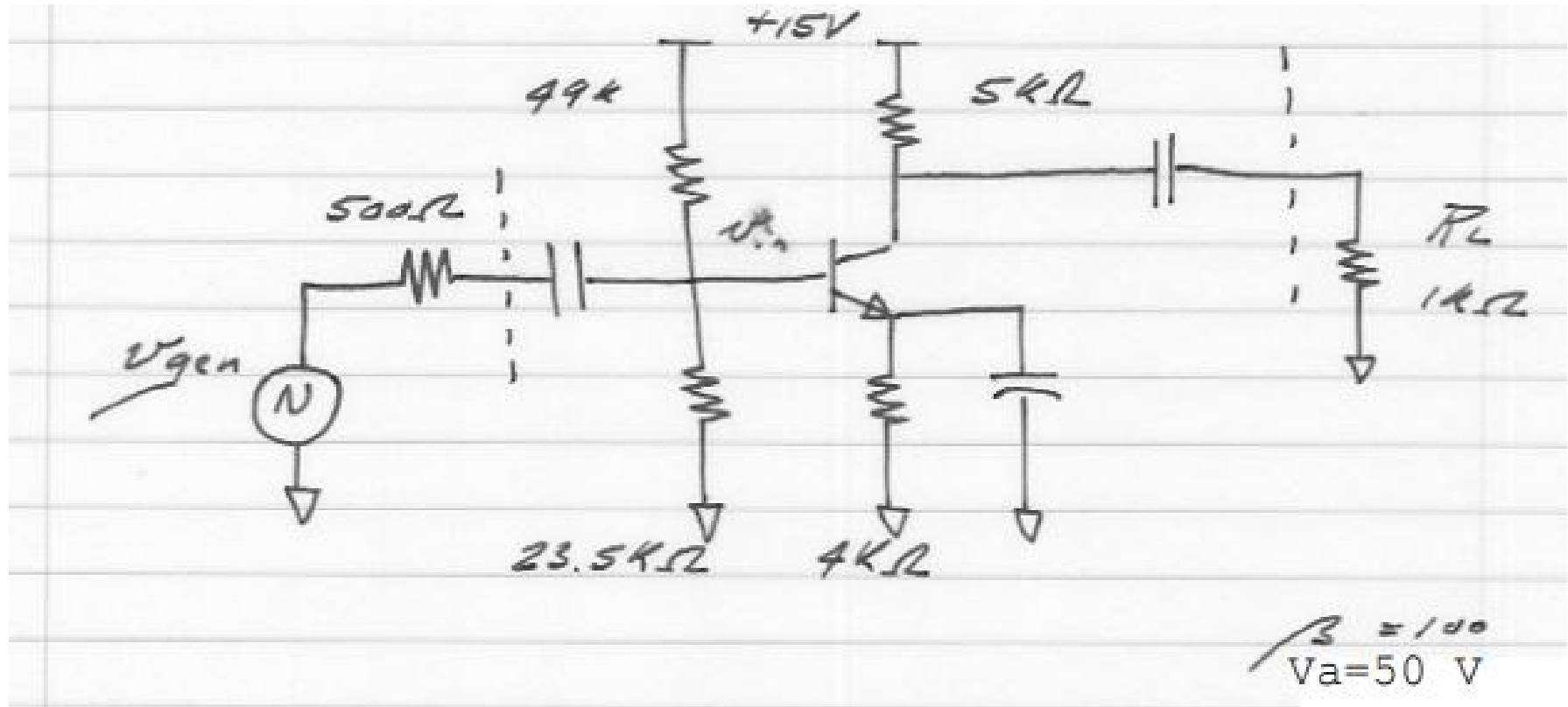


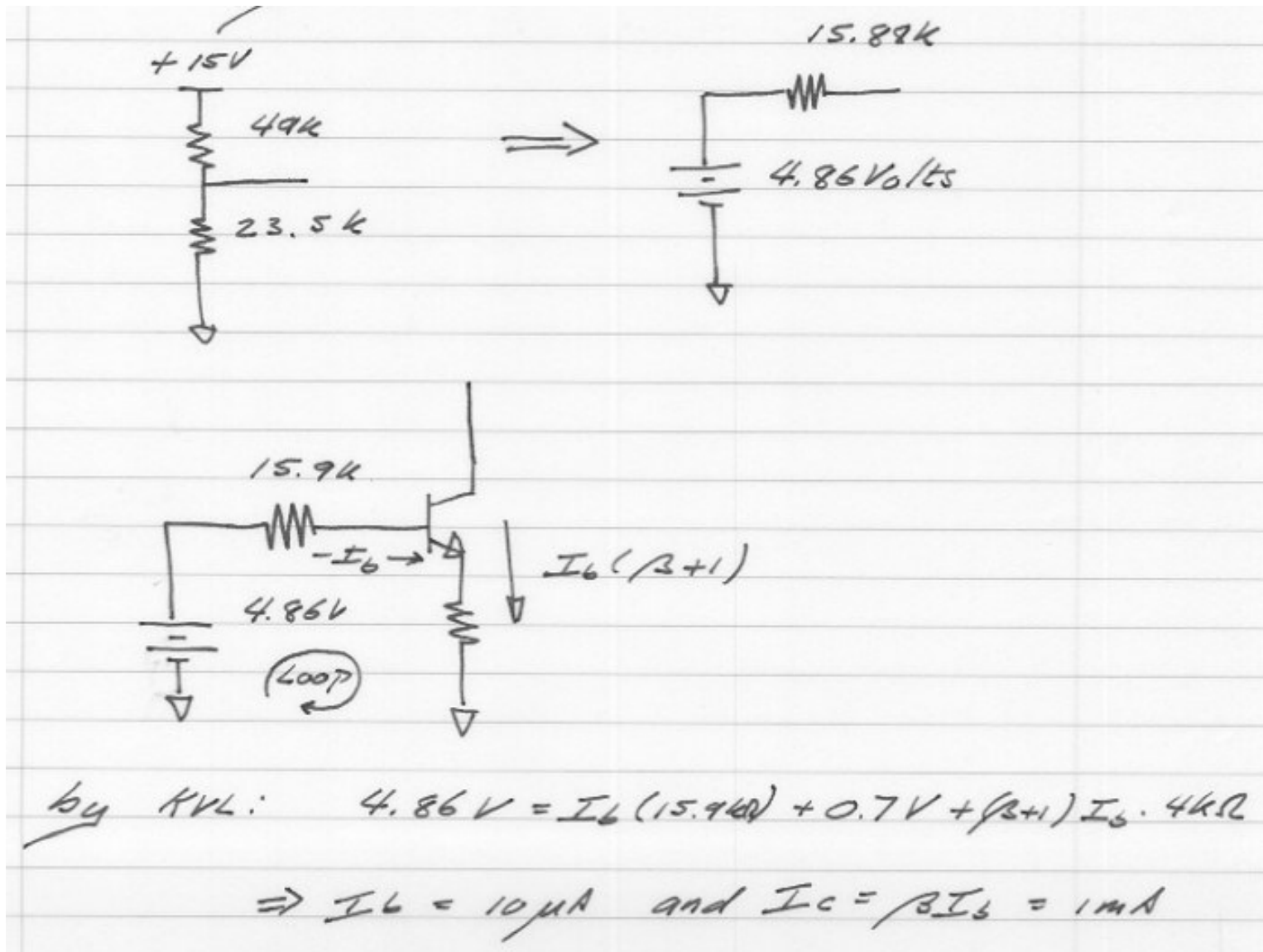
ECE137A Notes Set 3: Basic Common-Emitter Amplifier

***Mark Rodwell,
Doluca Family Chair, ECE Department
University of California, Santa Barbara
rodwell@ece.ucsb.edu***

Common-Emitter Amplifier: 1950's-style



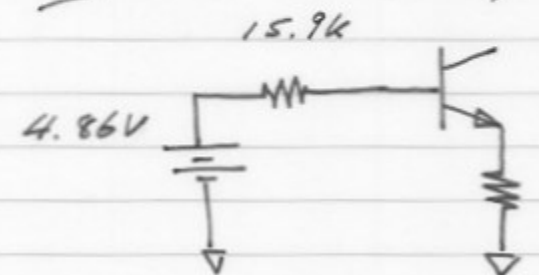
DC bias analysis: exact (slow) method



fast DC bias analysis: iteration

Relies on I_b having only small effect in well-designed circuit: treat I_b as a *perturbation*

First guess: assume $\beta = \infty$

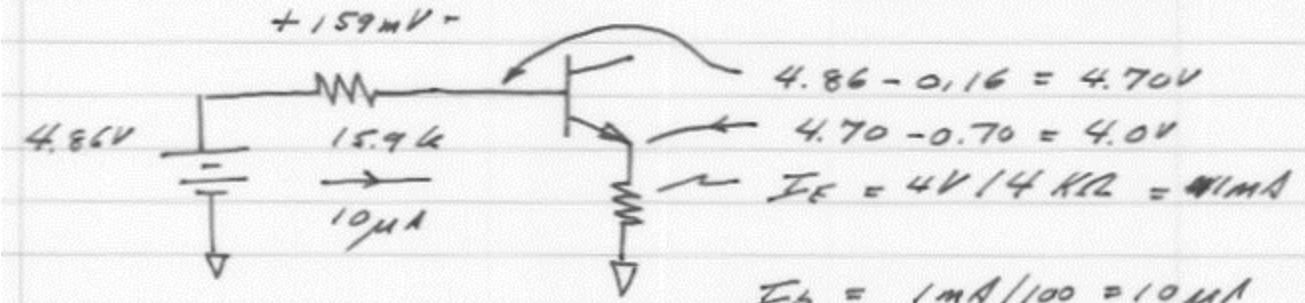


$I_b = 0 \Rightarrow V_b = 4.86V$
 $\Rightarrow V_E = 4.16V$
 $\Rightarrow I_E = 4.16 / 4k = 1.04mA$

Now, if $\beta = \infty \Rightarrow I_E = 1.04mA$

But $\beta \neq \infty \Rightarrow \beta = 100$ so $I_b = 1.04mA / 100 \approx 10.4\mu A$

Second guess - reanalyze with the base current we have found

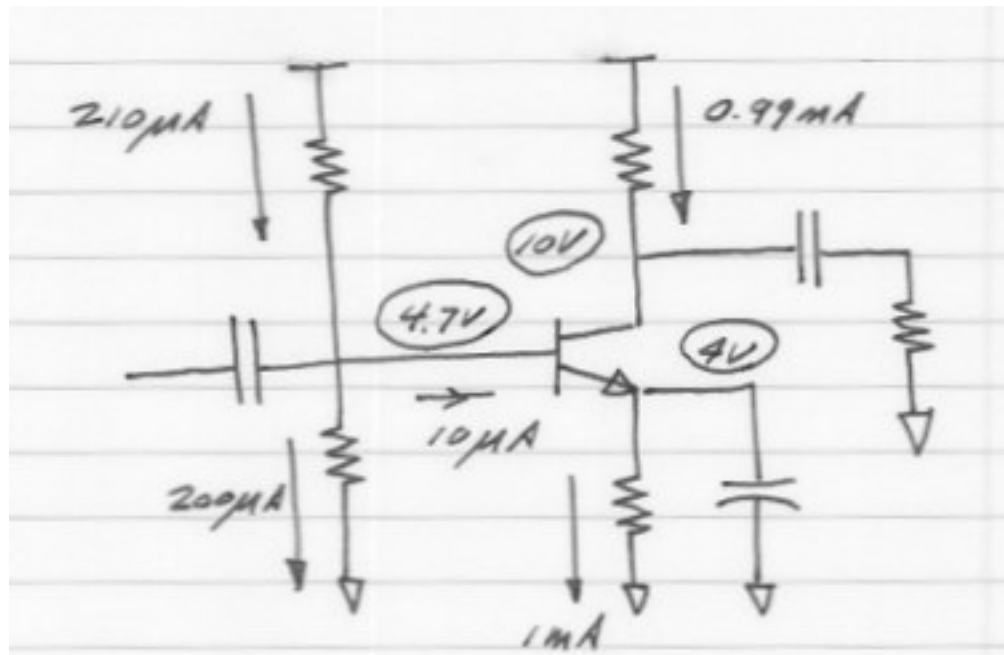


+159mV -

$4.86V$ $15.9k$ $4.70V$
 $4.86 - 0.16 = 4.70V$
 $4.70 - 0.70 = 4.0V$
 $I_E = 4V / 4k\Omega = 1mA$
 $I_b = 1mA / 100 = 10\mu A$

Iteration can be repeated if necessary

DC bias solution



This circuit is AC coupled with RC bias network. Why teach such old-fashioned techniques ? (1) As we progress from single-transistor to multi-stage designs, it is easier to progress from AC to DC coupling than to start with DC-coupled designs. (2) AC coupled designs are easier for the first 1-2 lab projects. (3) Even modern RF gain stages *are* AC coupled.

Above all (4), we will quickly transition in the next 3 weeks to DC coupling.

AC small signal analysis.

- replace $\frac{1}{s}$ with small signal model
- replace supplies with AC ∇
- replace large $\frac{1}{s}$ with short circuits

$$\text{---} \parallel \text{---} \quad Z = 1/j\omega C = \text{is this very small?}$$

→ if so, neglect

- replace large ∞ with open circuits

$$Z = j\omega L = \text{is this large?}$$

→ if so, neglect.

ω is the signal frequency.

At some low ω , $1/j\omega C$ and $j\omega L$ become significant.

We treat this in ece137B

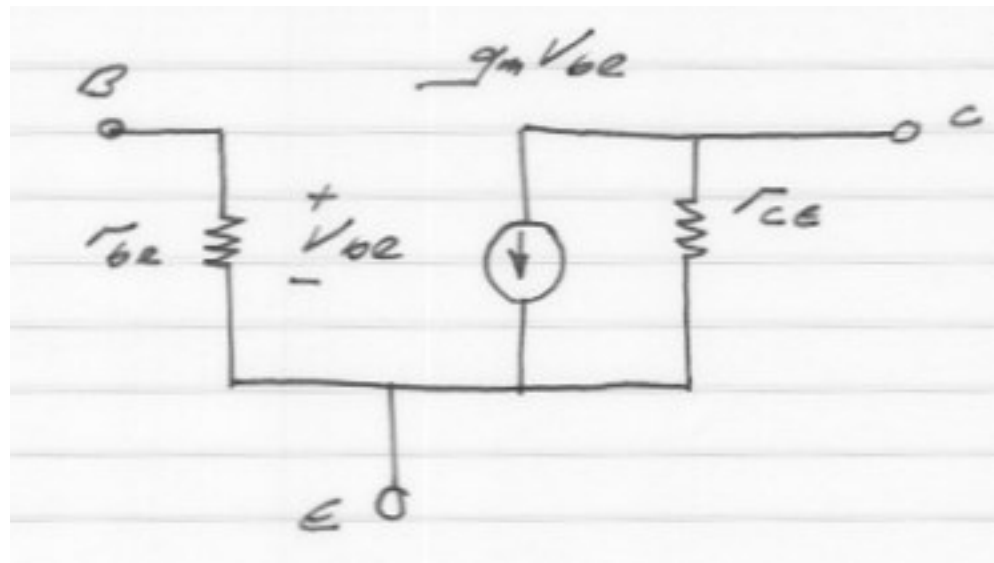
Small-signal model

$$r_e = V_T / I_E = 25 \text{ mV} / 1 \text{ mA} = 26 \Omega$$

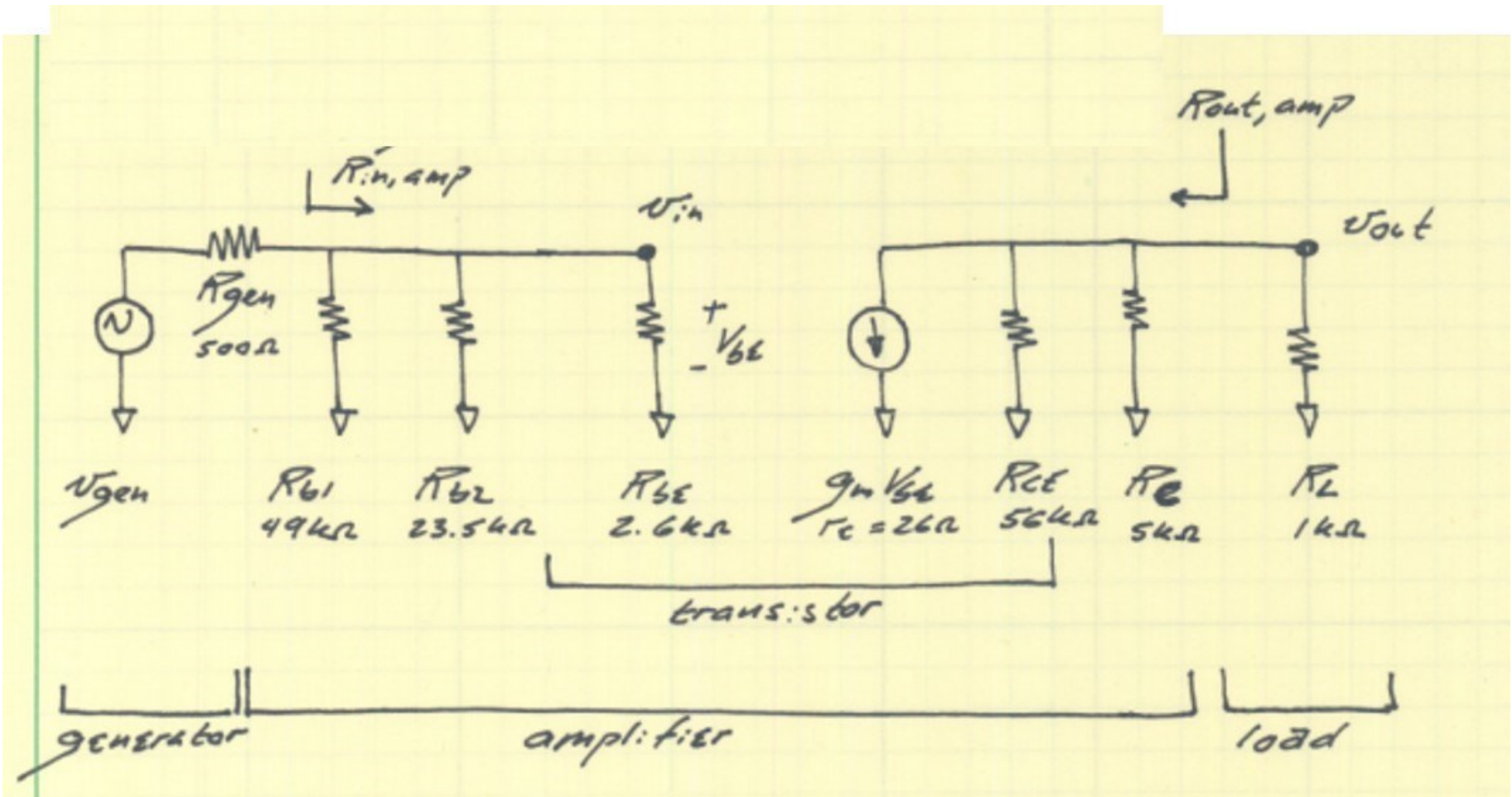
$$g_m = \alpha / r_e \approx 1 / 26 \Omega \quad (\alpha = 0.99)$$

$$r_o = r_{ce} = (V_{CE} + V_A) / I_C = 56 \text{ V} / 1 \text{ mA} = 56 \text{ k}\Omega$$

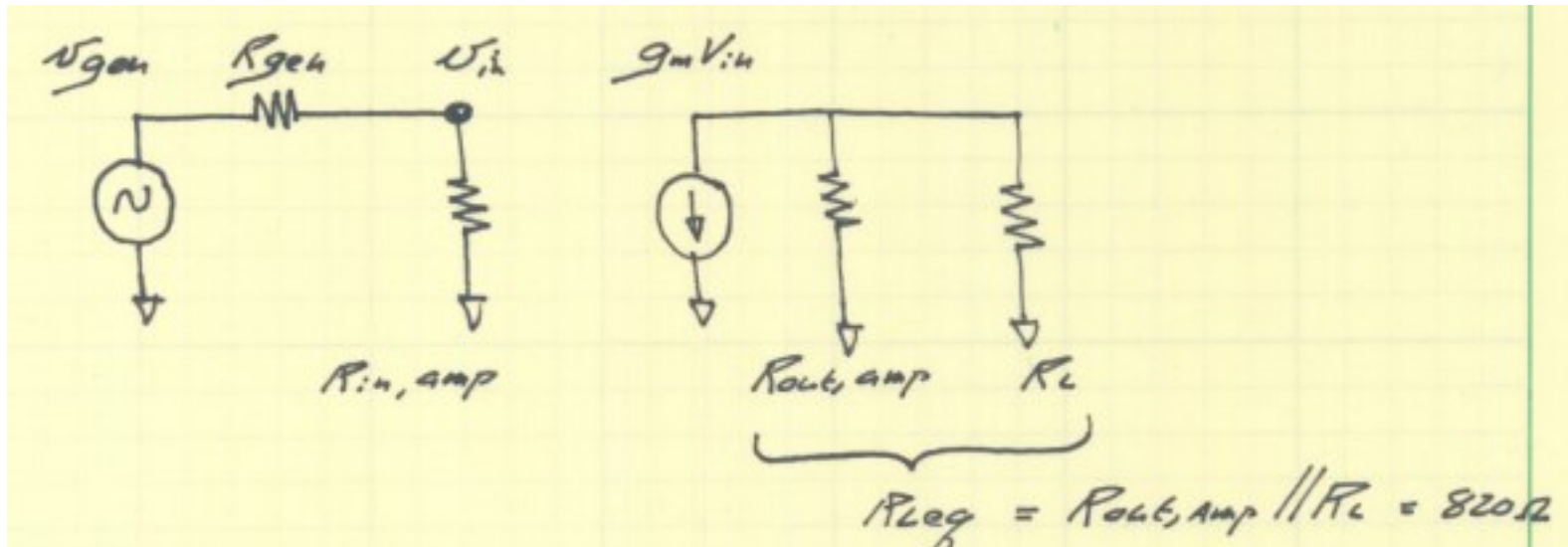
$$r_{\pi} = r_{be} = (\beta + 1) r_e \approx \beta r_e = 100 (26) = 2.6 \text{ k}\Omega$$



Circuit diagram: small-signal



Small-signal analysis



$$R_{in,amp} = R_{s1} \parallel R_{b2} \parallel R_{be} = 2.23 \text{ k}\Omega$$

$$R_{out,amp} = R_{ce} \parallel R_c = 4.60 \text{ k}\Omega$$

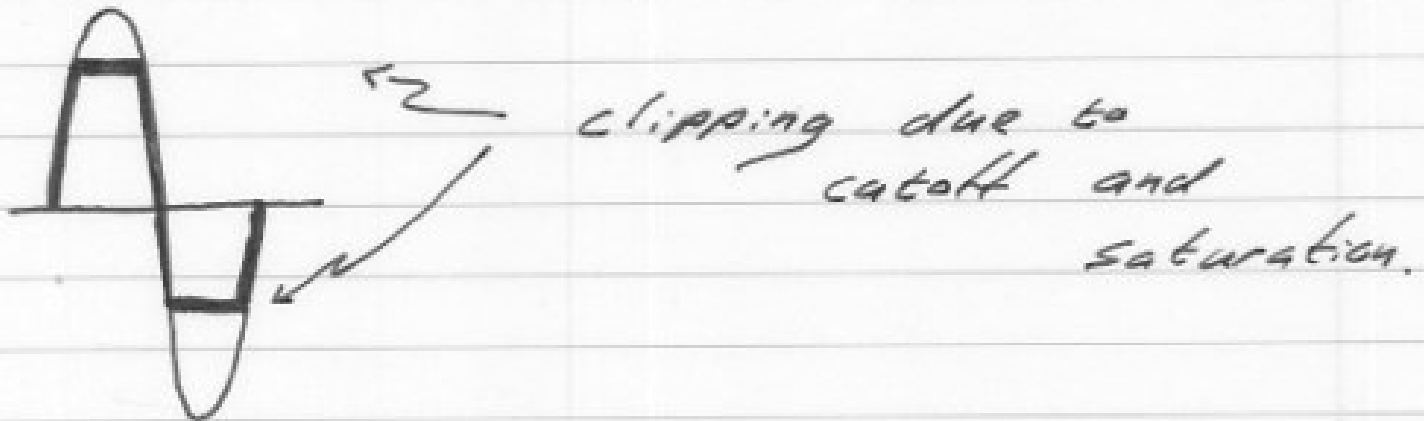
$$v_{in} / v_{gen} = R_{in,amp} / (R_{in,amp} + R_{gen}) = 0.817$$

$$v_o / v_{in} = -g_m \cdot R_{eq} = -31.5$$

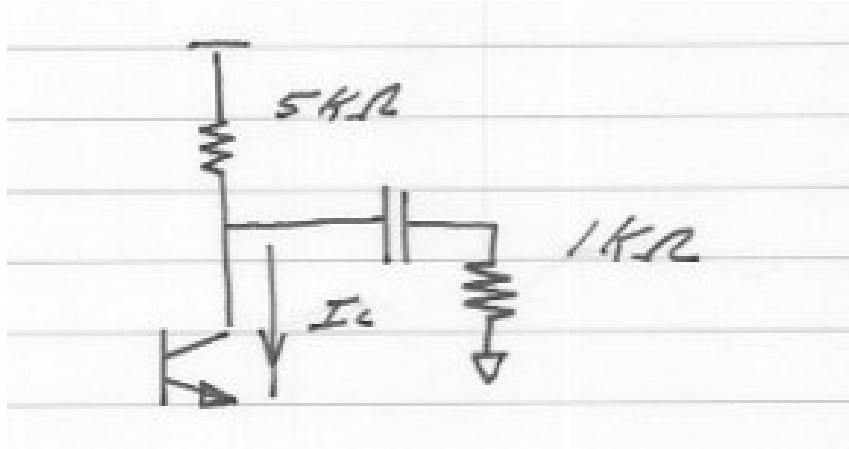
Limits on output swing

Output - small signal 

Output with larger input signal



Limits on output swing: cutoff



Clipping is large-signal, but AC, not DC.

→ Capacitors remain AC short-circuits.

$$R_{Leq} = 5k\Omega \parallel 1k\Omega = 800\Omega$$

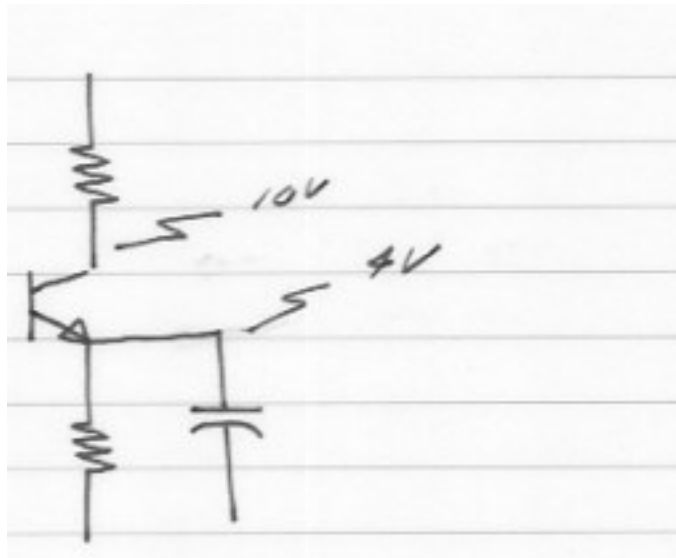
$$I_{CQ} = 1\text{mA} \text{ but } I_{C,\min} = 0\text{mA} \rightarrow \Delta I_C \downarrow_{\max} = 1\text{mA}.$$

We can decrease I_C by at most 1mA.

$$\Delta V_{out} \uparrow_{\max} = 1\text{mA} \cdot R_{Leq} = 0.8\text{V}.$$

V_{out} can increase by at most 0.8V.

Limits on output swing: saturation



Under bias: $V_{CEQ} = 10 - 4 = 6V$

Minimum: $V_{CEmin} = V_{CEsat} \approx 0.5V$

$\Delta V_{CE \downarrow max} = 6 - 0.5 = 5.5 \text{ Volts}$

Since there is no ac voltage on the emitter,

this corresponds to $\Delta V_{out \downarrow maximum} = 5.5 \text{ Volts}$.