

# ECE 137 B: Notes Set 15

## Feedback with finite, nonzero port impedances

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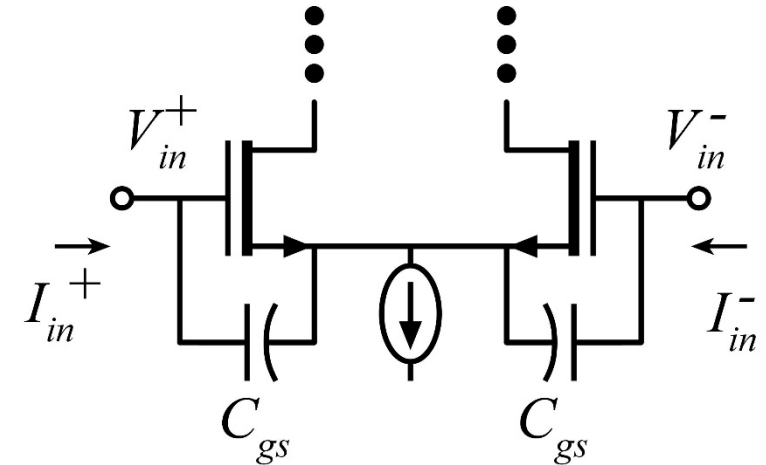
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# Models of feedback amplifier input stages

Elementary treatment: ignore  $C_{gd}$  to simplify analysis.

$$I_{in}^+ = -I_{in}^- = I_{in} = (V_{in}^+ - V_{in}^-)(1/sC_{gs} + 1/sC_{gs})^{-1} = (V_{in}^+ - V_{in}^-)(sC_{gs}/2)$$

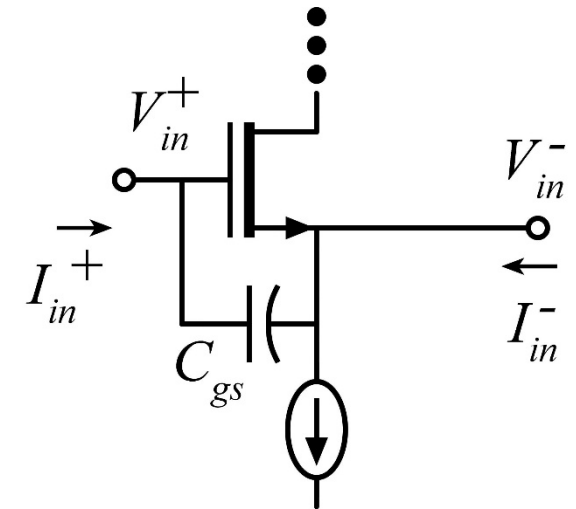
$$I_{in} = Y_{in}(V_{in}^+ - V_{in}^-) = sC_{in}(V_{in}^+ - V_{in}^-) \text{ where } Y_{in} = sC_{in} \text{ and } C_{in} = C_{gs}/2$$



$$I_{in}^+ = (V_{in}^+ - V_{in}^-)sC_{gs} = Y_{in}^+(V_{in}^+ - V_{in}^-) \text{ where } Y_{in}^+ = sC_{in} \text{ and } C_{in} = C_{gs}$$

$$I_{in}^- = (g_m + sC_{in})(V_{in}^- - V_{in}^+) = Y_{in}^-(V_{in}^- - V_{in}^+) \text{ where } Y_{in}^- = (g_m + sC_{in})$$

**Key point:**  $I_{in}^+ \neq -I_{in}^-$



# Model and analysis of Feedback Amplifier (1)

Nodal analysis:  $\Sigma I = 0$  at  $V_{in}^-$ :

$$V_{in}^- (Y_1 + Y_2 + Y_{in}^-) + V_{out} (-Y_2) + V_{in}^- (-Y_{in}^-) = 0$$

also:

$$V_{out} = A_{OL} (V_{in}^+ - V_{in}^-) \rightarrow V_{in}^- = V_{in}^+ - V_{out} / A_{OL} = V_{in} - V_{out} / A_{OL}$$

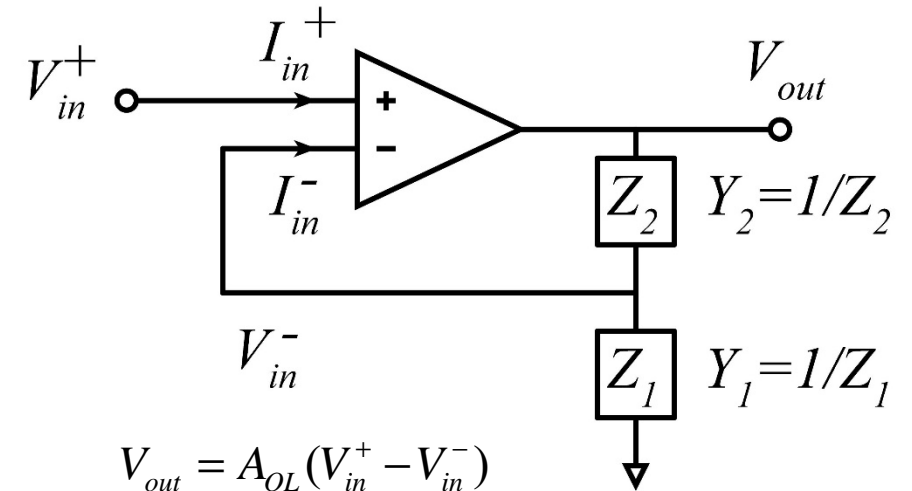
Now combine these two equations and solve:

$$(V_{in} - V_{out} / A_{OL})(Y_1 + Y_2 + Y_{in}^-) + V_{out} (-Y_2) + V_{in}^- (-Y_{in}^-) = 0$$

$$V_{in} (Y_1 + Y_2) + V_{out} \left( -\frac{Y_1 + Y_2 + Y_{in}^-}{A_{OL}} - Y_2 \right) = 0$$

$$V_{in} (Y_1 + Y_2) = V_{out} \left( \frac{Y_1 + Y_2 + Y_{in}^-}{A_{OL}} + Y_2 \right) = V_{out} Y_2 \left( \frac{Y_1 + Y_2 + Y_{in}^-}{Y_2 A_{OL}} + 1 \right)$$

$$\frac{V_{out}}{V_{in}} = \frac{Y_1 + Y_2}{Y_2} \frac{1}{\left( \frac{Y_1 + Y_2 + Y_{in}^-}{Y_2 A_{OL}} + 1 \right)} = \frac{Y_1 + Y_2}{Y_2} \frac{\left( A_{OL} \frac{Y_2}{Y_1 + Y_2 + Y_{in}^-} \right)}{\left( 1 + A_{OL} \frac{Y_2}{Y_1 + Y_2 + Y_{in}^-} \right)}$$



$$V_{out} = A_{OL} (V_{in}^+ - V_{in}^-)$$

$$I_{in}^+ = Y_{in}^+ (V_{in}^+ - V_{in}^-)$$

$$I_{in}^- = Y_{in}^- (V_{in}^- - V_{in}^+)$$

$Y_{in}^-$  may or may not be equal to  $Y_{in}^+$

# Model and analysis of Feedback Amplifier (2)

We want an expression we can recognize.

We are looking for expressions similar to  $T / (1+T)$ , so...

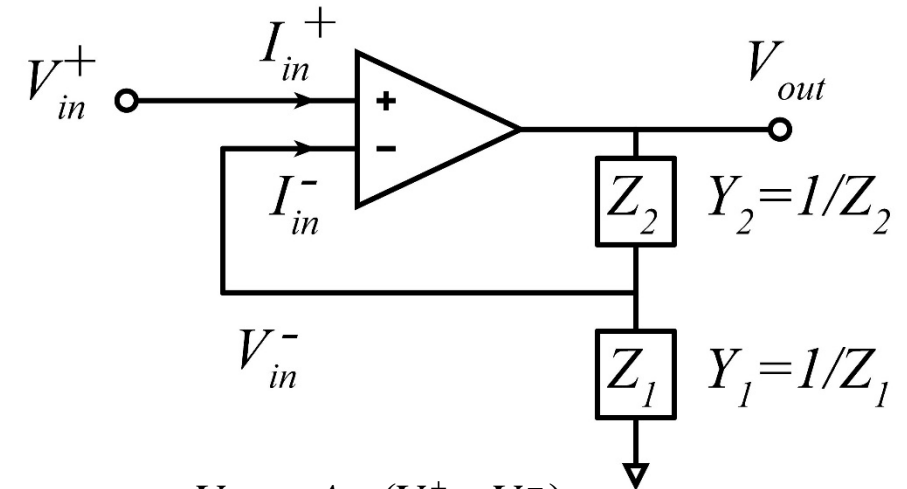
$$\frac{V_{out}}{V_{in}} = \frac{Z_1 + Z_2}{Z_1} \frac{A_{OL} \left( \frac{Y_2}{Y_1 + Y_2 + Y_{in}^-} \right)}{1 + A_{OL} \left( \frac{Y_2}{Y_1 + Y_2 + Y_{in}^-} \right)}$$

Calculate the voltage divider between  $V_{out}$  and  $V_{in}^-$ :

$$\frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_2} = \frac{\left( \frac{1}{Y_1 + Y_{in}^-} \right)}{\left( \frac{1}{Y_1 + Y_{in}^-} \right) + \left( \frac{1}{Y_2} \right)} = \frac{Y_2}{Y_1 + Y_2 + Y_{in}^-}$$

So:

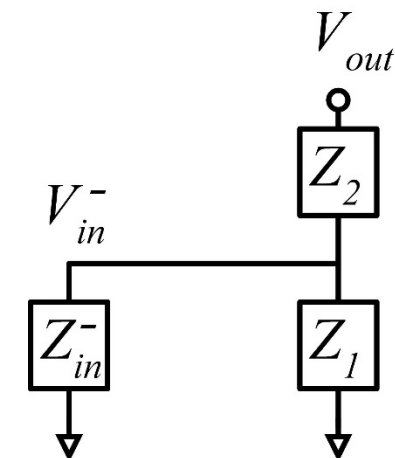
$$\frac{V_{out}}{V_{in}} = \frac{Z_1 + Z_2}{Z_1} \frac{A_{OL} \left( \frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_2} \right)}{1 + A_{OL} \left( \frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_2} \right)}$$



$$V_{out} = A_{OL} (V_{in}^+ - V_{in}^-)$$

$$I_{in}^+ = Y_{in}^+ (V_{in}^+ - V_{in}^-)$$

$$I_{in}^- = Y_{in}^- (V_{in}^- - V_{in}^+)$$



# Model and analysis of Feedback Amplifier (3)

Compare our answer to  $A_{\infty} \frac{T}{1+T}$ :

To compute  $T$ , unwrap the feedback loop,  
and compute gain from the point  $TV_{test}$  to the point  $T^2V_{test}$

$$\rightarrow T = A_{OL} \left( \frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_2} \right)$$

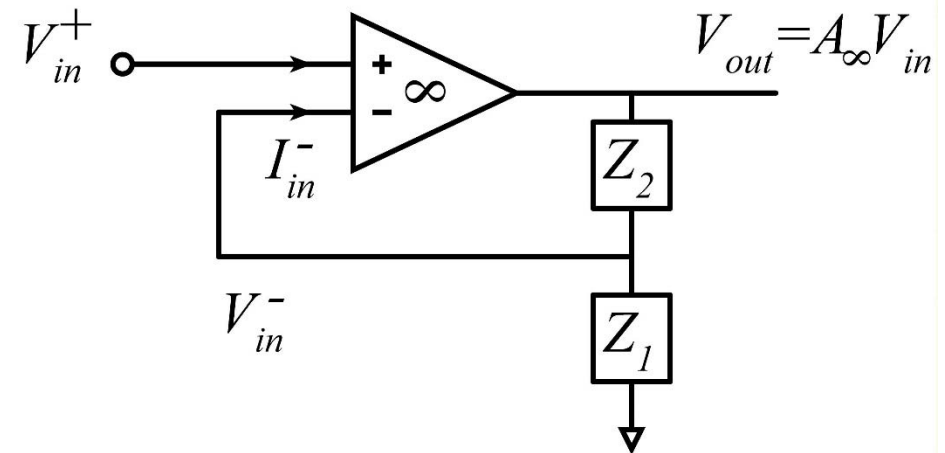
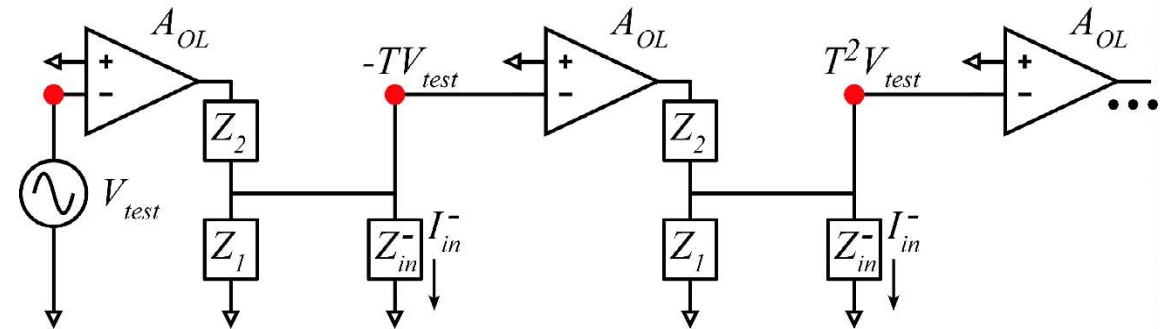
To compute  $A_{\infty}$ , assume  $A_{OL} = \infty$  and compute  $V_{out} / V_{in}$ :

$$A_{\infty} = \frac{V_{out}}{V_{in}} \Big|_{\text{infinite } A_{OL}} = \frac{Z_1 + Z_2}{Z_1}$$

So, we have shown that

$$A_{CL} = \frac{Z_1 + Z_2}{Z_1} \frac{A_{OL} \left( \frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_2} \right)}{1 + A_{OL} \left( \frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_2} \right)} = A_{\infty} \frac{T}{1+T}$$

...shown given (1)  $Z_{out} = 0\Omega$  and (2) voltage-sense, voltage sum feedback



# Formula for the other three cases

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We have shown that

$$A_{CL} = A_{\infty} \frac{T}{1+T}$$

...given (1)  $Z_{out} = 0\Omega$  and (2) voltage-sense, voltage sum feedback.

We have not considered

voltage-sense, current sum

current-sense, voltage sum

current-sense, current sum.

...I will leave these as exercises to the reader.

# Model with finite output impedance

Nodal analysis:  $\Sigma I = 0$  at  $V_{in}^-$ :

$$V_{in}^-(Y_1 + Y_2 + Y_{in}^-) + V_{out}(-Y_2) + V_{in}^-(Y_{in}^-) = 0$$

Nodal analysis:  $\Sigma I = 0$  at  $V_{out}$ :

$$V_{out}(Y_{out} + Y_2) + V_{in}^-(Y_2) + A_{OL}(V_{in}^+ - V_{in}^-)(-Y_{out}) = 0$$

From our earlier calculation, treating  $V_x$  as a feedback amplifier output:

$$\frac{V_x}{V_{in}^+} = \frac{Z_1 + Z_2 + Z_{out}}{Z_1} \frac{A_{OL}\beta}{1 + A_{OL}\beta} \quad \text{where } \beta = \frac{Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_{out} + Z_2}$$

$$\text{also } V_{out} = \frac{Z_2 + Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_{out} + Z_2} V_x + \frac{Z_{out}}{Z_{out} + Z_2} \frac{(Z_{out} + Z_2) \parallel Z_1}{Z_{in}^- + (Z_{out} + Z_2) \parallel Z_1} V_{in}^+$$

So

$$\frac{V_{out}}{V_{in}^+} = \frac{Z_1 + Z_2 + Z_{out}}{Z_1} \frac{Z_2 + Z_1 \parallel Z_{in}^-}{Z_1 \parallel Z_{in}^- + Z_{out} + Z_2} \frac{T}{1 + T} \quad \dots \text{forward gain term}$$

$$+ \frac{Z_{out}}{Z_{out} + Z_2} \frac{(Z_{out} + Z_2) \parallel Z_1}{Z_{in}^- + (Z_{out} + Z_2) \parallel Z_1} V_{in}^+ \quad \dots \text{feed forward through feedback loop}$$

