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***ECE 2C, notes set 8:  
Amplifier Pulse Response:  
Effect of Low-Frequency  
and High-Frequency Poles***

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# Goals:

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Transient response by

LaPlace analysis

partial-fraction expansion

Inverse LaPlace transform by table look-up

Effect of "high - frequency" rolloff on step response

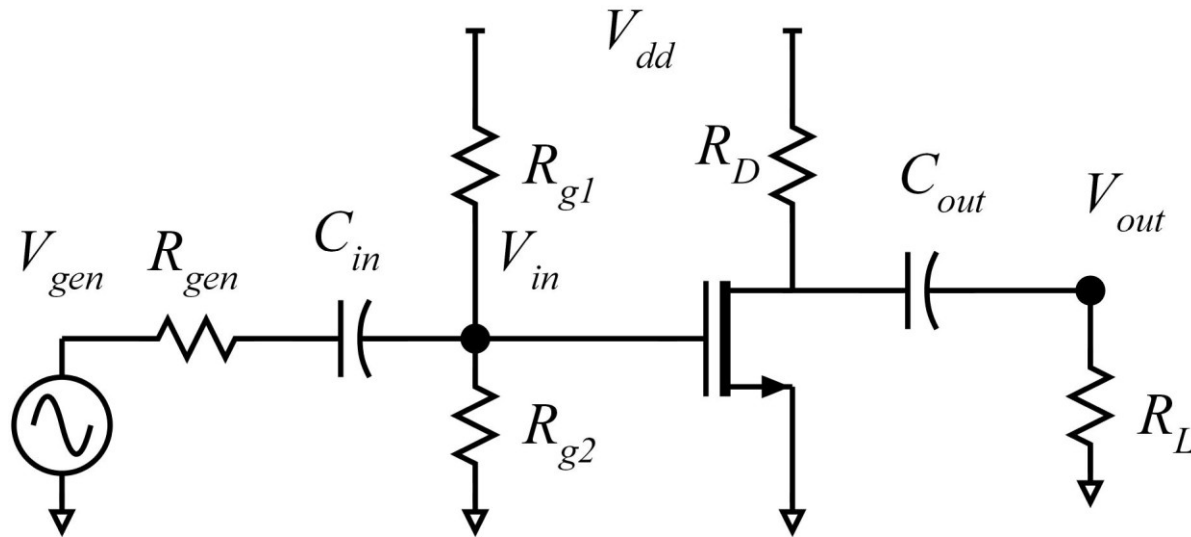
"high - frequency" rolloff  $\leftrightarrow 1/(1 + s\tau)$

Effect of "low - frequency" rolloff on step response

"low - frequency" rolloff  $\leftrightarrow (s\tau)/(1 + s\tau)$

Effect of dominant vs. non-dominant poles on step response.

# Amplifier Pulse Response



$$\frac{V_{out}(s)}{V_{gen}(s)} = -8.65 \cdot \frac{1 + b_1 s}{(1 + a_1 s)(1 + (a_2 / a_1) s)}$$

$$a_1 = 0.326 \mu s, \quad a_2 / a_1 = 1.42 \text{ ns}, \quad b_1 = -0.532 \text{ ns}$$

\*\*\* let us approximate by ignoring the zero \*\*\*

$$\frac{V_{out}(s)}{V_{gen}(s)} \cong -8.65 \cdot \frac{1}{(1 + a_1 s)(1 + (a_2 / a_1) s)}$$

# Step Response

response to 1 mV step-function input:

$$v_{gen}(t) = B \cdot u(t) \rightarrow V_{gen}(s) = B/s \text{ where } B = 1 \text{ mV}$$

$$A_0 = -8.65$$

$$v_0/v_{gen} = \frac{A_0}{(1 + A\tau_1)(1 + A\tau_2)}$$

$$v_0(s) = \frac{A_0 B}{A(1 + A\tau_1)(1 + A\tau_2)}$$

$$= \frac{\kappa_1}{1 + A\tau_1} + \frac{\kappa_2}{1 + A\tau_2} + \frac{\kappa_3}{A}$$

# Step Response: Partial Fraction Expansion

let A approach  $-1/\tau_1$ :

$$\frac{A_0 B}{(-1/\tau_1)(1 - \tau_2/\tau_1)} = K_1 = A_0 B \cdot \frac{\tau_1}{\tau_2 - \tau_1} \cdot \tau_1$$

let A approach  $-1/\tau_2$ :

$$K_2 = \frac{A_0 B}{(-1/\tau_2)(1 - \tau_1/\tau_2)} = A_0 B \frac{\tau_2}{\tau_1 - \tau_2} \cdot \tau_2$$

let A approach zero:

$$K_3 = A_0 B$$

# Step Response: Inverse LaPlace Transform

$$\begin{aligned}
 V_O(s) = & A_0 B \left( \frac{\tau_1}{\tau_2 - \tau_1} \right) \frac{\tau_1}{1 + s\tau_1} \\
 & + A_0 B \left( \frac{\tau_2}{\tau_1 - \tau_2} \right) \frac{\tau_2}{1 + s\tau_2} + \frac{A_0 B}{s}
 \end{aligned}$$

$$v_{out}(t) = A_0 B \left[ u(t) - u(t) \frac{\tau_1}{\tau_1 - \tau_2} \cdot e^{-t/\tau_1} - u(t) \frac{\tau_2}{\tau_2 - \tau_2} \cdot e^{-t/\tau_2} \right]$$

$$A_0 B = -8.65 \text{ mV}, \quad \tau_1 = 0.326 \mu\text{s}, \quad \tau_2 = 1.42 \text{ ns}$$

# Step Response: Effect of the Two Poles

$$v_{out}(t) = A_0 B \left[ u(t) - 1.0044 \cdot e^{-t/0.326\mu s} + 0.0044 \cdot u(t) \cdot e^{-t/1.42ns} \right]$$

= this term, due to the 2<sup>nd</sup> pole in the frequency response

1) Is really small :  $\tau_2 \ll \tau_1$

2) Dies down much more quickly :  $\tau_2 \ll \tau_1$

Conclusion: pulse response is dominated by  
the effect of the dominant pole

# Finding Approximate Pulse Response More Quickly:

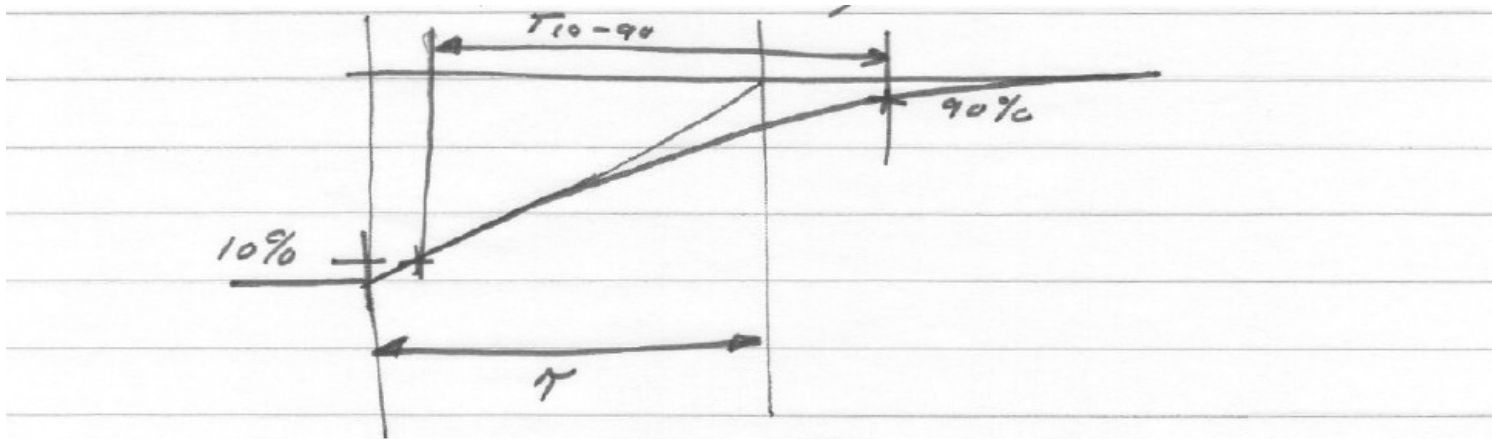
Knowing this, we could have ignored the 2nd pole at the beginning :

$$\frac{V_{out}(s)}{V_{gen}(s)} \cong \frac{-8.65}{1 + s(0.326\mu s)} \text{ with 2nd pole neglected.}$$

$$\text{So if } V_{gen}(s) = (1 \text{ mV})/s$$

$$V_{out}(s) \cong \frac{1 \text{ mV}}{s} \frac{-8.65}{1 + s(0.326\mu s)} = -8.65 \text{ mV} \cdot \left[ \frac{1}{s} - \frac{0.326\mu s}{1 + s(0.326\mu s)} \right]$$

$$v_{out}(t) = -8.65 \text{ mV} \cdot (1 - e^{-t/0.326\mu s}) \cdot U(t)$$

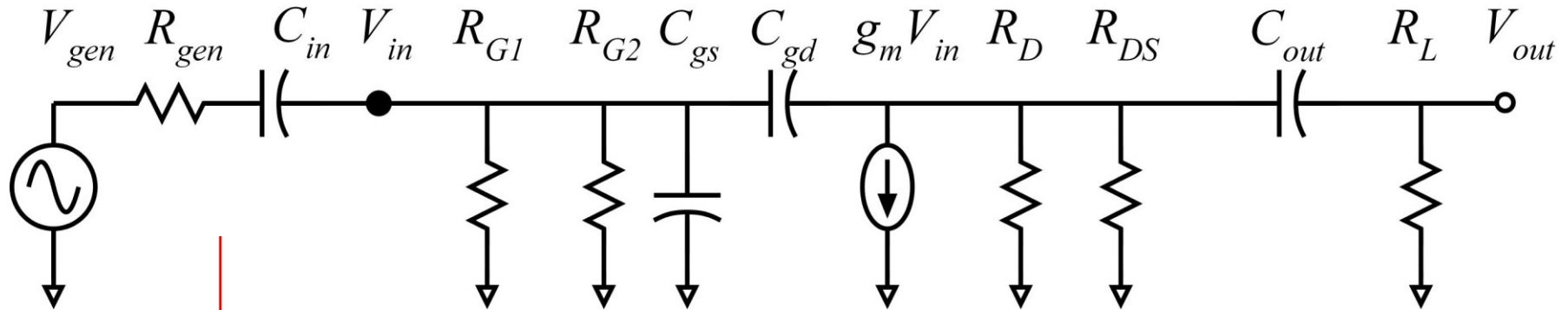


$$T_{10-90} = \tau \cdot [\ln 0.9 - \ln 0.1] = 2.2\tau$$



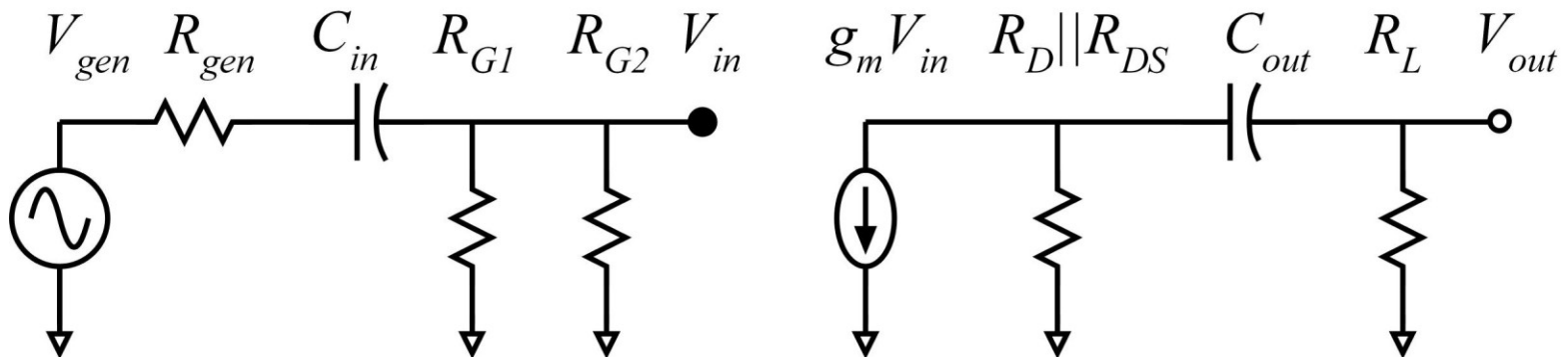
# Low Frequency Response

Common - source amplifier : small - signal equivalent circuit :

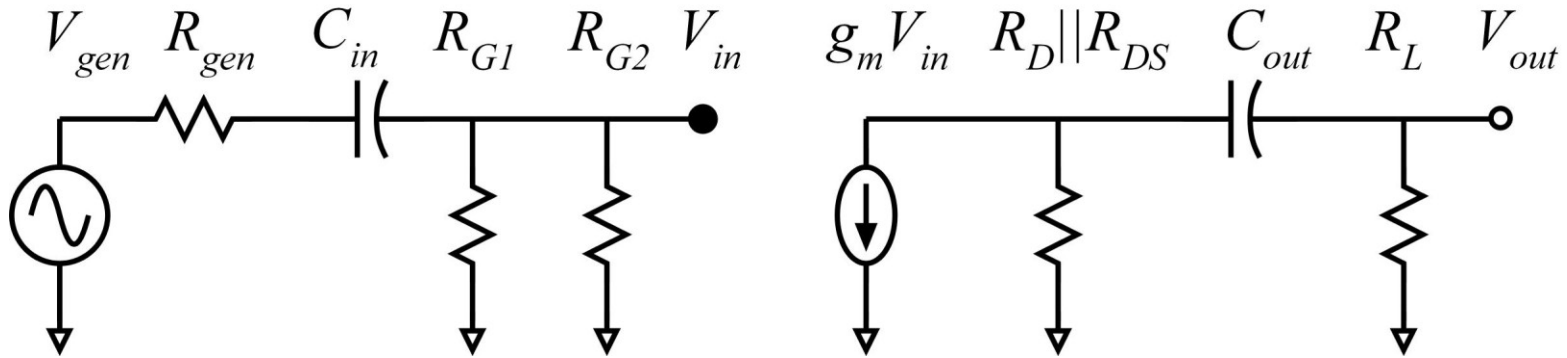


Let us first consider response at high frequencies.

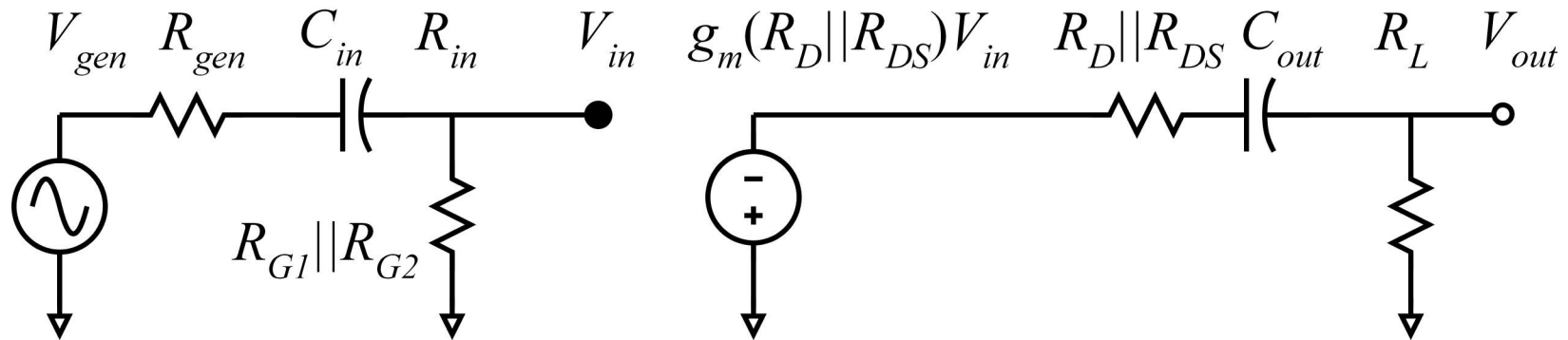
We will therefore temporarily neglect  $C_{in}$  and  $C_{out}$ .



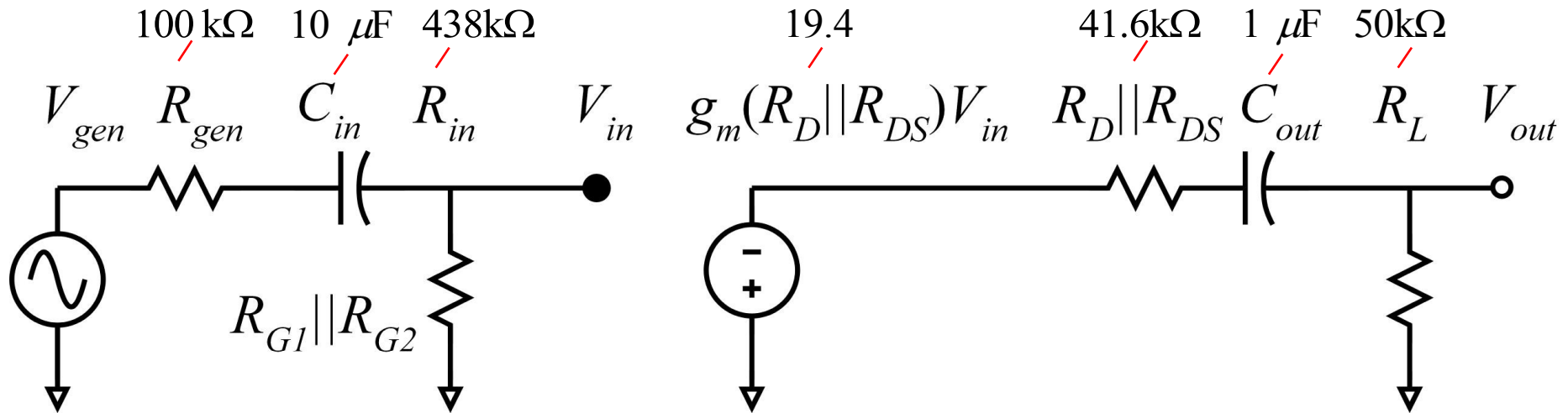
# Low-Frequency Response



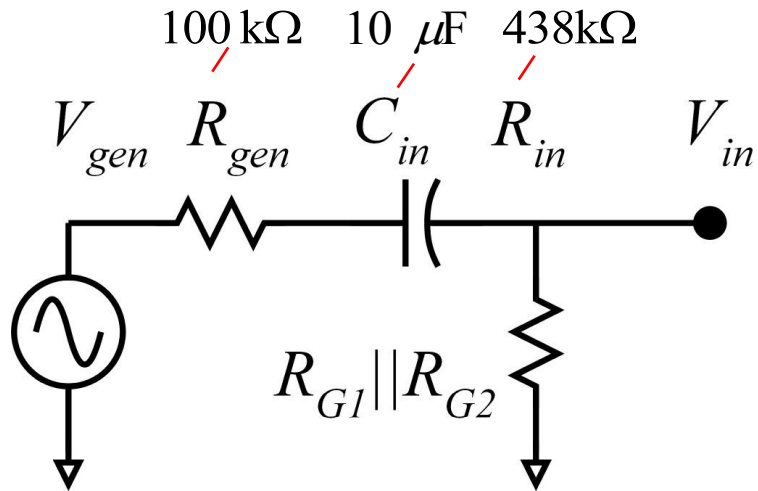
Simplify parallel resistances. Transform from Norton  $\rightarrow$  Thevenin



# Low-Frequency Response



# Low-Frequency Response



$$\begin{aligned}
 \frac{V_{in}(s)}{V_{gen}(s)} &= \frac{R_{g1} \parallel R_{g2}}{R_{g1} \parallel R_{g2} + R_{gen} + 1/sC_{in}} = \frac{sC_{in}(R_{g1} \parallel R_{g2})}{1 + sC_{in}(R_{g1} \parallel R_{g2} + R_{gen})} \\
 &= \frac{(R_{g1} \parallel R_{g2})}{(R_{g1} \parallel R_{g2}) + R_{gen}} \frac{sC_{in}(R_{g1} \parallel R_{g2} + R_{gen})}{1 + sC_{in}(R_{g1} \parallel R_{g2} + R_{gen})} \\
 &= \frac{V_{in}}{V_{gen}} \Bigg|_{\text{mid-band}} \times \frac{s\tau_{in}}{1 + s\tau_{in}}
 \end{aligned}$$

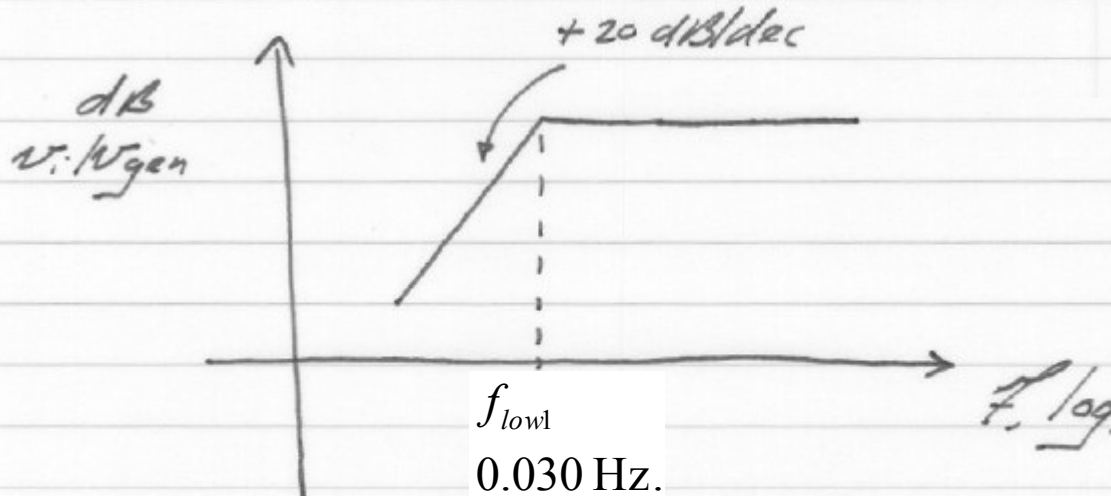
# Low Frequency Response

$$\frac{v_{in}}{v_{gen}} = \frac{v_{in}}{v_{gen} / \text{MB}} \times \frac{1 + A T_{in}}{1 + A T_{in}} ;$$

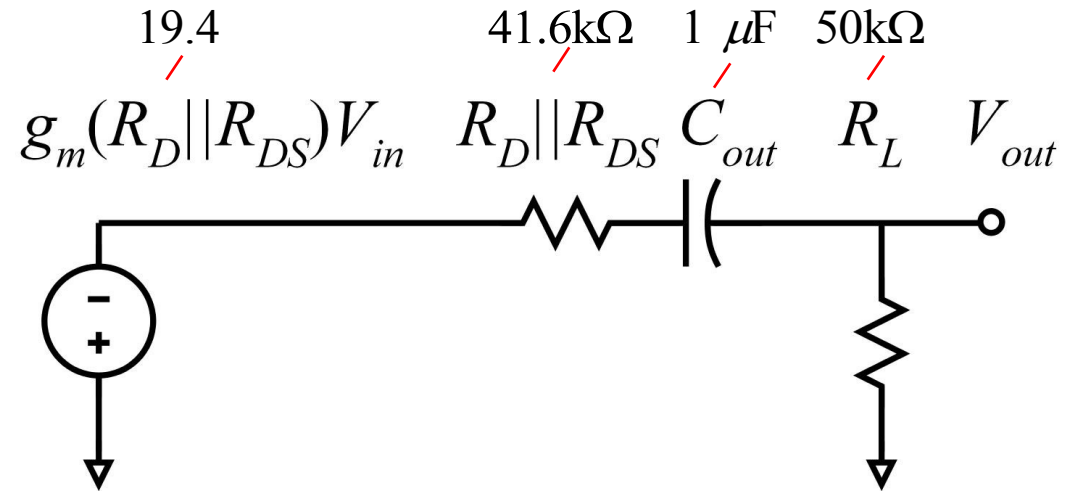
$$\begin{aligned} \tau_{in} &= C_{in} (R_{g1} \parallel R_{g2} + R_{gen}) \\ &= 10 \mu\text{F} \cdot (438 \text{k}\Omega + 100 \text{k}\Omega) \\ &= 5,380 \text{ ms} = 5.38 \text{ s}. \end{aligned}$$

$$= \frac{v_{in}}{v_{gen} / \text{MB}} \frac{j f / f_{low1}}{1 + j f / f_{low1}} ;$$

$$f_{low1} = 1 / 2\pi\tau_{in} = 0.030 \text{ Hz}.$$



# Low-Frequency Response



$$\begin{aligned}
 \frac{V_{out}(s)}{V_{in}(s)} &= -g_m(R_D \parallel R_{DS}) \cdot \frac{R_L}{R_D \parallel R_{DS} + R_L + 1/sC_{out}} \\
 &= -g_m(R_D \parallel R_{DS}) \cdot \frac{R_L}{(R_D \parallel R_{DS} + R_L)} \frac{sC_{out}(R_D \parallel R_{DS} + R_L)}{1 + sC_{out}(R_D \parallel R_{DS} + R_L)} \\
 &= -g_m(R_D \parallel R_{DS} \parallel R_L) \cdot \frac{sC_{out}(R_D \parallel R_{DS} + R_L)}{1 + sC_{out}(R_D \parallel R_{DS} + R_L)} \\
 &= \left. \frac{V_{out}}{V_{in}} \right|_{mid-band} \times \frac{s\tau_{out}}{1 + s\tau_{out}}
 \end{aligned}$$

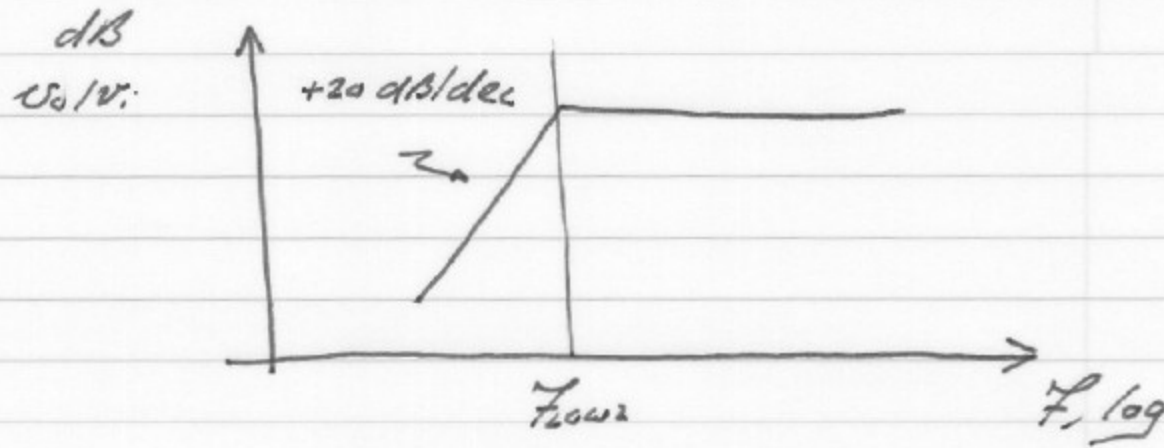
# Low Frequency Response

$$\frac{v_o}{v_i} = \frac{v_o}{v_i} \cdot \frac{A_{T_{out}}}{1 + A_{T_{out}}}$$

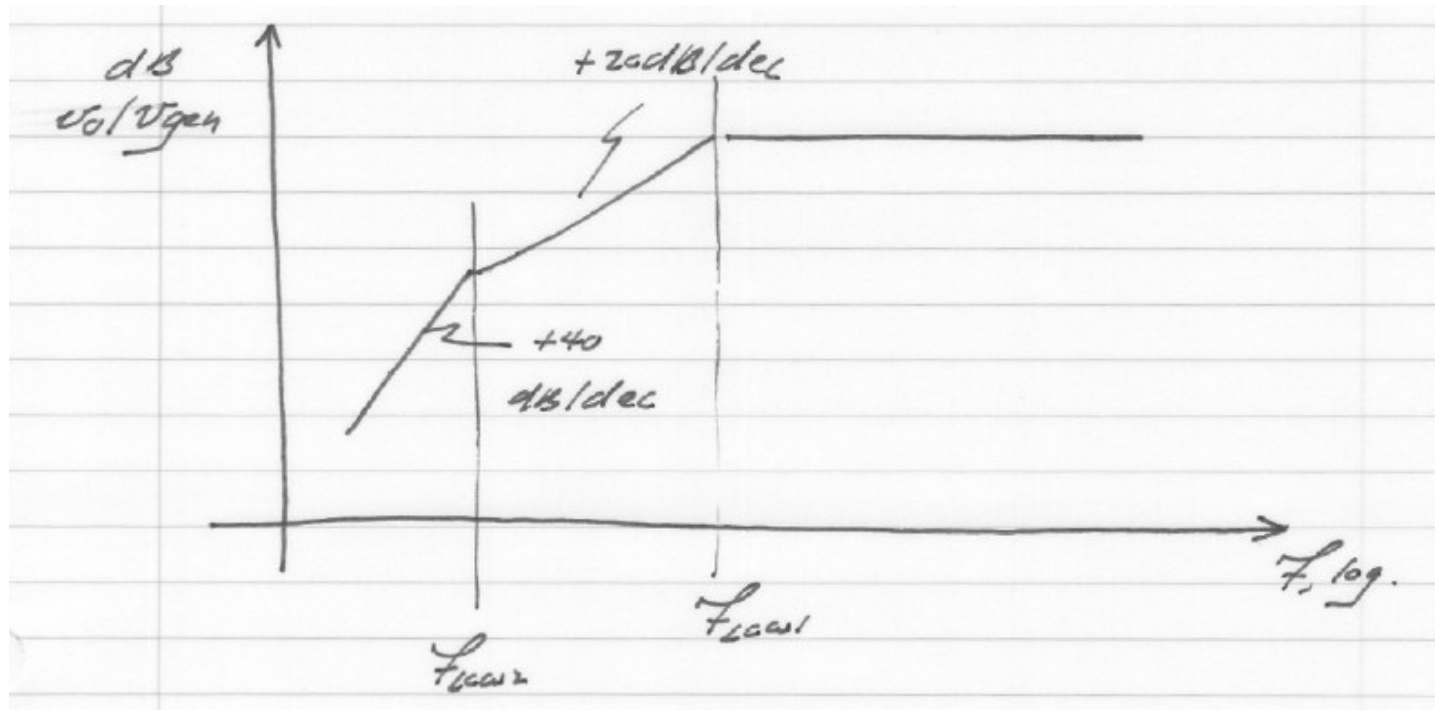
$$\begin{aligned} \tau_{out} &= C_{out}(R_D \parallel R_{DS} + R_L) \\ &= 1\mu\text{F} \cdot (41.6\text{k}\Omega + 50\text{k}\Omega) \\ &= 91.6\text{ms} \end{aligned}$$

$$\frac{v_o}{v_i} = \frac{v_o}{v_i} \cdot \frac{1}{1 + jf/f_{low2}}$$

$$f_{low2} = 1/2\pi\tau_{out} = 1.73\text{Hz}$$



# Overall Low Frequency Response



$$\frac{v_o}{v_{gen}} = \frac{v_o}{v_{gen}} \Big|_{MB} \frac{A_{T_{in}}}{1 + A_{T_{in}}} \frac{A_{T_{out}}}{1 + A_{T_{out}}}$$

"Amb"

— this ignores the high frequency rolloff



# Step Response Due to Low-Frequency Poles

$$v_{gen}(s) = v_x / s \quad \text{e.g. } v_{gen}(t) = v_x \cdot u(t)$$

$$v_{out}(s) = \frac{\tau_o}{1 + s\tau_o} \cdot \frac{\tau_i}{1 + s\tau_i} \cdot A \cdot A_{mb} \cdot v_x$$

$$= A_{mb} v_x \left[ \frac{\tau_{in}}{\tau_{in} - \tau_{out}} \cdot \frac{\tau_{out}}{1 + s\tau_{out}} + \frac{\tau_{out}}{\tau_{out} - \tau_{in}} \cdot \frac{\tau_{in}}{1 + s\tau_{in}} \right]$$

+1.0173

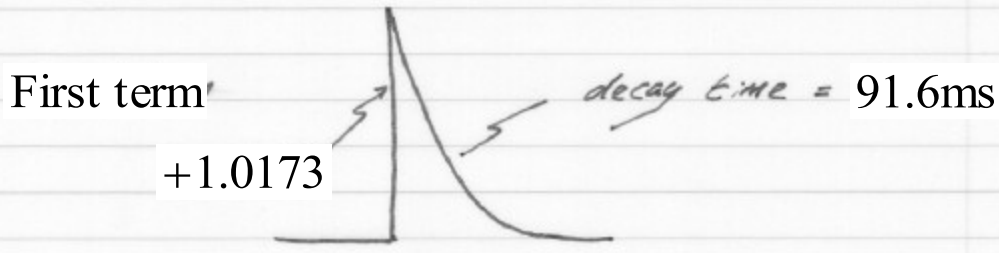
-0.0173

$$v_{out}(t) = A_{mb} v_x \left[ \frac{\tau_{in}}{\tau_{in} - \tau_{out}} u(t) e^{-t/\tau_{out}} + \frac{\tau_{out}}{\tau_{out} - \tau_{in}} u(t) e^{-t/\tau_{in}} \right]$$

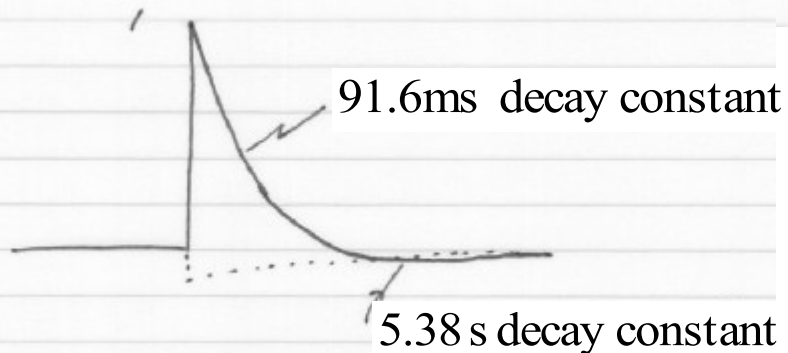
$$\tau_{in} = 5.38 \text{ s.}$$

$$\tau_{out} = 91.6 \text{ ms}$$

# Step Response Due to Low-Frequency Poles



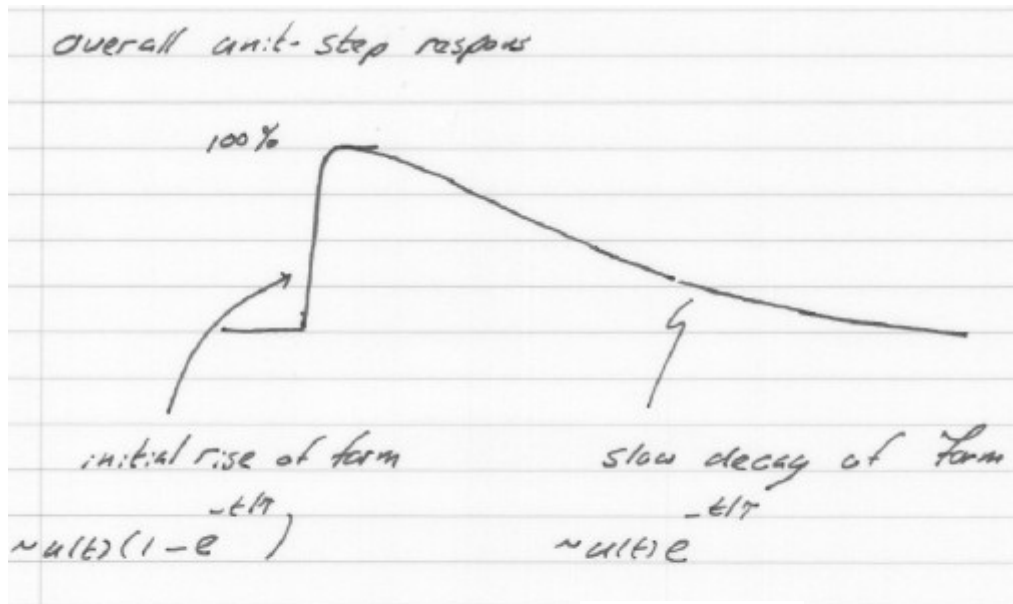
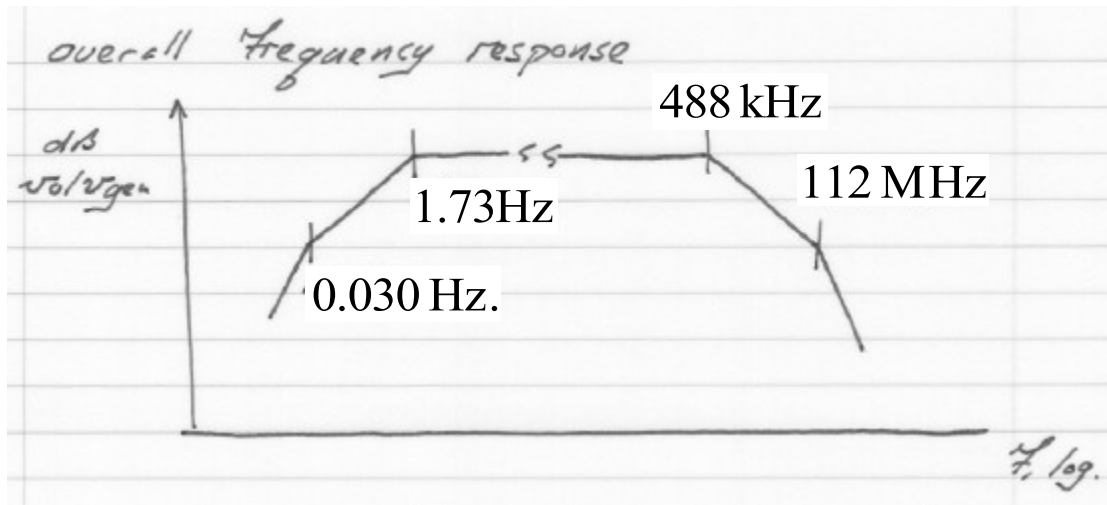
total response (normalized to  $AmbV_x$ ):



Step response is dominated by the \*highest\* of the low - frequency poles

Again, the lower of the two low-frequency poles contributes only a small amount to the step response and decays away more slowly.

# Step Response with Low- and High-Frequency Poles



$$\tau = 0.326 \mu\text{s}$$

$$\tau = 91.6 \text{ ms}$$

$$T_{10-90} = 2.2\tau = 0.72 \mu\text{s}$$

High - frequency rolloff  
sets the risetime.

Low frequency rolloff  
sets the droop rate.

