

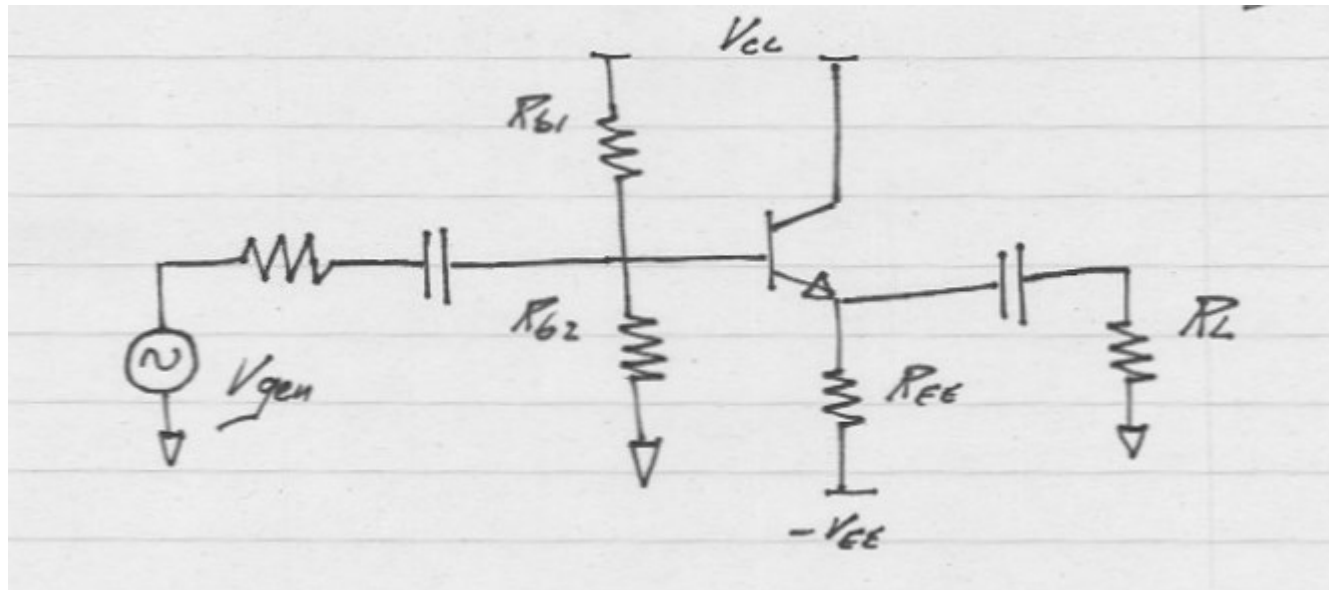
ECE137A, notes set 5: Source Follower, Emitter Follower

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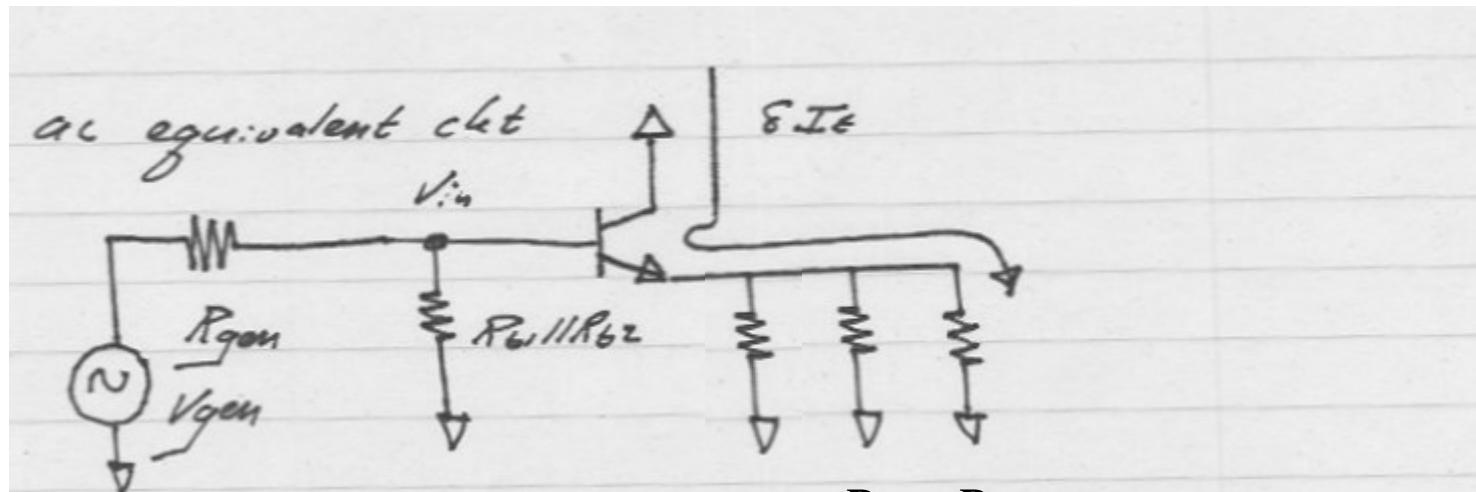
Emitter Follower, Source Follower

Both used when:

- driving a low load resistance
- small output impedance required.
- operating from a high generator resistance
- high input impedance required.



Analysis



$$R_{CE} \quad R_{EE} \quad R_L$$

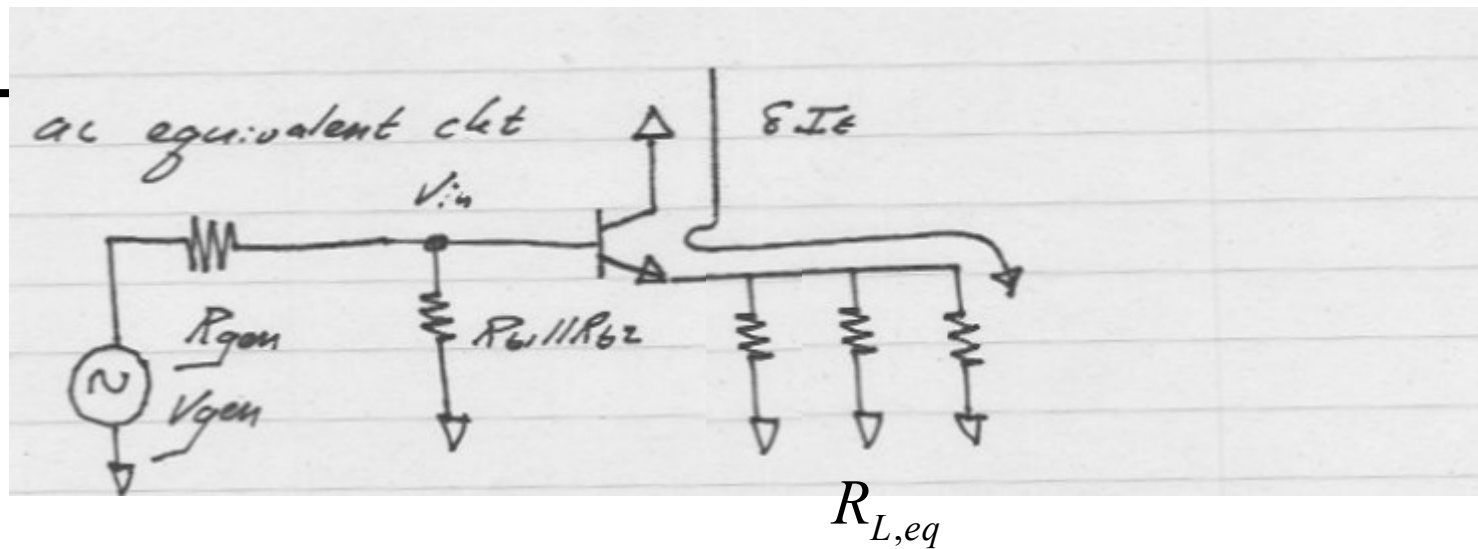
$$R_{CE} \parallel R_{EE} \parallel R_L = R_{L,eq}$$

given δI_E :

$$\delta V_{emitter} = \delta V_{out} = R_{L,eq} \cdot \delta I_E$$

$$\delta V_{be} = r_e \cdot \delta I_E \quad \text{because} \quad r_e^{-1} = g_m \triangleq \frac{\partial I_E}{\partial V_{be}}$$

Analysis



so: $\delta V_{in} = \delta V_{be} + \delta V_e$

$$= \delta I_e (R_{L,eq} + r_e) = R_{L,eq} \cdot \delta I_e \left(\frac{R_{L,eq} + r_e}{R_{L,eq}} \right)$$

$$\delta V_{in} = \delta V_{out} \left(\frac{R_{L,eq} + r_e}{R_{L,eq}} \right)$$

Small signal gain: $\frac{v_{out}}{v_{in}} = \frac{R_{L,eq}}{R_{L,eq} + r_e}$

$r_e = 1/g_m$

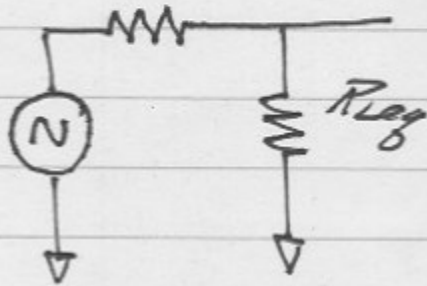
Emitter Follower Voltage Gain

Small signal gain:
$$\frac{v_{out}}{v_{in}} = \frac{R_{L||\beta}}{R_{L||\beta} + r_e}$$

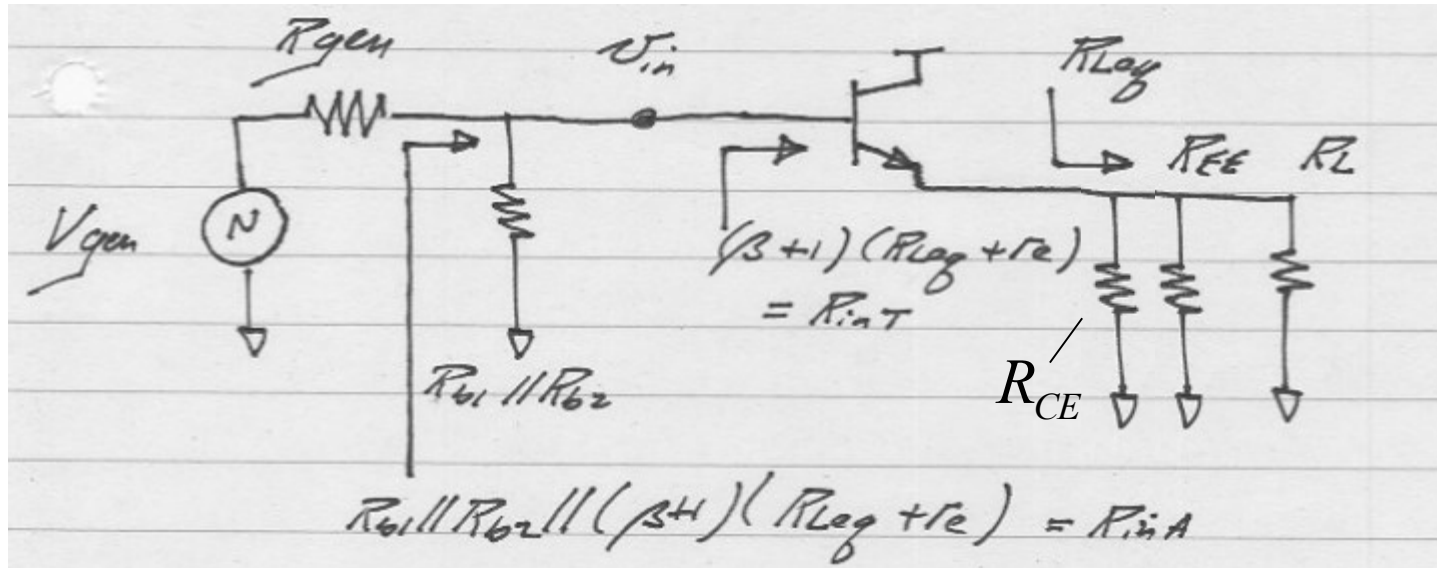
$r_e = 1/g_m$

this is similar to a voltage divider

between r_e and $R_{L||\beta}$:

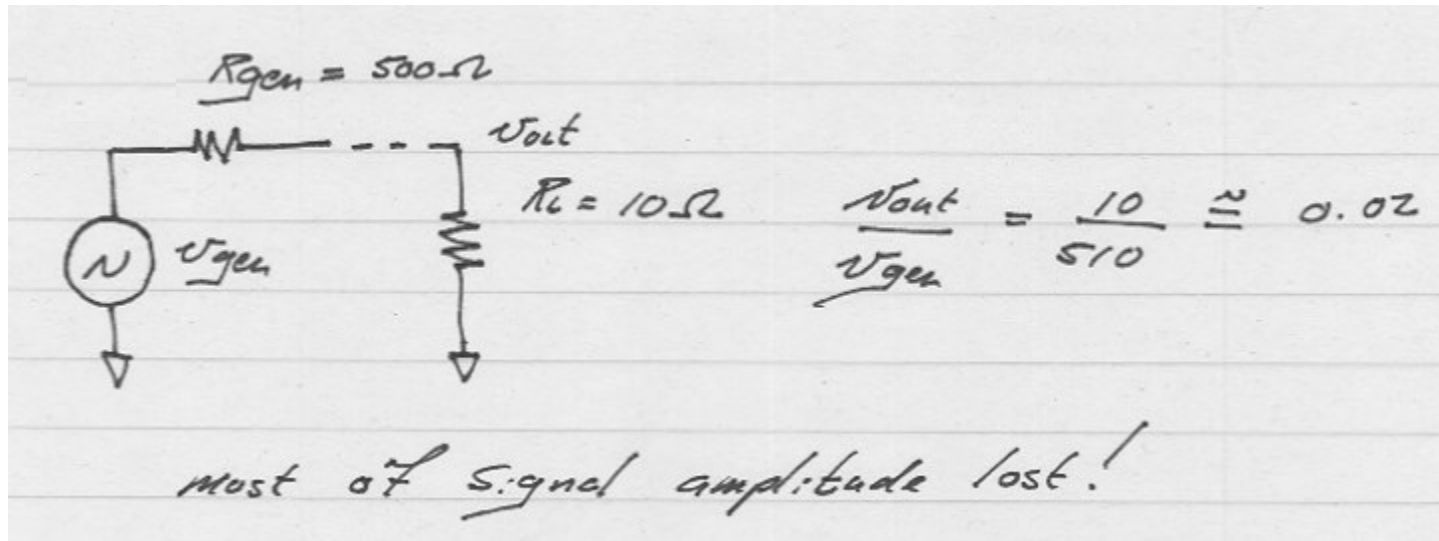


Impedances in the Emitter Follower

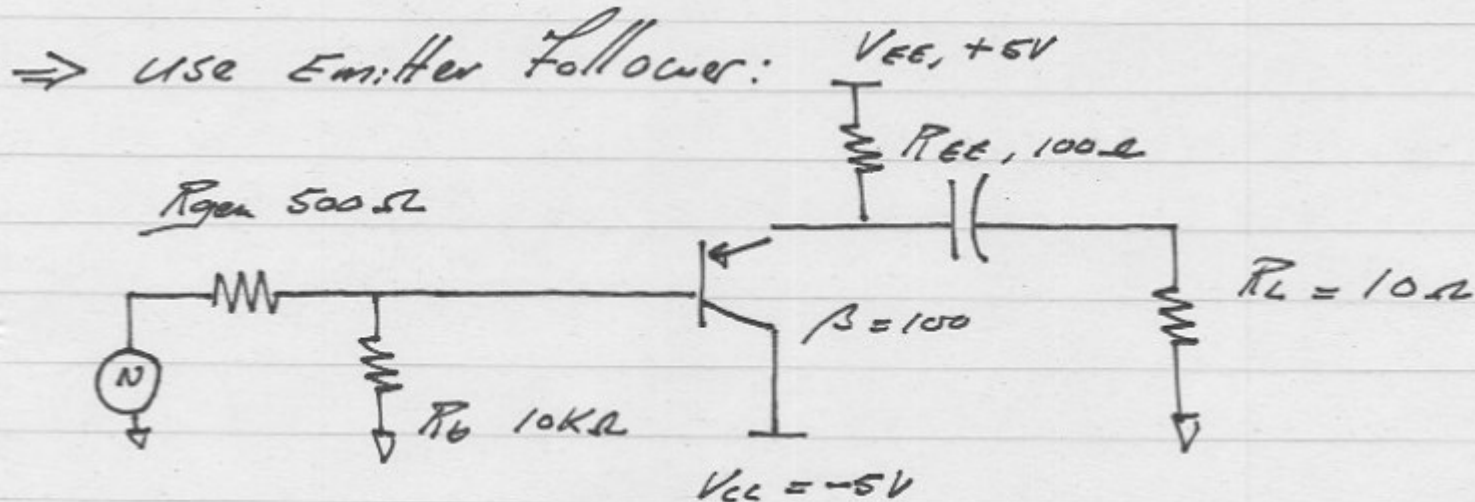


Follows from formulas earlier derived for emitter - degenerati on.

Emitter Follower: Example (1)



Emitter Follower: Example (2)



bias: guess $I_B \sim 0 \Rightarrow V_b = 0, V_E = 0.7V$ volts

$$\Rightarrow I_E = (5 - 0.7)V / 100\Omega = 43 \text{ mA}$$

$$\text{hence } I_B = 43 \text{ mA} / 100 = 430 \mu\text{A}$$

Repeat calculation:

$$V_b = 430 \mu\text{A} \cdot (500\Omega // 10k\Omega) = 0.143 \text{ V}$$

$$V_E = 0.143 + 0.7 = 0.843 \text{ V}$$

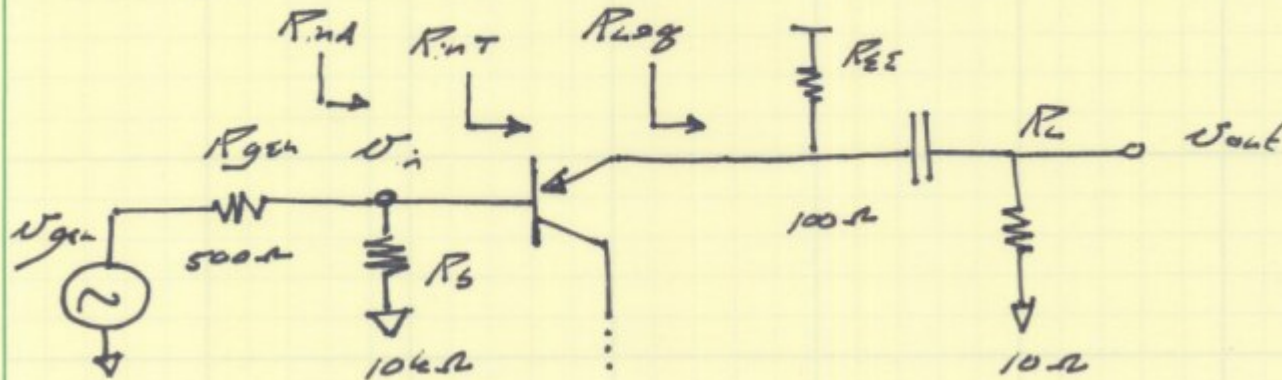
$$I_E = (5 - 0.843)V / 100\Omega = 41.6 \text{ mA}$$

$$I_B = 416 \mu\text{A}$$

Emitter Follower: Example (3)

Small signal analysis

$$r_e = 1/g_m = 26\text{mV} / 41.6\text{mA} = 0.63\ \Omega$$



$$R_{log} = 10\ \Omega \parallel 100\ \Omega = 9.09\ \Omega$$

$$v_{out}/v_{in} = R_{log} / (r_e + R_{log}) = 0.94$$

\downarrow
 $0.63\ \Omega$

$$R_{inT} = \beta (r_e + R_{log}) = 982\ \Omega$$

\downarrow \downarrow \downarrow
100 0.63 Ω 9.09 Ω

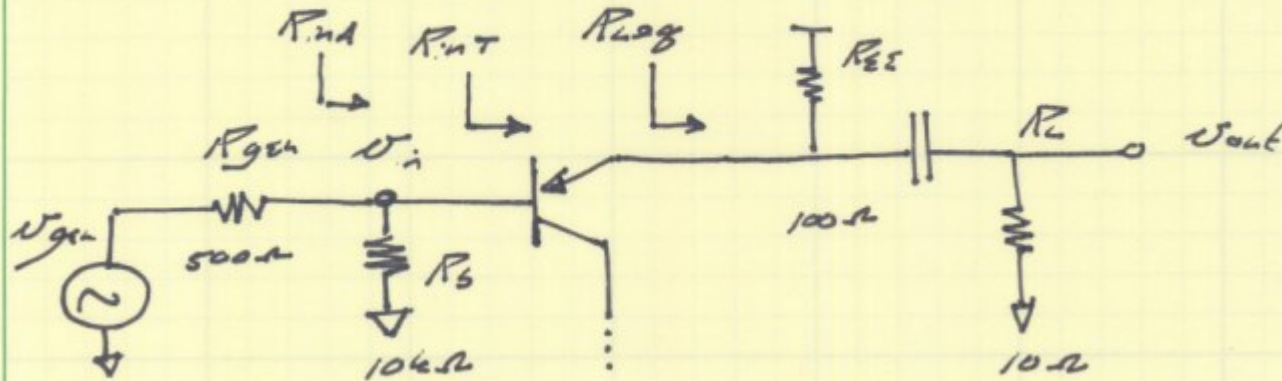
$$R_{inA} = R_b \parallel R_{inT} = 894\ \Omega$$

\downarrow \downarrow
10k Ω 982 Ω

Emitter Follower: Example (4)

small signal analysis

$$r_s = 1/g_m = 26\text{mV} / 41.6\text{mA} = 0.63\ \Omega$$

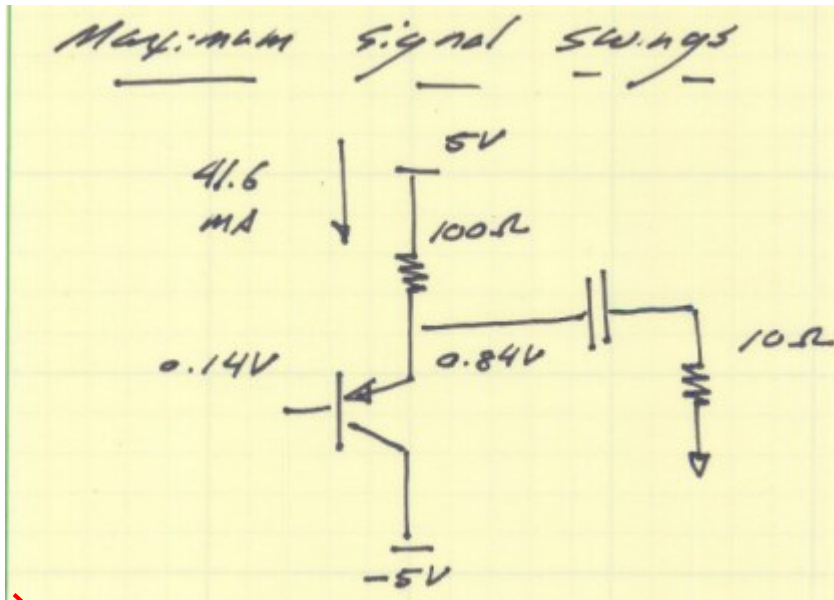


$$v_{in} / v_{gs} = R_{in} / (R_{in} + R_{gen}) = 0.64$$

$$v_o / v_{gs} = (v_o / v_{in}) \cdot (v_{in} / v_{gs}) = 0.94 \cdot 0.64 \approx 0.6$$

much more than 0.020

Emitter Follower: Example (5)



Saturation: $V_{CE} \approx 0.5V$

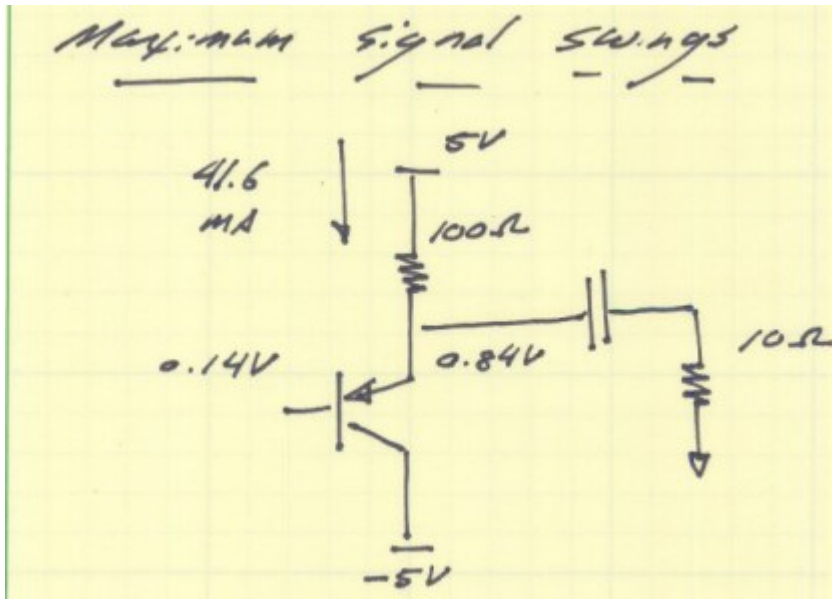
bias : $V_{CE} = 0.84V - (-5V) = 5.84V$

$$\Delta V_{CE} = 5.34V = \Delta V_C - \Delta V_E$$

\uparrow clearly zero \uparrow = ΔV_{out}

$$\Delta V_{out} = 5.34V \downarrow$$

Emitter Follower: Example (6)



bias: $I_C = 41.6 \text{ mA}$

cutoff $I_C = 0 \text{ mA}$

$\Delta I_C = 41.6 \text{ mA}$ (decrease)

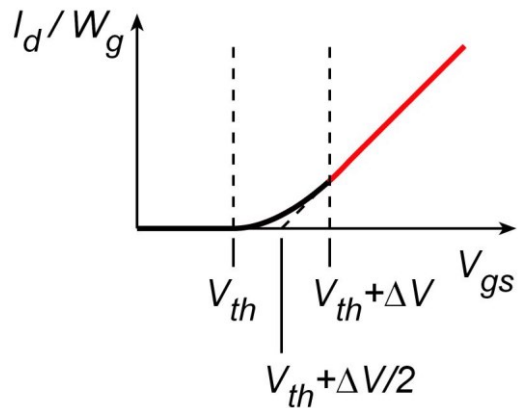
$$\Delta V_{out} = \Delta I_C \cdot R_{load}$$

$$= 41.6 \text{ mA} \cdot (10 \Omega \parallel 100 \Omega)$$

$$= 0.39 \text{ V} \uparrow$$

Source Follower Example (1)

Recall FET $I_D - V_{gs}$ characteristics in constant-current region

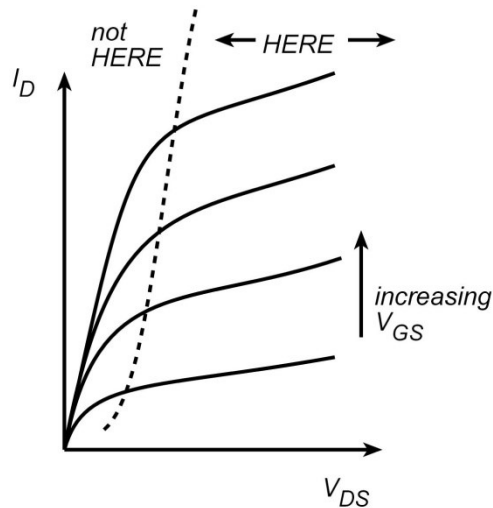


$$I_D \cong K_\mu (V_{gs} - V_{th})^2 (1 + \lambda V_{DS})$$

for $V_{gs} - V_{th} < \Delta V$, where $K_\mu = \mu c_{gs} W_g / 2L_g$

$$I_D \cong K_v (V_{gs} - V_{th} - \Delta V / 2)(1 + \lambda V_{DS})$$

for $V_{gs} - V_{th} > \Delta V$, where $K_v = v_{inj} c_{gs} W_g$



Device model: NMOS @ 15nm gate length

$$L_g = 15\text{nm}$$

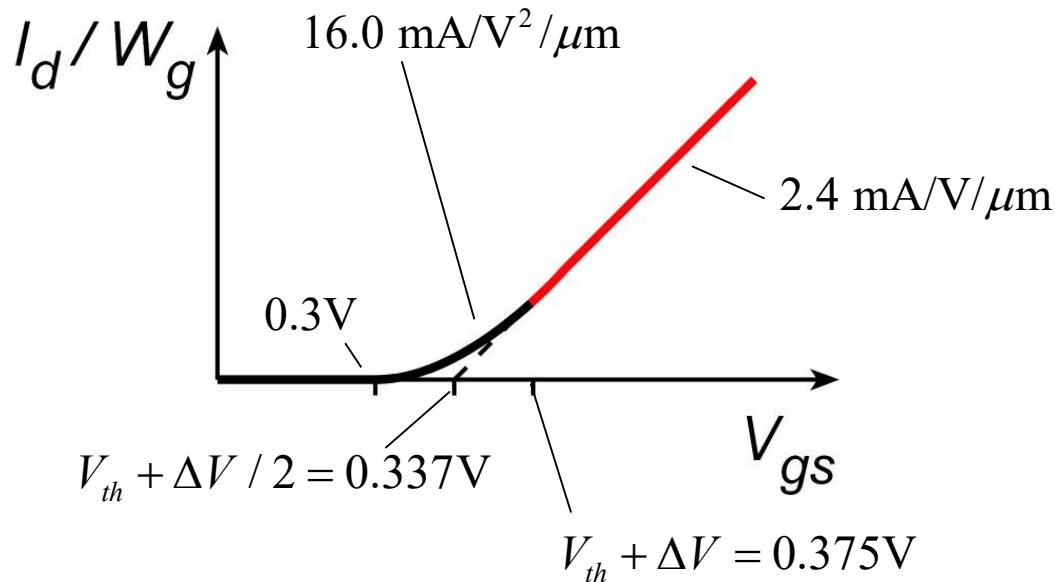
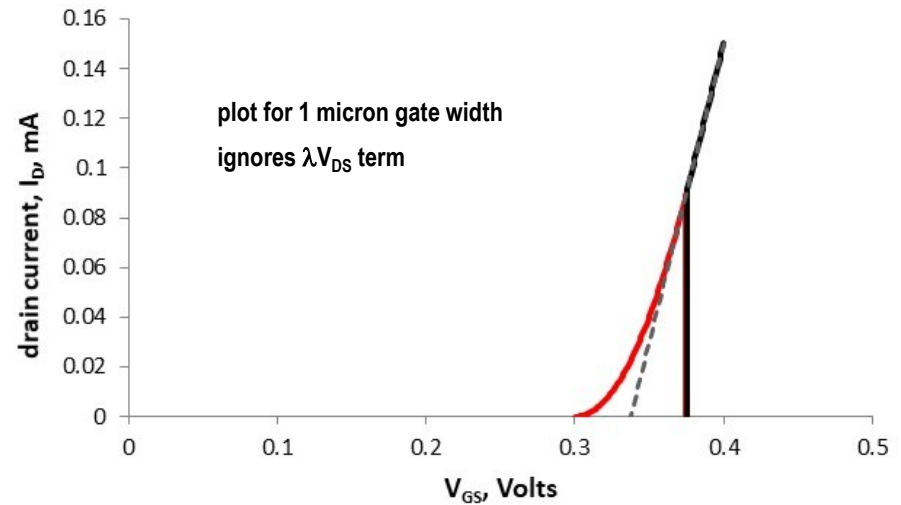
$$V_{th} = 0.3\text{ V}$$

$$K_\mu = 16\text{mA/V}^2 \cdot (W_g / 1\mu\text{m})$$

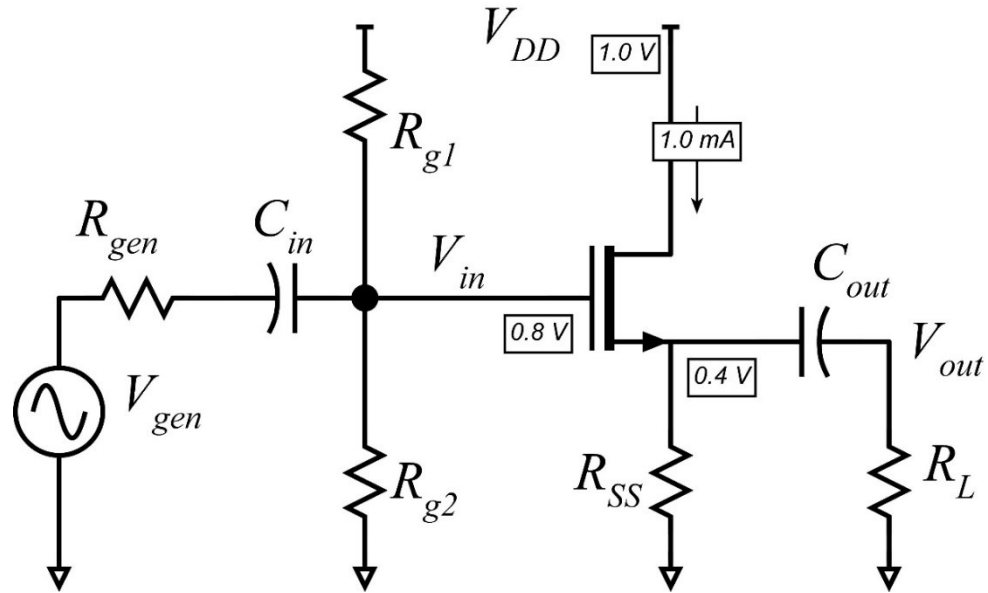
$$K_\nu = 2.40\text{mA/V} \cdot (W_g / 1\mu\text{m})$$

$$\Delta V = 75\text{mV}$$

$$1/\lambda = 5\text{V}$$



Source Follower Example (3)



We've chosen to bias the FET @ $V_{gs} - V_{th} = 0.4\text{V} - 0.3\text{V} = 0.1\text{V}$ and $V_{DS} = 0.6\text{V}$.

Velocity-limited: $I_D = 2.4\text{mA/V} \cdot (W_g / 1\mu\text{m})(V_{gs} - V_{th} - \Delta V / 2)(1 + \lambda V_{DS}) = 1\text{mA}$.

$1\text{mA} = 2.4\text{mA/V} \cdot (W_g / 1\mu\text{m})(0.1 - 75\text{mV})(1 + 0.6\text{V}/5\text{V}) \rightarrow W_g = 14.9\mu\text{m}$.

Setting $R_{g1} = 200\text{k}\Omega$ and $R_{g2} = 800\text{k}\Omega$ provides $V_g = 0.8\text{V}$.

$R_{SS} = 0.4\text{V}/1.0\text{mA} = 400\Omega$.

Source Follower Example (4)

AC small-signal analysis

$$\begin{aligned}
 g_m &= K_v (1 + \lambda V_{DS}) \\
 &= 2.4 \text{mA/V} \cdot \left(\frac{14.9 \mu\text{m}}{1 \mu\text{m}} \right) \left(1 + \frac{0.6 \text{V}}{5 \text{V}} \right) \\
 &= 40 \text{mS}.
 \end{aligned}$$

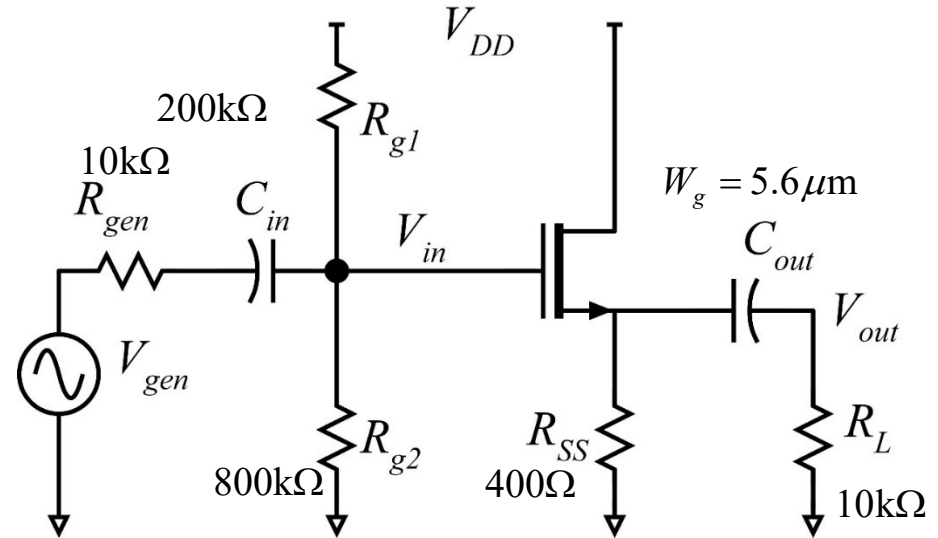
$$R_{DS} \cong 1 / \lambda I_D = 5 \text{V} / 1 \text{mA} = 5 \text{k}\Omega$$

$$R_{Leq} = R_{DS} \parallel R_{SS} \parallel R_L = 357 \Omega$$

$$V_{out} / V_{in} = R_{Leq} / (R_{Leq} + 1 / g_m) = 0.93$$

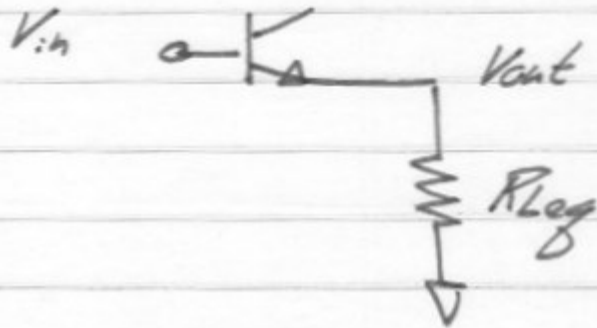
$$R_{in,A} = 200 \text{k}\Omega \parallel 800 \text{k}\Omega = 160 \text{k}\Omega$$

$$V_{in} / V_{gen} = R_{in,A} / (R_{in,A} + R_{gen}) = 0.94$$



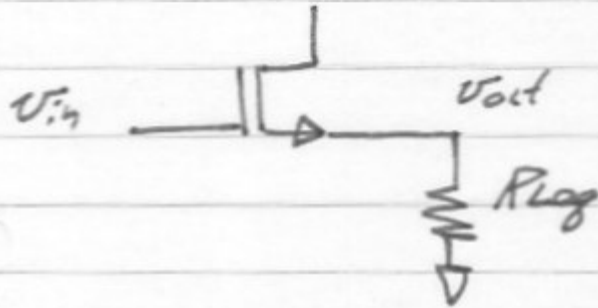
Emitter Followers vs Source Followers

Note that with emitter follower:



$$\frac{V_{out}}{V_{in}} = \frac{R_{EG}}{\beta} = \frac{R_{EG}}{R_{EG} + 1/g_m}$$

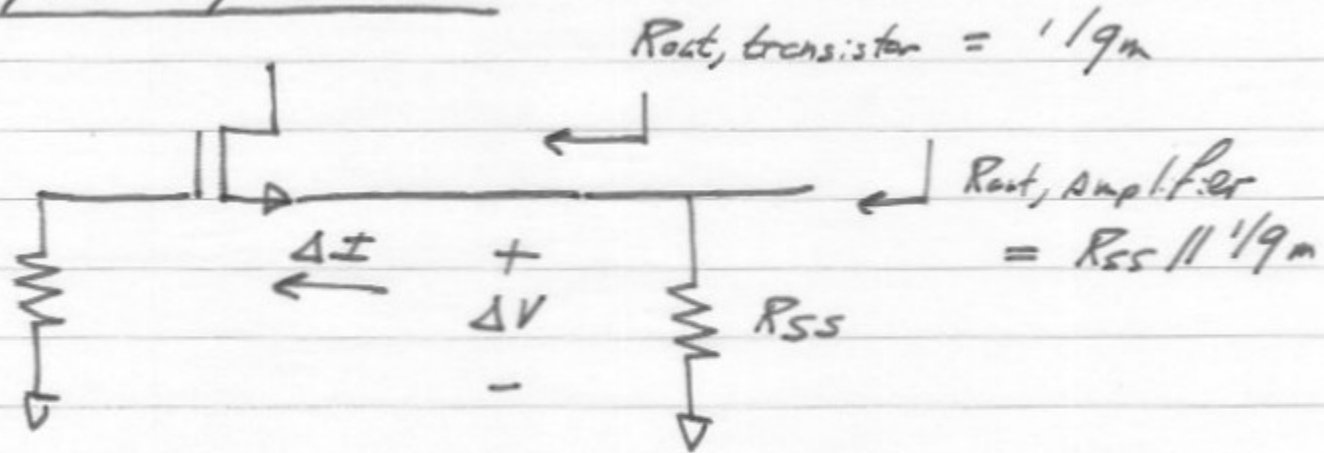
Since the MOSFET has the same s.s. model:



$$\frac{V_{out}}{V_{in}} = \frac{R_{EG}}{R_{EG} + 1/g_m}$$

Source Follower Output Impedance

Output impedance:



why is $r_{out, transistor} = 1/g_m$??

$$\begin{aligned}
 (r_{out, transistor})^{-1} &\triangleq \Delta I / \Delta V = \Delta I_s / \Delta V_{gs} \\
 &= g_m \quad \nabla
 \end{aligned}$$

More carefully working from the s.s. model shows that $R_{out,T} = (1/g_m) \parallel R_{DS}$