

**ECE ECE145A (undergrad) and ECE218A (graduate)**

**Final Exam. Tuesday, December 10, 12-3 p.m.**

Do not open exam until instructed to.

Open notes, open books, etc. You have 3 hrs.

Use all reasonable approximations (5% accuracy is fine. ),

***AFTER STATING and justifying THEM.***

***Think before doing complex calculations. Sometimes there is an easier way.***

Problem	Points Received	Points Possible
1a		5
1b		5
1c		5
1d		5
1e		5
1f		5
2		10
3		10
4a		5
4b		5
5a		5
5b		5
5c		10
6a		10
6b		10
total		100

Name: Solution

$$G_T = \frac{|S_{21}|^2 (1-|\Gamma_s|^2)(1-|\Gamma_L|^2)}{|(1-\Gamma_s S_{11})(1-\Gamma_L S_{22}) - S_{21} S_{12} \Gamma_s \Gamma_L|^2} \quad G_P = \frac{1}{1-\|\Gamma_m\|^2} \cdot |S_{21}|^2 \cdot \frac{1-|\Gamma_L|^2}{|1-\Gamma_L S_{22}|^2}$$

$$G_a = \frac{1-|\Gamma_s|^2}{|1-\Gamma_s S_{11}|^2} \cdot |S_{21}|^2 \cdot \frac{1}{1-\|\Gamma_{out}\|^2} \quad G_{max} = \frac{|S_{21}|}{|S_{12}|} \cdot [K - \sqrt{K^2 - 1}] \text{ if } K > 1$$

$$G_{MS} = \frac{|S_{21}|}{|S_{12}|} \cdot \text{if } K < 1 \quad K = \frac{1-|S_{11}|^2 - |S_{22}|^2 + |\Delta|^2}{2|S_{21} S_{12}|} \quad \text{where } \Delta = \det[S]$$

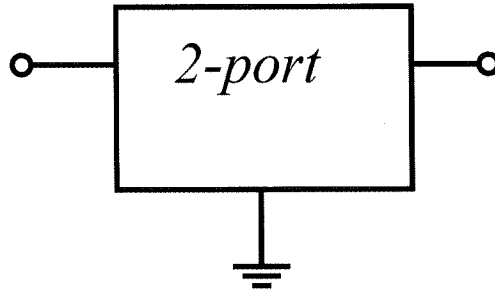
Unconditionally stable if : (1)  $K > 1$  and (2)  $\|\det[S]\| < 1$



**Problem 1, 30 points**

*gain definitions*

At a signal frequency of 1 GHz, a two-port has  $S_{11} = 0.6$ ,  $S_{12} = 1/4$ ,  $S_{21} = 2$  and  $S_{22} = 0$ , as defined with a 50 Ohm impedance reference.



part a, 5 points

If the 2-port were directly connected to 50 Ohm load, and a 50 Ohm generator with 10 mW available power, what would be the power dissipated in the load ?

2 [ this is insertion gain

2 [  $P_L = |S_{21}|^2 \cdot P_{avg}$

1 [  $= 4 \cdot 10 \text{ mW} = 40 \text{ mW}$ .

part b, 5 points

If the load is an open circuit (infinity Ohms), then what is the input impedance?

$$2 \left[ Z_{in} = S_{11} + \frac{S_{12} S_{21} Z_L}{1 - S_{22} Z_L} \right]$$

$$1 \left[ \begin{aligned} &= 0.6 + \frac{(2)(1)(4)(1)}{1 - 0.1} \\ &= 0.6 + 0.5 = 1.1 \end{aligned} \right]$$

$$1 \left[ Y_{in} = \frac{1 + Z_{in}}{1 - Z_{in}} = \frac{2.1}{-0.1} = -21 \right]$$

$$1 \left[ Z_{in} = -21 \text{ } 50\Omega = -1050\Omega \text{ negative} \right]$$

(c)  $\square$  network is potentially unstable

part c, 5 points

If you were to first stabilize (if necessary) and then impedance match the input and output to 50 Ohms, and drive the input with generator of 10mW available power, what would be the power delivered to the load ?

2 [ since the network is potentially unstable, after doing the above, the amplifier will have a <sup>power</sup> gain equal to the transistor MSG.

2 [  $Gain = MSG = |S_{21}| / |S_{12}| = 8$

1 [  $P_{load} = 8 \cdot 10mW = 80mW$ .

part d, 5 points

If you were to load the 2-port, without matching or stabilization elements, with a 150 Ohm load, is it possible to select a generator impedance which would cause the 2-port to oscillate?

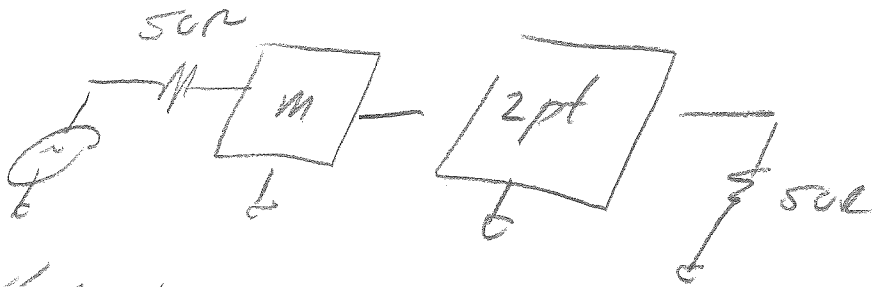
$$\begin{aligned} 1 & \left[ \begin{aligned} Z_L &= 150 \Omega \\ \Gamma_L &= 3 \\ \Gamma_{in} &= \frac{\Gamma_L - 1}{\Gamma_L + 1} = \frac{3 - 1}{3 + 1} = 1/2 \end{aligned} \right. \\ 2 & \left[ \begin{aligned} \Gamma_{in} &= S_{11} + \frac{S_{12} S_{21} \Gamma_L}{1 - S_{22} \Gamma_L} = \\ &= 0.6 + \frac{(2)(1/4) \cdot 1/2}{1} = 0.6 + 0.25 \\ &= 0.85 < 1 \end{aligned} \right. \\ 1 & \left[ \right. \end{aligned}$$

the input reflection coefficient is less than 1 in magnitude.

cannot oscillate with any generator impedance.

part e. 5 points

If you were to load the 2-port, without stabilization elements, in 50 Ohms, and then impedance-match the input to a 50 Ohm generator with 10mW available source power, what would be the power in the load ?



note, that because  $\Gamma_{out} \neq S_{22}$ , we are not matched on the output. But, we are on the input

$\Rightarrow$  operating gain!

$$G_T = \frac{1}{1 - |\Gamma_{in}|^2} |S_{21}|^2 \frac{1 - |\Gamma_L|^2}{1 - |\Gamma_L S_{22}|^2}$$

where  $\Gamma_L = S_{11} + \frac{S_{21} S_{12} \Gamma_L}{1 - S_{22} \Gamma_L} = S_{11}$   
 note  $\Gamma_L = 0$

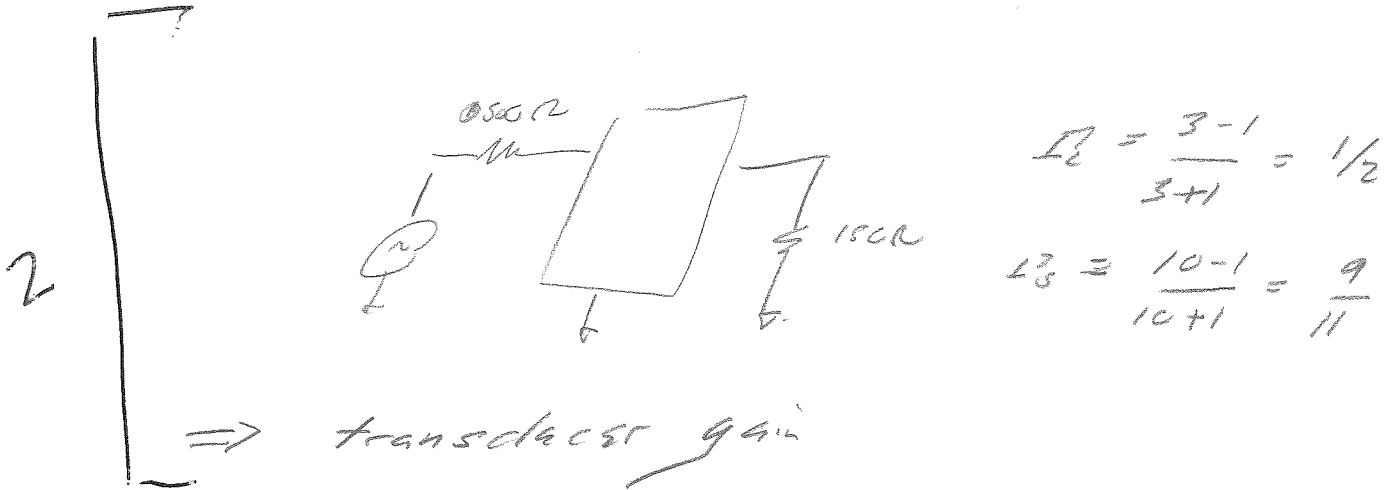
$$G_T = \frac{1}{1 - \|S_{11}\|^2} \|S_{21}\|^2$$

$$= \frac{4}{1 - (0.6)^2} = \frac{4}{1 - 0.36} = \dots = 6.25$$

$$P_{load} = \frac{62.5 \mu W}{1}$$

part f, 5 points

If you were to take the 2-port, without stabilization elements, connect the input directly to a 500 Ohm generator with 10mW available source power, and then connect the output directly to a 150 Ohm load, what would be the power in the load ?



2

$$G_T = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2) (1 - |\Gamma_L|^2)}{(1 - \Gamma_S S_{11})(1 - \Gamma_L S_{22}) - S_{21} S_{12} \Gamma_S \Gamma_L} / Z$$

$$= \frac{4 (1 - (9/11)^2) (1 - 1/4)}{1 (1 - 9/11 \cdot 0.6) - 1 - 2 (1/4) \cdot 1/2 \cdot 9/11} / Z$$

1

$$= \frac{4 (0.331) (0.75)}{0.5 - 0.284} / Z$$

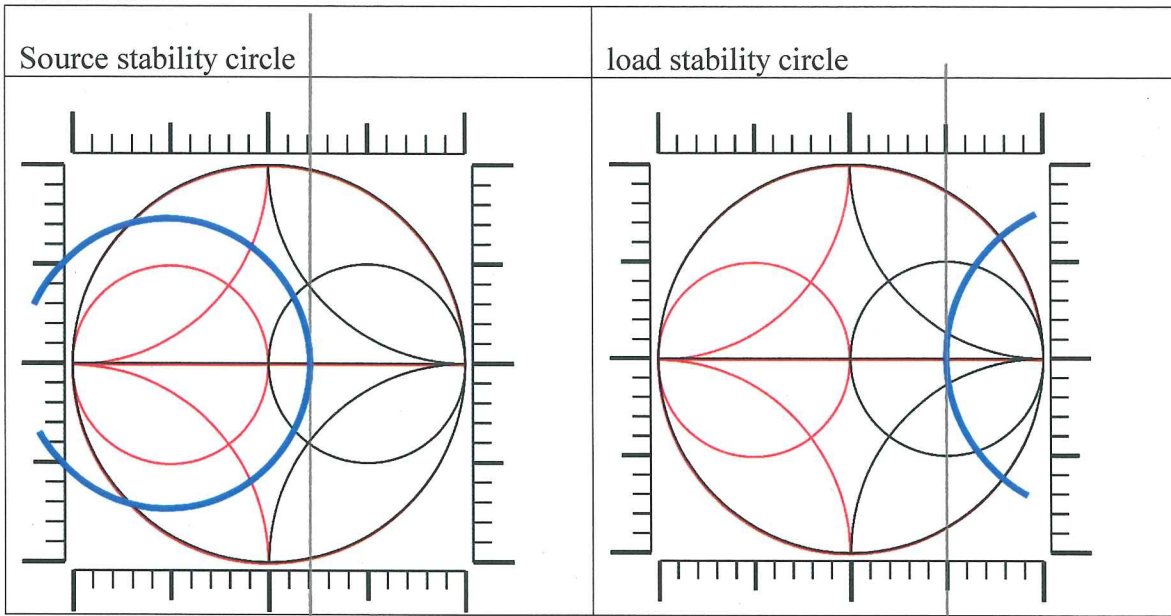
$$= 11.69$$

Load power = 106.9 mW



**Problem 2, 10 points**

*Stabilization*



A MOSFET in common-source mode has  $\|S_{11}\|$  and  $\|S_{22}\|$  both less than 1. . Source and load stability circles are as shown. The Smith charts use 50 Ohms impedance normalization. Draw **3** circuit diagrams, giving resistor values, of methods of stabilizing the transistor. **Please draw your answers in the 3 boxes to the right and below**

circuit #1

5

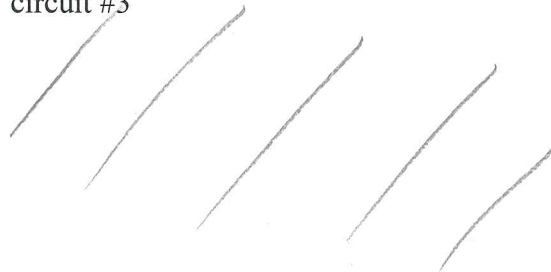


circuit #2

5



circuit #3



Source  $\rightarrow$  Inside of circle is stable. ]

Source stability circle - hits line  $\Gamma = +0.2$  ]

$$\Rightarrow \frac{z}{y} = \frac{1+0.2}{1-0.2} = \frac{1.2}{0.8} \Rightarrow y = \frac{0.8}{1.2} ]$$

$$\Rightarrow Y_{\text{parallel}} = \frac{0.8}{1.2} \cdot \frac{1}{50\Omega} \text{ or } 50\Omega \cdot \frac{1.2}{0.8} = 75\Omega ]$$

$\Rightarrow$  75  $\Omega$  parallel load ]

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Load  $\rightarrow$  outside is stable.

[ Circle hits line  $\Gamma = 0.5$  ]

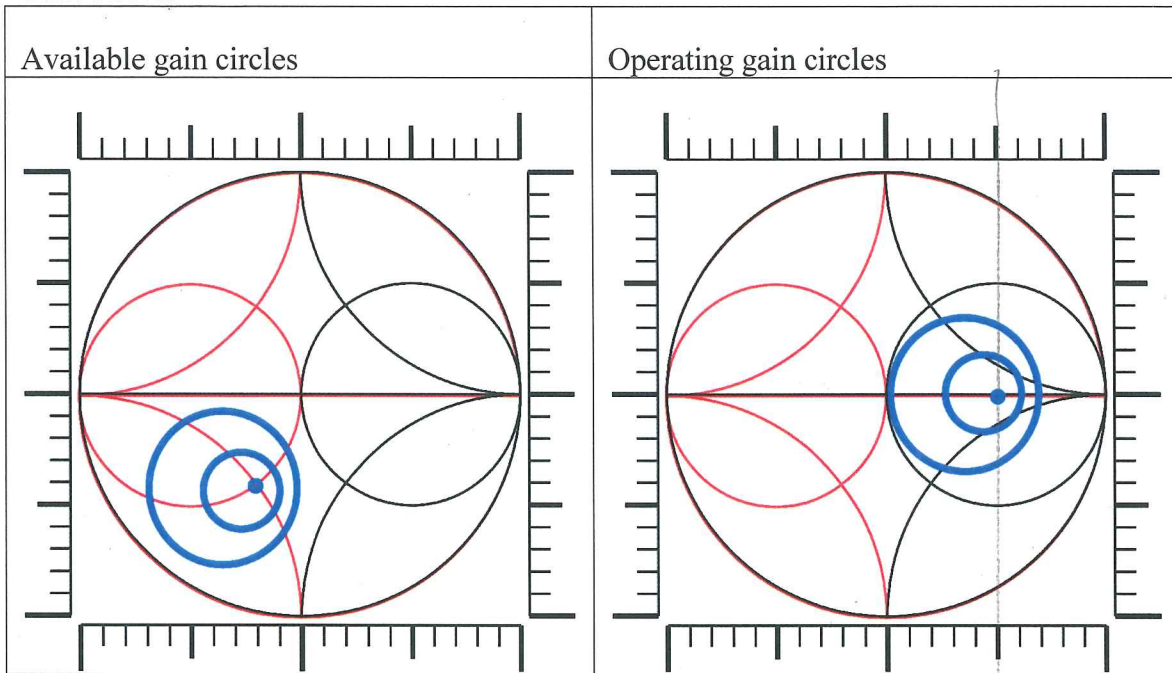
$$\Rightarrow \frac{z}{y} = \frac{1+0.5}{1-0.5} = 3 \Rightarrow y = \frac{1}{3} ]$$

$$\Rightarrow Y_{\text{parallel}} = \frac{1}{3} \cdot \frac{1}{50\Omega} \text{ or } 50\Omega \cdot 3 = 150\Omega ]$$

$\Rightarrow$  150  $\Omega$  parallel load ]

**Problem 3, 10 points**

*Gain circles*



A FET in common-source mode has operating and available gain circles as shown. Find the optimum generator and load impedances (in complex Ohms).

optimum source impedance =  $25\Omega - j25\Omega$

optimum load impedance =  $150\Omega$

available gain

$$y_{\text{source}} = 1 + j1 \quad \text{3}$$

$$\begin{aligned} Z_{\text{source}} &= \frac{1}{1 + j1} = \frac{1 - j1}{(1 + j1)(1 - j1)} = \frac{1 - j1}{1^2 + 1^2} \\ &= \frac{1}{2} - j\frac{1}{2} \\ Z_{\text{source}} &= \underline{25\Omega - j25\Omega} \end{aligned} \quad \begin{array}{l} \text{2} \\ \text{1} \end{array}$$

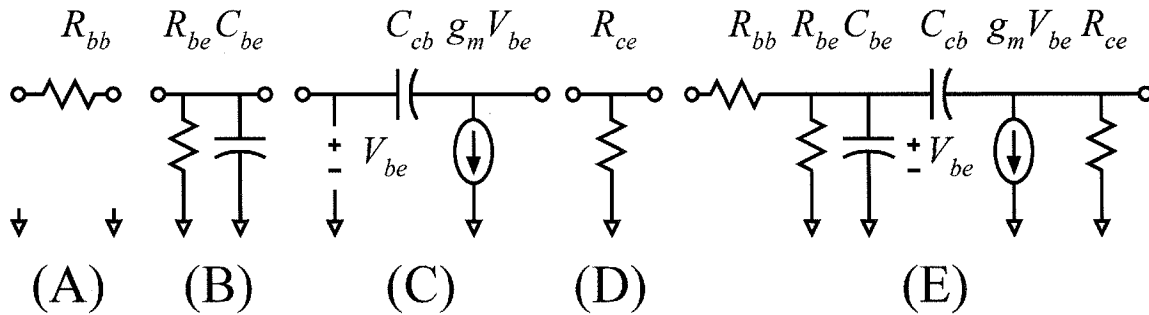
operating gain

$$I_{\text{load}} = \frac{1}{2}$$

$$\Rightarrow g_{\text{load}} = \frac{1 + \frac{1}{2}}{1 - \frac{1}{2}} = 3$$

$$Z_{\text{load}} = 3 \cdot 50\Omega = 150\Omega$$

**Problem 4, 10 points**  
 2-port parameters and gains.

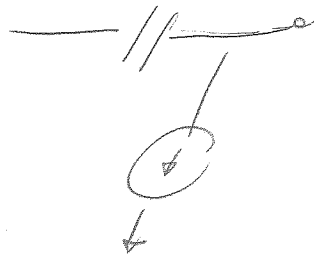


Examining the figure above, we note that network E can be represented as a cascade of networks A-D. Note also that it can be easily shown that  $S_{21}/S_{12} = Y_{21}/Y_{12}$  for any 2-port network.

part a, 5 points

Compute  $Y_{21}$  and  $Y_{12}$  of network C.

$Y_{21} =$  \_\_\_\_\_  $Y_{12} =$  \_\_\_\_\_



$$Y_{21} = g_m - j\omega C_{cb} \quad ]_3$$

$$Y_{12} = -j\omega C_{cb} \quad ]_2$$

part b, 5 points

Find  $S_{21}/S_{12}$  of network E.

$S_{21}/S_{12} =$  \_\_\_\_\_

**\*\*State your arguments clearly\*\***. Points will be deducted if steps are not justified.  
This analysis explain why transistor maximum stable gain tends to have specific variation with frequency.

① 1) networks a, b, d are reciprocal  
have  $S_{12} = S_{21}$

2) a cascade of 2 elements has  $\frac{S_{21}}{S_{12}} = \frac{S_{21}}{S_{12}} = \frac{S_{21}}{S_{12}}$

②

$$S_{21 \text{ overall}} = \frac{S_{21A} S_{21B}}{1 - S_{11A} S_{22B}}$$

$$S_{12 \text{ overall}} = \frac{S_{12A} S_{12B}}{1 - S_{11A} S_{22B}}$$

3)  $\frac{S_{21}}{S_{12}} = \frac{S_{21}}{S_{12}} = \frac{Y_{21}}{Y_{12}}$

$$= \frac{g_m - j\omega C_{cb}}{-j\omega C_{cb}}$$

$$\approx \frac{g_m}{j\omega C_{cb}}$$

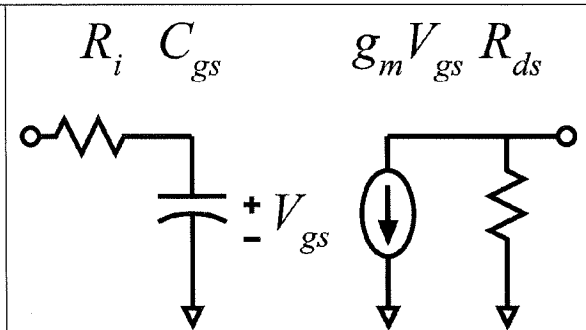
**Problem 5, 20 points**

Transistor cutoff frequencies and gain relationships.

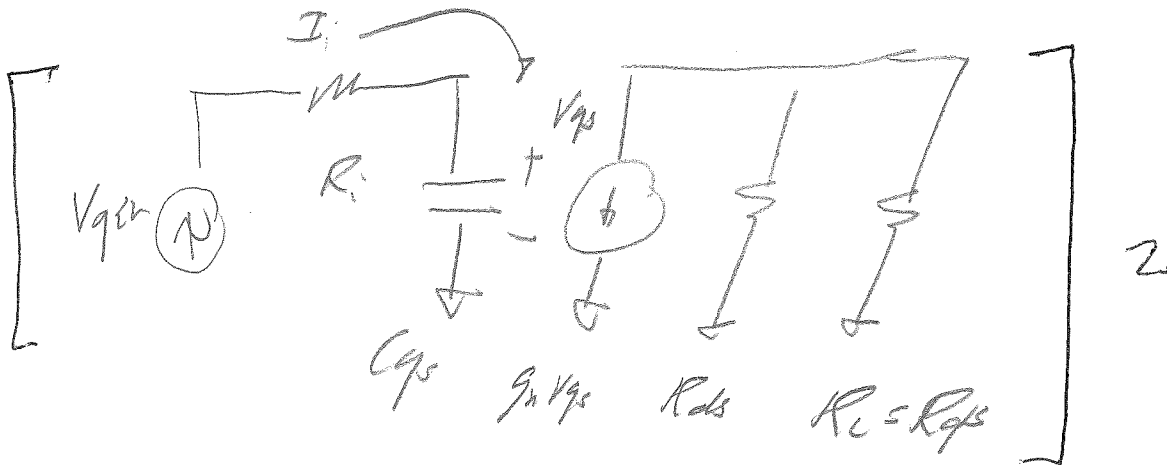
part a, 5 points

Compute, as a function of  $R_i$ ,  $C_{gs}$ ,  $g_m$ , and  $R_{ds}$  the maximum available power gain as a function of frequency.

- 1) Answers from memory are not acceptable: show your work.
- 2) the answer must be in a clear, simple, and tractable form.



MAG=



$$P_{in} = |I_{in}|^2 R_i \quad \text{but} \quad I_{in} = j\omega C_{gs} \cdot V_{gs}$$

so  $P_{in} = \omega^2 C_{gs}^2 R_i |V_{gs}|^2$

If load is matched,  $P_{AVA} = (g_m V_{gs})^2 \cdot 1/4 \cdot R_{DS}$

$$G_{max} = \frac{P_{AVA}}{P_{in}} = \frac{g_m^2 R_{ds} / 4}{\omega^2 C_{gs}^2 R_i}$$

part b: 5 points

Give expressions for the optimum generator and load impedances.

The answers must be in clear, simple, and tractable form.

$Z_{gen,opt} =$  \_\_\_\_\_

$Z_L,opt =$  \_\_\_\_\_

$$3 \left[ Z_{gen,opt} = Z_{in}^* = R_i - j\omega C_{gs} \right]$$

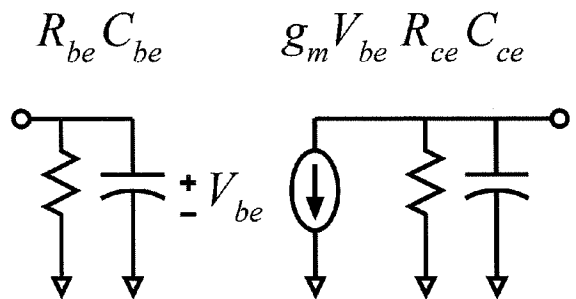
$$2 \left[ Z_{L,opt} = R_{ds} \right]$$



part c: 10 points

Compute, as a function of  $R_{be}$ ,  $C_{be}$ ,  $g_m$ ,  $C_{ce}$  and  $R_{ce}$  the maximum available power gain as a function of frequency. Find also the  $f_{max}$  of the transistor

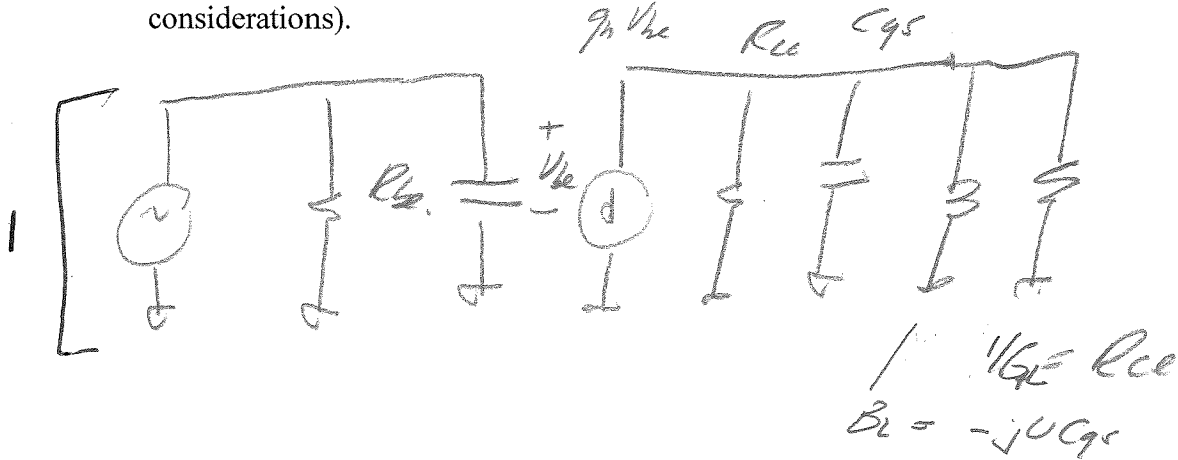
1) the answer must be in a clear, simple, and tractable form.



MAG= \_\_\_\_\_

$f_{max}$  = \_\_\_\_\_

(this answer should give some insight into high-frequency transistor design considerations).



$B_1 = -j\omega C_{ce}$

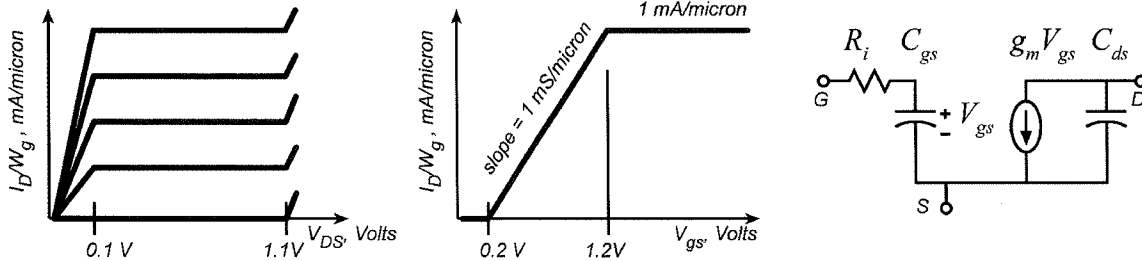
$$P_{in} = \frac{V_{be}^2}{R_{be}}$$

$$P_{avs} = P_{out} = (g_m V_{be})^2 \cdot \frac{1}{4} \cdot R_{ce}$$

$$\frac{P_{avs}}{P_{in}} = \frac{g_m R_{ce}}{4 R_{be}}$$

$$f_{max} = \infty$$

**Problem 6, 20 points**  
Power amplifier design.



A MOSFET has large-signal parameters as given above and small-signal parameters as given below:

$$g_m = 1.0 \text{ mS} / \mu\text{m} \cdot W_g \quad R_i = 1.0 / g_m \quad C_{gd} = 0.0 \text{ fF} / \mu\text{m} \cdot W_g \quad C_{gs} = 1.0 \text{ fF} / \mu\text{m} \cdot W_g$$

$$C_{ds} = 0.5 \text{ fF} / \mu\text{m} \cdot W_g \quad G_{ds} = 0 \text{ mS} / \mu\text{m} \cdot W_g$$

part a, 10 points

You will use a FET of 50 microns total gate width. The signal frequency is 15.9GHz. What is the maximum linear RF output power? What is the optimum load (give either load impedance or load admittance)?

Pout, max = 6.25 mW

Yload = 50 - j2.5 mS

or

Zload = \_\_\_\_\_

$$\sqrt{I_{max} = 1 \text{ mA} / \mu\text{m} \cdot W_g \rightarrow = 50 \text{ mA}}$$

$$\sqrt{V_{max} = 1.2 \text{ V}, V_{mi} = 0.2 \text{ V} \Rightarrow \Delta V = 1.0 \text{ V}}$$

$$\sqrt{P_{max} = 1 \text{ V} \cdot 50 \text{ mA} / 8 = 50 \text{ mW} / 8 = \underline{6.25 \text{ mW}}}$$

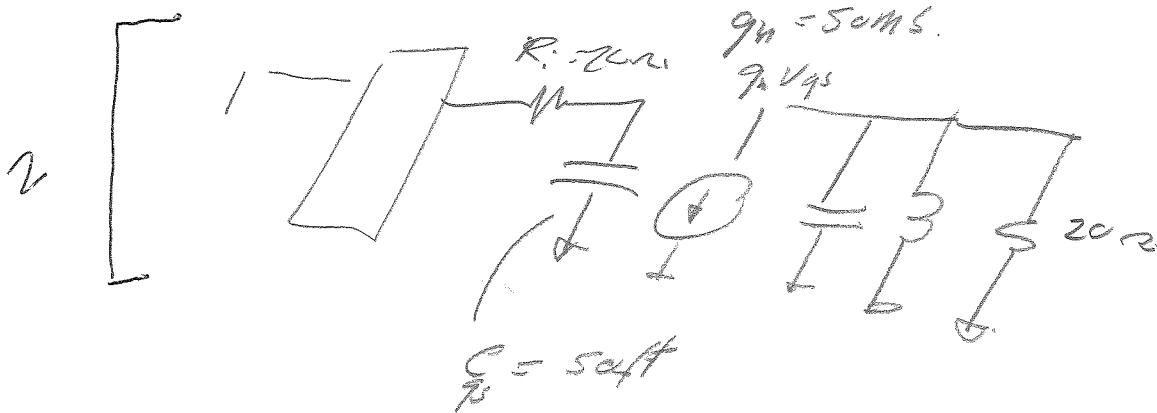
$$\sqrt{1/G_L = \frac{\Delta V}{\Delta I} = \frac{1.0 \text{ V}}{50 \text{ mA}} = 20 \Omega \rightarrow G_L = 50 \text{ mS}}$$

$$\sqrt{B_L = -\omega C_{ds} = -2\pi (15.9 \text{ GHz}) (50 \cdot 0.5 \text{ fF}) = -2.5 \text{ mS}}$$

part b, 10 points

The amplifier has a properly-designed input matching network. With the output power you calculated above, what available generator power is required ?

Available generator power = \_\_\_\_\_



2

$$P_{out} = (g_m V_{gs})^2 \cdot 20 \Omega$$

2

$$P_{in} = (\omega C_{gs})^2 V_{gs}^2 R_i = \omega^2 C_{gs}^2 R_i V_{gs}^2$$

2

$$\frac{P_{out}}{P_{in}} = \frac{g_m^2 \cdot 20 \Omega}{\omega^2 C_{gs}^2 R_i} = \underline{\underline{100}}$$

1

$$P_{out}/P_{in} = 100 \text{ but } P_{out} = 6.25 \text{ mW}$$

1

$$P_{in} = 62.5 \mu\text{W}$$