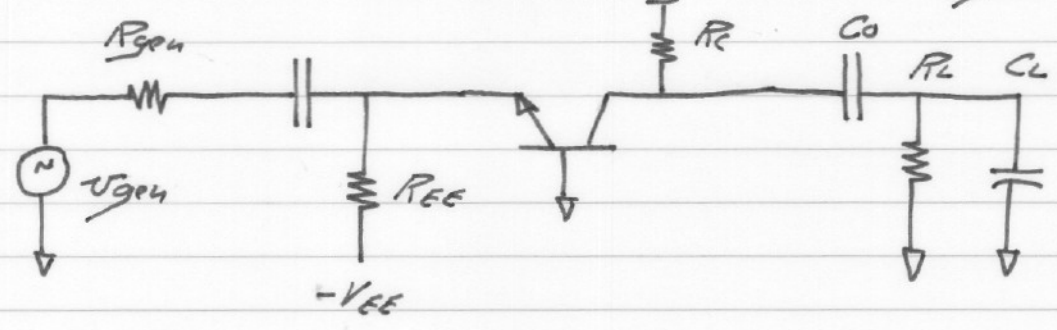
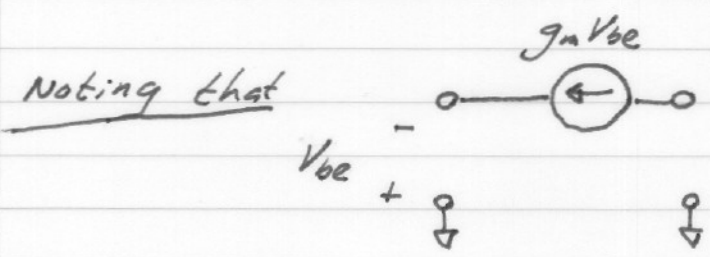
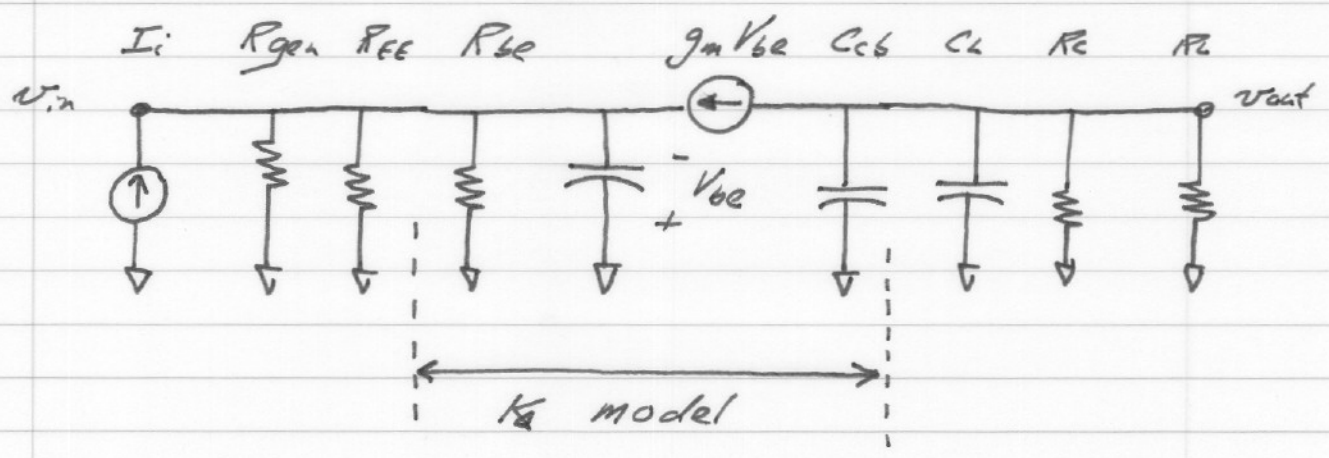


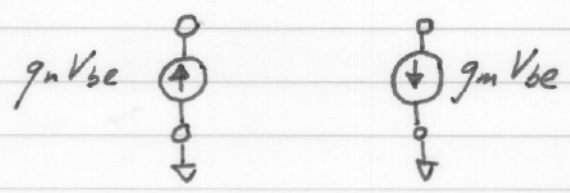
ECE137B Notes set 5: CB & CG stages:



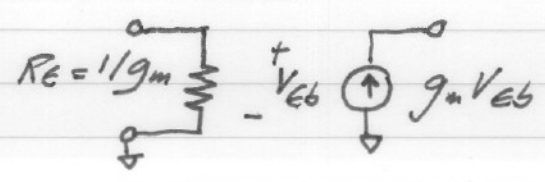
we will neglect  $R_{EE}$  in h.f. analysis; usually negligible effect unless  $R_L$  is very large.



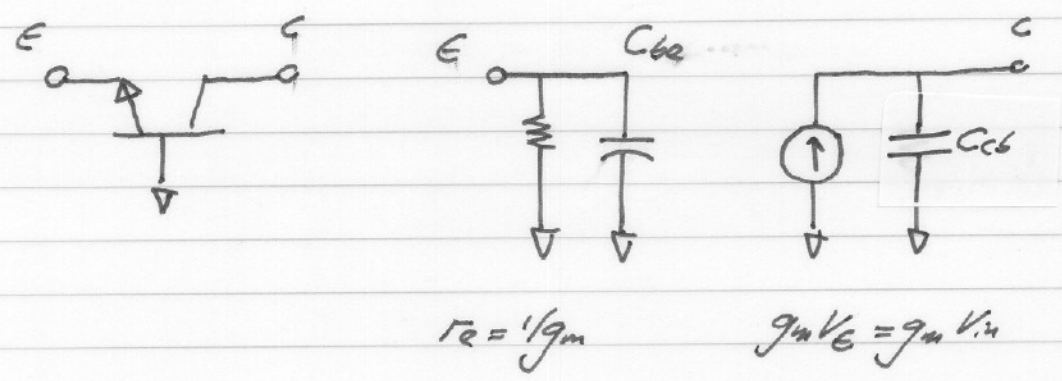
is exactly equivalent to



which in turn transforms to

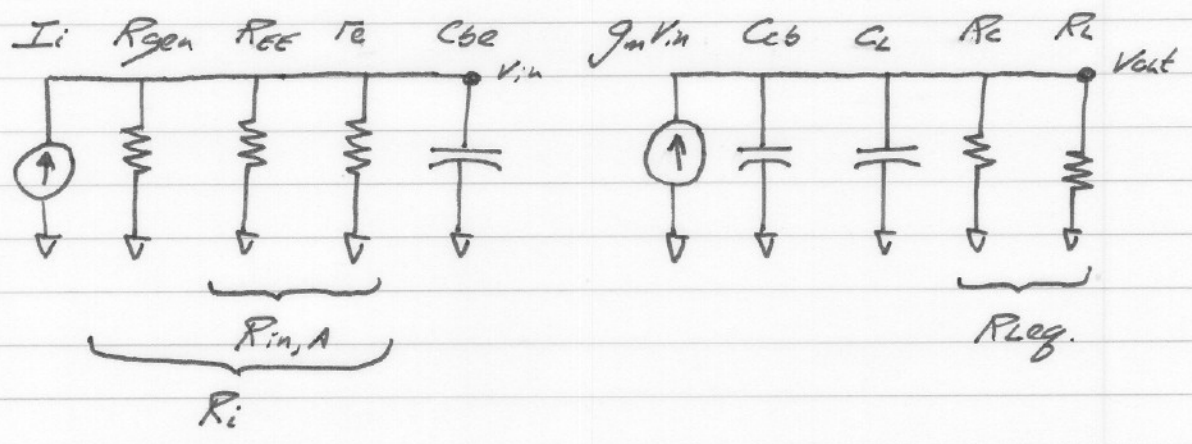


we can model the common-base K<sub>e</sub> as so:



This is the common-base T-model

using the T-model, the circuit is modeled thus

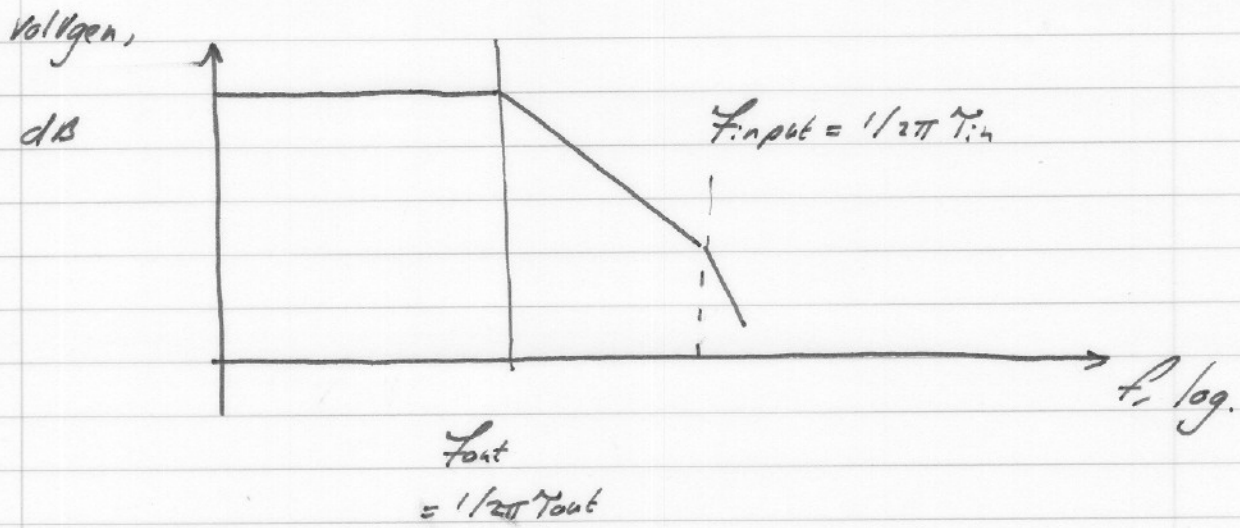


$$v_i/v_{gen} = v_{in}/v_{gen} / m_{\beta} \cdot \frac{1}{1 + A T_{in}} ; T_{in} = R_i \cdot C_{be}$$

$$v_o/v_i = v_o/v_{in} / m_{\beta} \cdot \frac{1}{1 + A T_{out}} ; T_{out} = (C_{cb} + C_L) R_{eq}$$

Analysis is much more complex if  $R_{bb}$  is included.

(3)



Note  $f_{input} = 1/2\pi T_{in} \Rightarrow$  is higher than  $f_T$ !

Model is only good up to  $f_T \rightarrow$

input pole "somewhere around  $f_T$ "

To the level we have analyzed it, the c.b. stage.

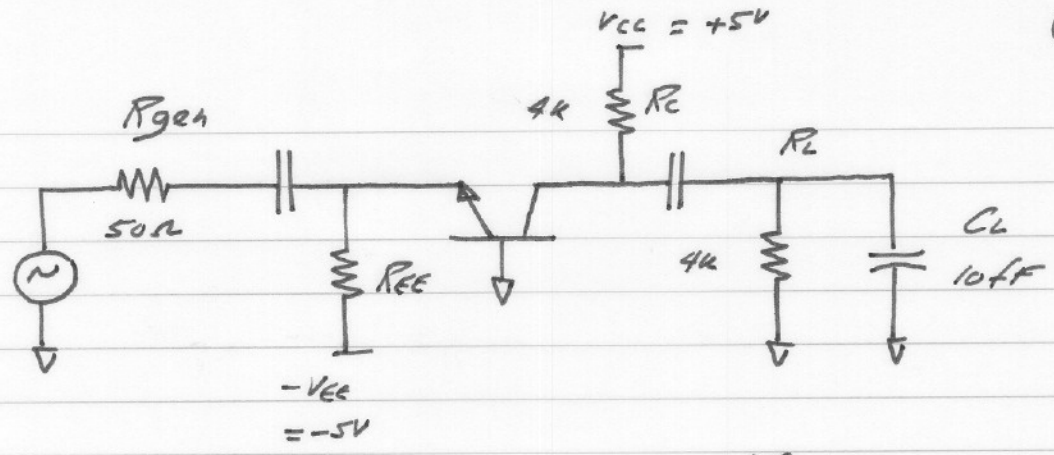
- is limited by the output pole
- has no interaction between input & output.
- is simple to analyze.

However, the effect of  $R_{ob}$ , neglected for simplicity, is in fact large and seriously affects c.b. bandwidth.

This is mostly beyond the scope of the course,

although it can be analyzed by the M.O.T.C., to be covered later.

(4)



h<sub>e</sub> parameters       $V_A = \infty V$ ,  $\beta = 200$ ,  $f_T = 100 \text{ GHz}$ ,  $C_{cb} = 10 \text{ fF}$   
 $V_{BE} = 0.9 \text{ V}$  @  $I_E = 1 \text{ mA}$

BIAS

$$I_E = 5.9 \text{ V} / R_{EE} = 1 \text{ mA} \rightarrow R_{EE} = 5.9 \text{ k}\Omega$$

$$V_C = V_{CC} - I_C R_C = +1 \text{ V}$$

Low Frequency analysis

$$R_{Log} = R_C \parallel R_L = 2 \text{ k}\Omega$$

$$r_e = 1/g_m = 26 \Omega$$

$$r_{int} = r_e = 26 \Omega$$

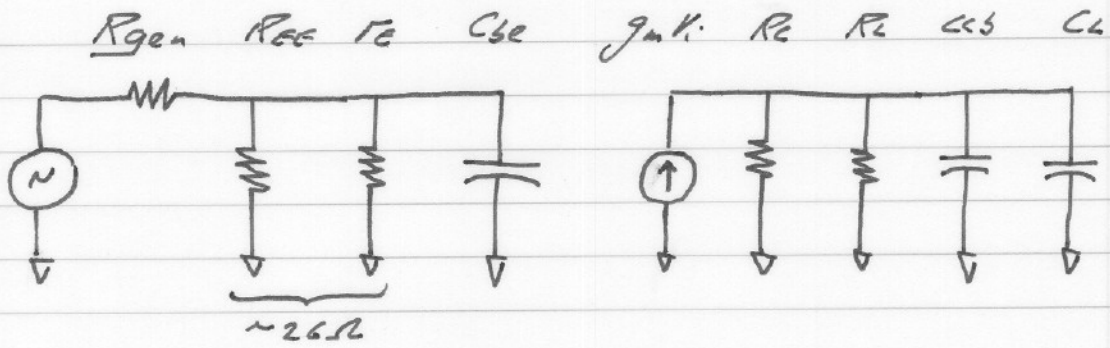
$$v_o/v_i /_{AB} = R_{Log} / r_{int} = 77$$

$$r_{inA} = r_{int} \parallel R_{EE} = 25.9 \Omega \approx 26 \Omega$$

$$v_{in}/v_{gen} = r_{inA} / (r_{inA} + r_{gen}) = 0.34$$

$$v_o/v_{gen} = 26.3$$





$$C_{be} = \frac{g_m}{2\pi f_T} - C_{cb} = 51 \text{ fF}$$

$$f_{inpt} = 1/2\pi T_{in}; \quad T_{in} = C_{be} (R_{gen} \parallel R_{EE} \parallel r_e)$$

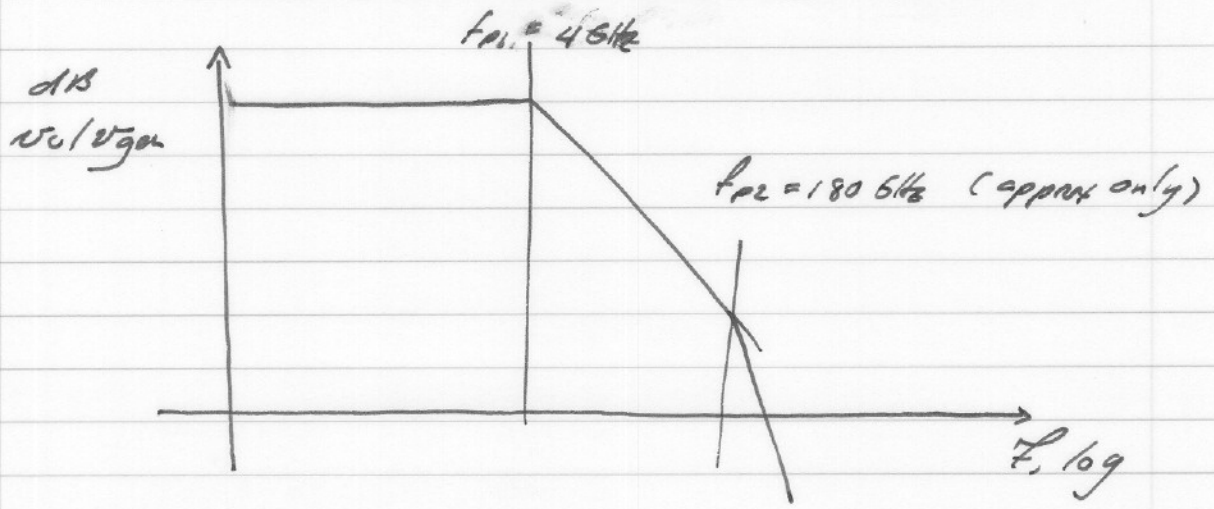
$$= 51 \text{ fF} \cdot 17.1 \Omega = 0.87 \text{ ps}$$

$$= 180 \text{ GHz}$$

→ higher than  $f_T$ ; not realistic.

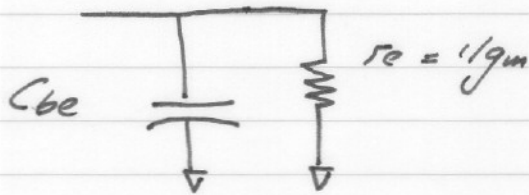
$$f_{outpt} = 1/2\pi T_{out}; \quad T_{out} = R_{log} (C_{cb} + C_L)$$

$$= 4.0 \text{ GHz} \quad = 40 \text{ ps}$$



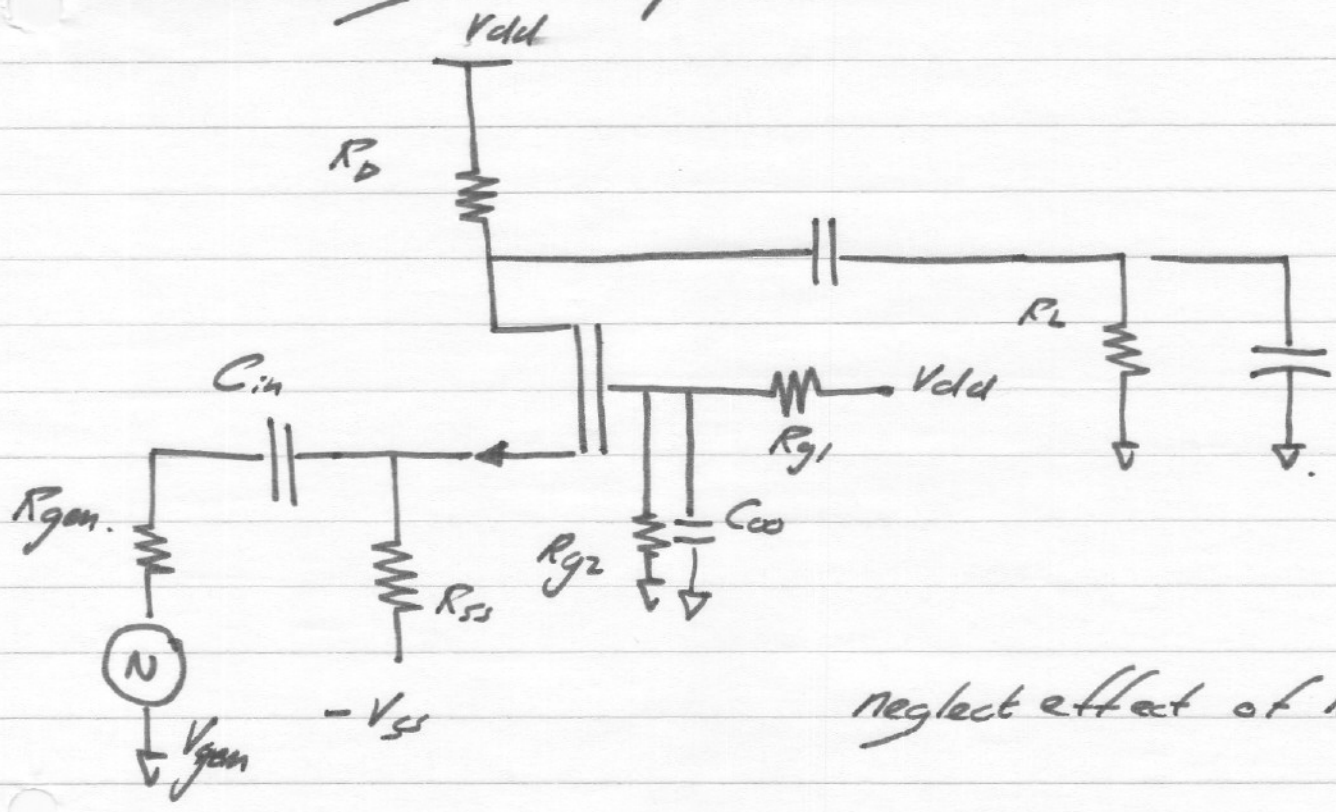
6

Input impedance of  $\beta$  in common-base

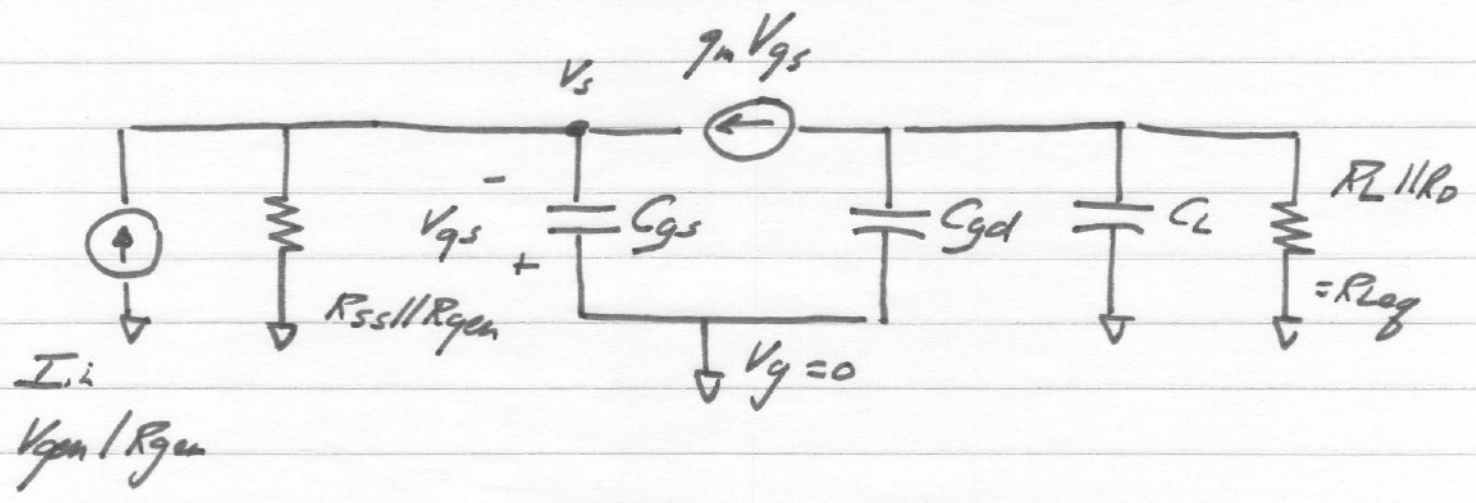


\* the impedance (1) changes greatly due to the effect of  $R_{bb}$ , and (2) in 137B we ignore the phase shift of the common-emitter hybrid- $\pi$  transconductance... this also changes  $Z_{in}$  at high frequencies.

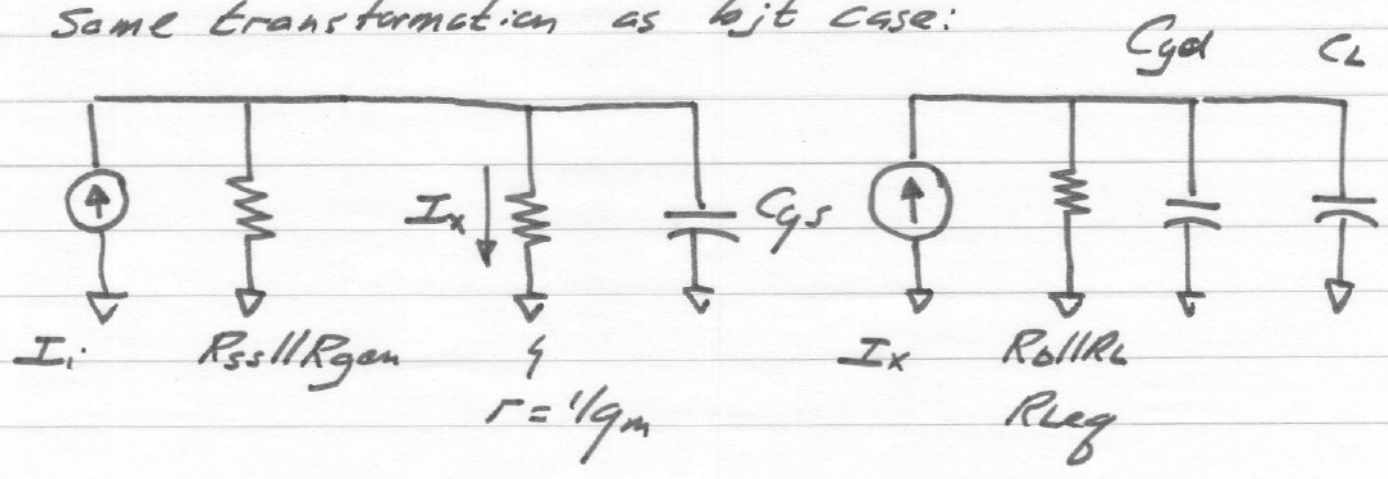
# Common-gate amplifier



neglect effect of  $R_{ds}^*$



same transformation as bjt case:



2 poles in transfer function.

one at  $f = 1/2\pi\tau_{in}$ , where  $\tau_{in} = R \cdot C$   
 $R = (1/g_m) || R_{ss} || R_{gen}$   
 $C = C_{gs}$

one at  $f = 1/2\pi\tau_{out}$ , where  $\tau_{out} = R \cdot C$

~~$R = (1/g_m) || R_{ss} || R_{gen}$~~   $R = R_{leg} = R_0 || R_L$

$C = C_{gd} + C_L$