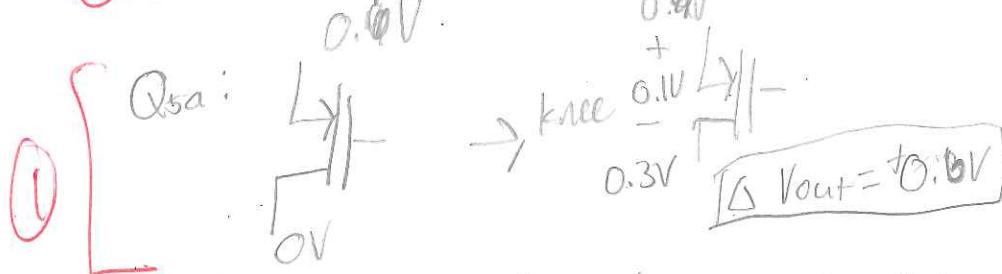
Part d, 10 points

Maximum peak-peak output voltage at the positive output V_{o+} (*show all your work*)

	magnitude and sign of maximum output signal swing due to <i>cutoff</i>	magnitude and sign of maximum output signal swing due to: <i>knee voltage</i> (saturation)
Transistor Q5a	-183 V	+0.6 V
Transistor Q6a	Cannot cut off	-0.6 V
Transistor Q2a	+ huge	Cannot be reached \rightarrow irrelevant
Transistor Q2b	- huge	- irrelevant

Be warned: in some cases a limit is not relevant. Mark those answers "not relevant". But, give a 1-sentence statement why below.

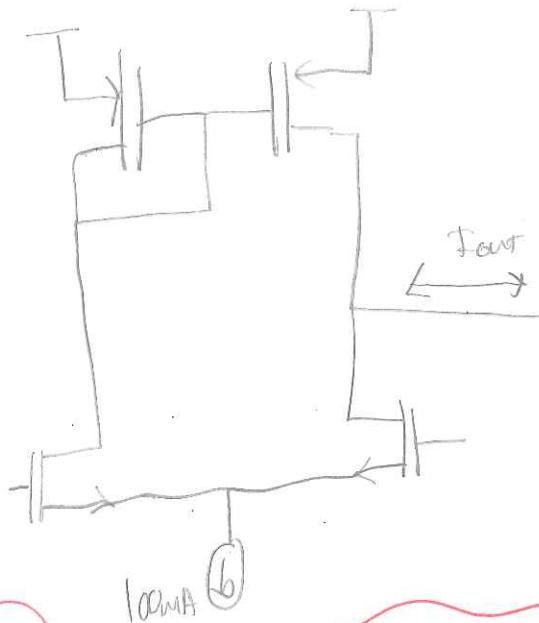
② μ -limited, so $V_{ds,sat} = V_{gs} - V_{th} = 0.1V$ for all Fets



① By symmetry, knee voltage of Q_{6a} limits ΔV_{out} to -0.3V

② Cutoff of Q_{5a} , $\Delta I_d = 200\text{mA}$ $R_{eq} = 915\text{k}\Omega$
 $\Delta V_{out} = -183V \rightarrow$ irrelevant

Cutoff of Q_{2a} & Q_{2b}



As Q_{2a} & Q_{2b} are driven, one full on and the other off cut off

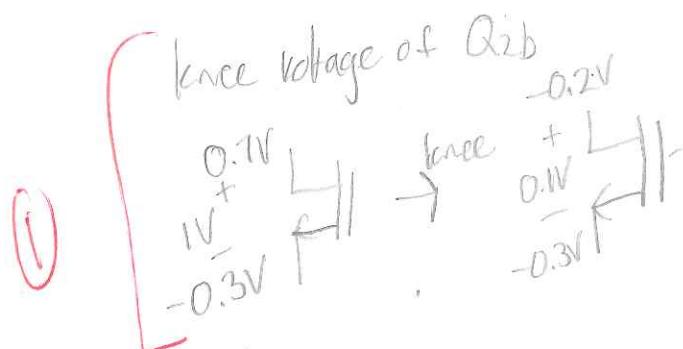
I_{out} varies by $\pm 100\text{mA}$

This drives $\pm 100\text{mA}$ into
effective load of $915\text{k}\Omega$

$$= \pm 91.5\text{V}$$

Huge \rightarrow irrelevant

① knee voltage of Q_{2a} cannot be reached until past Q_{2b} cutoff
irrelevant

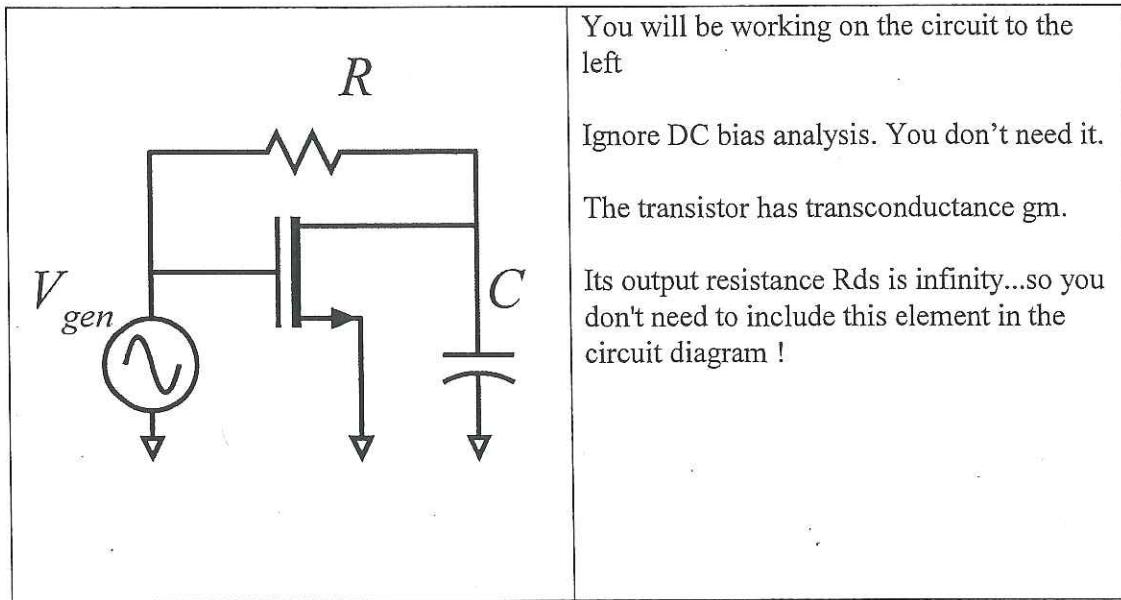


$$\Delta V_{diam} = -0.9\text{V}$$

$$\Delta V_{out} = (-0.9\text{V}) A_{v2a} = -\text{large number}$$

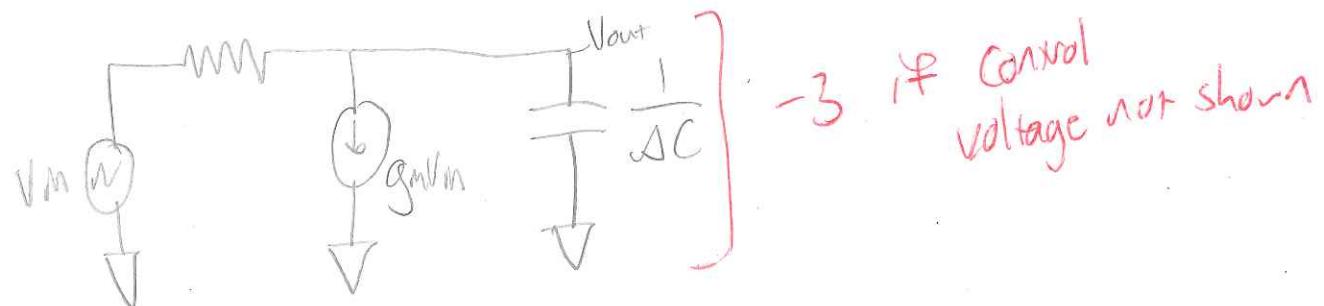
irrelevant

Problem 3, 30 points



Part a. 7 points

Draw a small-signal equivalent circuit of the circuit.



Part b, 8 points

$gm=20 \text{ mS}$, $C=1 \mu\text{F}$, $R=1000 \text{ Ohms}$

Find, by nodal analysis, a small-signal expression for V_{out}/V_{in} . Be sure to give the answer with **correct units** and in ratio-of-polynomials form, i.e.

$$\frac{V_{out}(s)}{V_{gen}(s)} = K \cdot \frac{1+b_1s+b_2s^2+\dots}{1+a_1s+a_2s^2+\dots} \text{ or (as appropriate)} \frac{V_{out}(s)}{V_{gen}(s)} = K \cdot (s\tau)^n \cdot \frac{1+b_1s+b_2s^2+\dots}{1+a_1s+a_2s^2+\dots}$$

Note that an expression like

$$\frac{V_{out}(s)}{V_{gen}(s)} = \frac{1}{1+(3 \cdot 10^{-6})s} \text{ is dimensionally wrong; } \frac{1}{1+(3 \cdot 10^{-6} \text{ seconds})s} \text{ is dimensionally correct}$$

$$V_{out}(s)/V_{in}(s) = \underline{\hspace{2cm}}$$

$$\sum I @ V_{out}=0 \Rightarrow V_{out} \left(sC + \frac{1}{R} \right) + V_{in} \left(gm - \frac{1}{R} \right) = 0$$

4pts for some version of this

$$\frac{V_o}{V_m} = \frac{-(gm - \frac{1}{R})}{sC + \frac{1}{R}} = \frac{-(gmR - 1)}{1 + sCR} \quad RC = 1 \text{ ms} = 10^{-3} \text{ sec}$$

$$\frac{V_{out}}{V_m} = -19 \left[\frac{1}{1 + s \cdot 1 \text{ ms}} \right] \quad \text{4pts}$$

$$2\pi f \cdot 1 \text{ ms} = 1 \Rightarrow f_{pole} = 159 \text{ Hz}$$

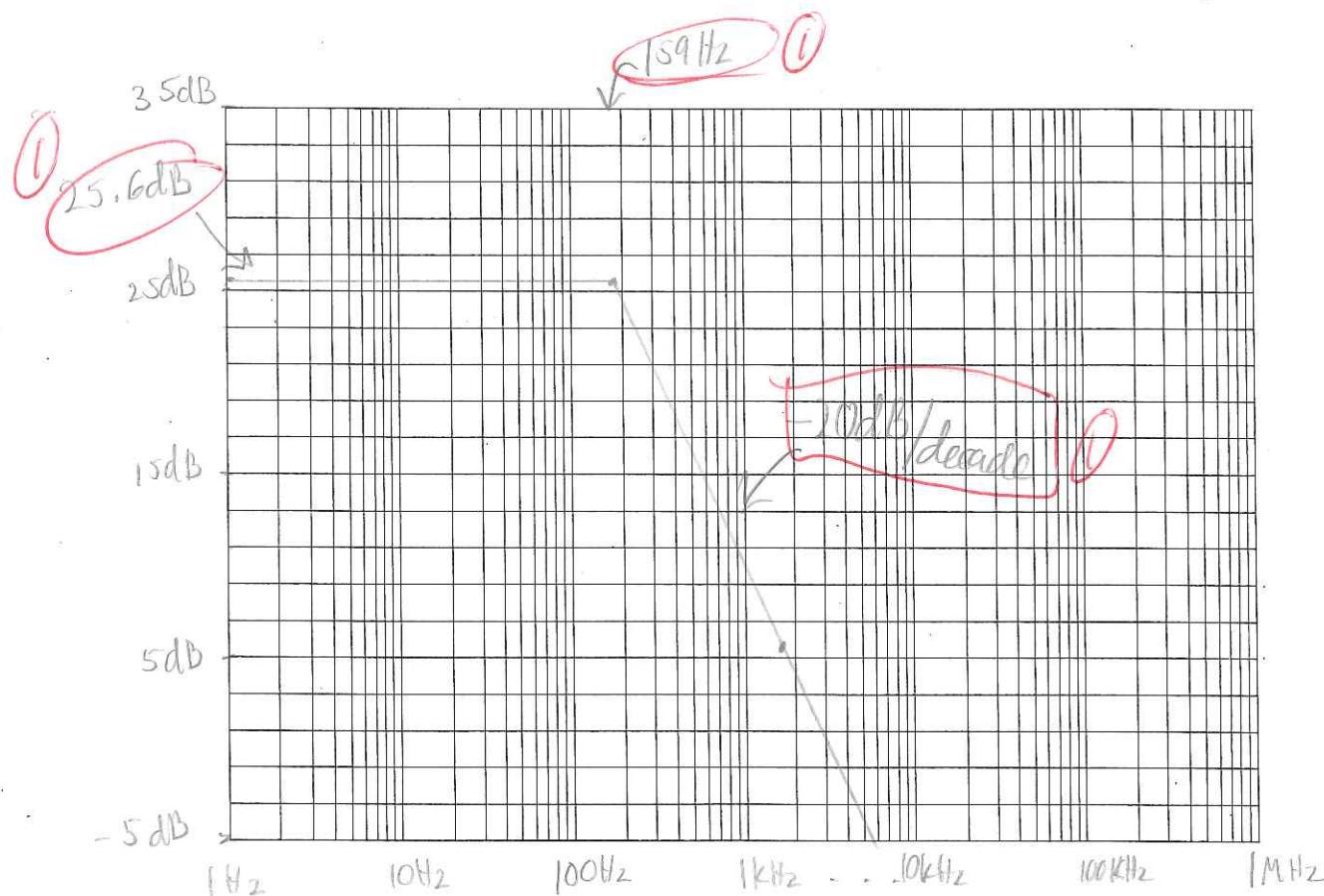
Part c, 7 points

Find any/all pole and zero frequencies of the transfer function, in Hz:

pole at 159 Hz (2)

Draw a clean Bode Plot of V_{out}/V_{in} ,

LABEL AXES, LABEL all relevant gains and pole or zero frequencies, Label Slopes



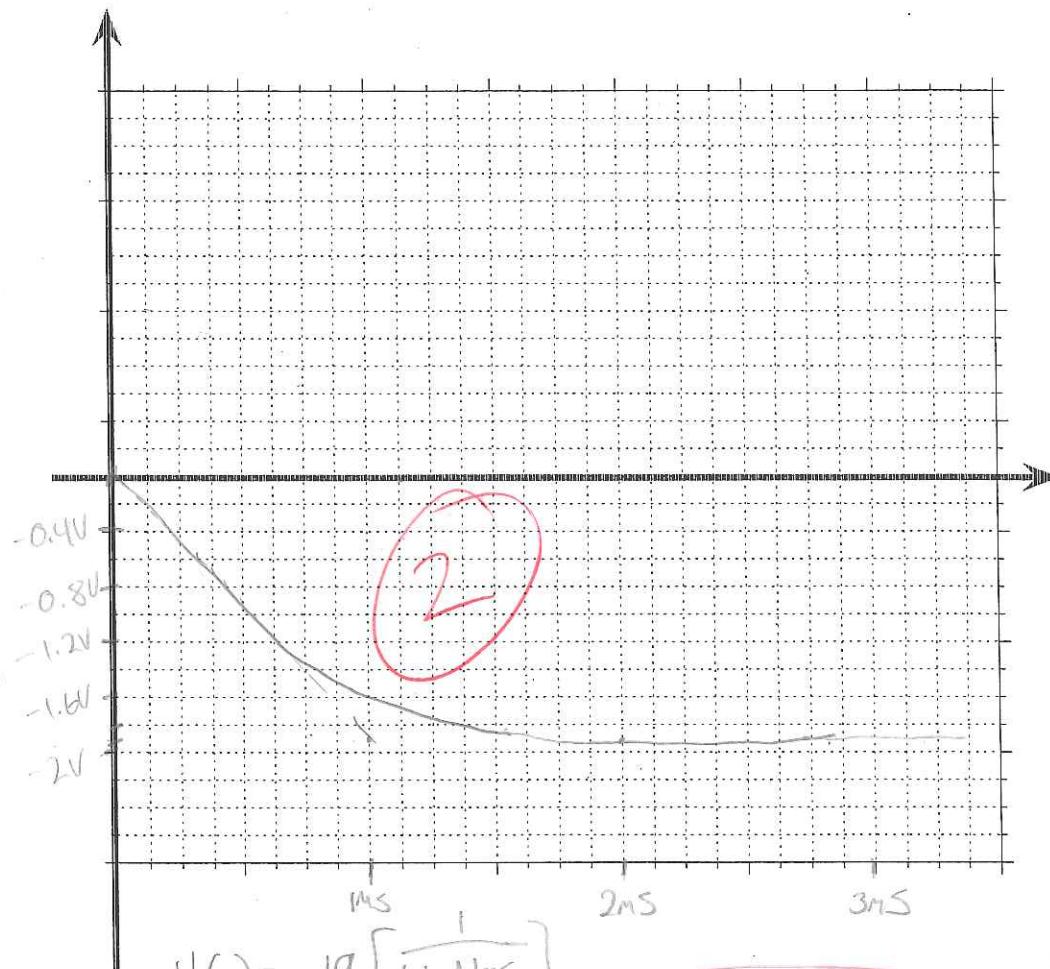
2 points for axes labelled sensibly

Part d, 8 points

$V_{in}(t)$ is a 0.1 V amplitude step-function.

Find $V_{out}(t) = \underline{\hspace{2cm}}$

Plot it below. Label axes, show initial and final values, show time constants.



$$H(s) = -19 \left[\frac{1}{1 + sT_{ms}} \right]$$

$$\textcircled{2} \quad V_{in}(s) = \frac{0.1V}{s}$$

$$\text{so } V_{out}(s) = -1.9V \cdot \left(\frac{1}{s} \right) \left(\frac{1}{1 + sT_{ms}} \right)$$

$$V_{out}(t) = \left[-1.9 + 1.9e^{-\frac{t}{T_{ms}}} \right] u(t)$$