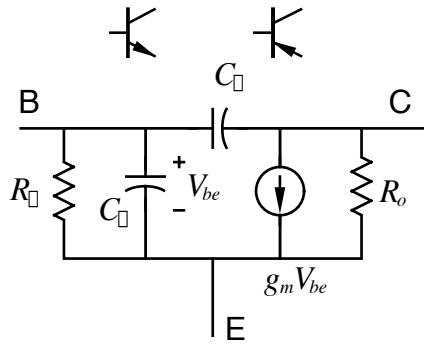


Basics: Transistor small-signal high-frequency models



Hybrid-pi model:

$$C_\mu = C_{bc}$$

$$C_\pi = C_{be} = C_{\pi,depl} + C_{\pi,diff}$$

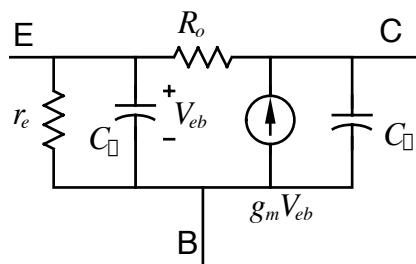
$$C_{\pi,diff} = g_m \tau_f$$

$$f_\tau = g_m / (2\pi(C_\pi + C_\mu))$$

$$g_m = \alpha/r_e = I_c/V_T$$

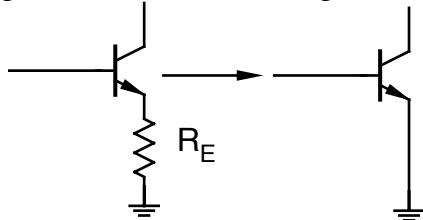
$$R_\pi = (\beta + 1)r_e$$

$$R_o = V_A/I_C$$



"T"-model
Makes common-base analysis much easier.
Both these models are only approximate,
being "good" up to f_t . Additionally $R_{b\oplus}$ is
often an important parasitic (not discussed
much in 137B).

Simplification of Emitter Degeneration



approximate only; check notes for bounds
on validity

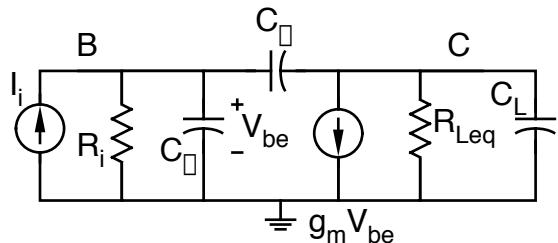
$$\mathcal{J}_\pi = C_\pi (r_e / (r_e + R_E))$$

$$\mathcal{g}_m = g_m (r_e / (r_e + R_E)) = \alpha / (r_e + R_E)$$

$$\mathcal{J}_\mu = C_\mu$$

$$\mathcal{R}_\pi = R_\pi ((r_e + R_E) / r_e) = (\beta + 1)(r_e + R_E)$$

Common-Emitter Stage



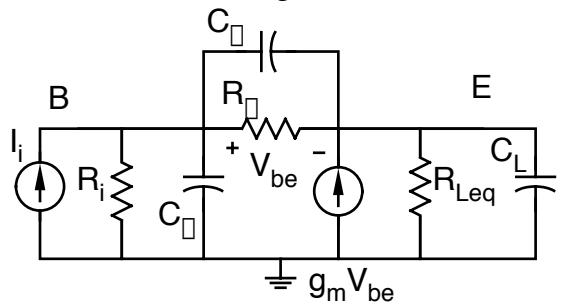
$$V_{out}/V_{gen} = (V_{out}/V_{gen})_{MB} \frac{1 + s\tau_{zero}}{1 + a_1 s + a_2 s^2}$$

$$a_1 = R_i (C_\pi + C_\mu (1 + g_m R_{L_{eq}})) + R_{L_{eq}} (C_\mu + C_L)$$

$$a_2 = R_i R_{L_{eq}} (C_\mu C_L + C_\mu C_\pi + C_\pi C_L)$$

$$\tau_{zero} = -C_\mu / g_m$$

Emitter-Follower Stage



$$V_{out}/V_{gen} = \left(V_{out}/V_{gen} \right)_{MB} \frac{1 + s\tau_{zero}}{1 + a_1s + a_2s^2}$$

given that $A_{vmb} = \left(r_e / (r_e + R_{Leq}) \right)$:

$$a_1 = C_\pi \left(R_\pi \parallel (r_e \parallel R_{Leq} + R_i(1 - A_{vmb})) \right)$$

$$+ C_\mu (R_i \parallel \text{transistor input resistance})$$

$$+ C_L (R_{Leq} \parallel \text{transistor output resistance})$$

$$a_2 = (R_i \parallel \text{transistor input resistance}) (R_{Leq} \parallel r_e)$$

$$\times (C_\mu C_\pi + C_\mu C_L + C_L C_\pi)$$

$$\tau_{zero} = g_m / C_\pi$$

General Solutions of Problems: Nodal analysis (Know how to do this!)

1) Write the nodal equations (sum of the currents=0) at each circuit node, and put the resulting equations in matrix form (the Y's being various combinations of g_m 's, $1/R$'s, and sC 's):

$$\begin{bmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} \\ Y_{41} & Y_{42} & Y_{43} & Y_{44} \end{bmatrix} \begin{bmatrix} V_1 = V_{in} \\ V_2 \\ V_3 \\ V_4 = V_{out} \end{bmatrix} = \begin{bmatrix} I_{in} \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

2) Use Cramer's rule to solve:

$$\frac{\begin{vmatrix} Y_{11} & Y_{12} & Y_{13} & I_{in} \\ Y_{21} & Y_{22} & Y_{23} & 0 \\ Y_{31} & Y_{32} & Y_{33} & 0 \\ Y_{41} & Y_{42} & Y_{43} & 0 \end{vmatrix}}{\begin{vmatrix} Y_{11} & Y_{12} & Y_{13} & Y_{14} \\ Y_{21} & Y_{22} & Y_{23} & Y_{24} \\ Y_{31} & Y_{32} & Y_{33} & Y_{34} \\ Y_{41} & Y_{42} & Y_{43} & Y_{44} \end{vmatrix}} = V_{out}$$

3) This comes out as:

$$\frac{V_{out}}{I_{in}} = ks^m \frac{c_0 + c_1s + c_2s^2 + \dots}{d_0 + d_1s + d_2s^2 + \dots}$$

, which is divided through to get:

(if present, m is the number of zeros, minus the number of poles, in the transfer function)

4)

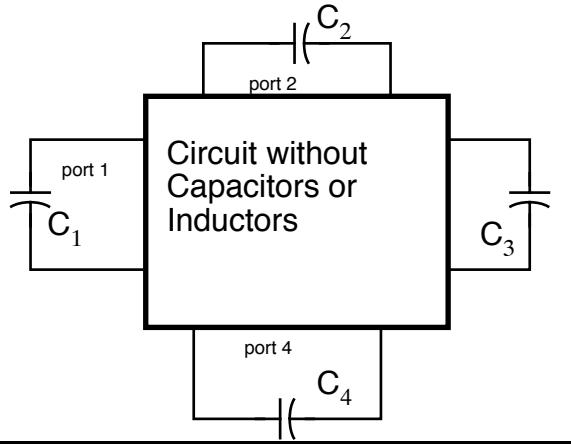
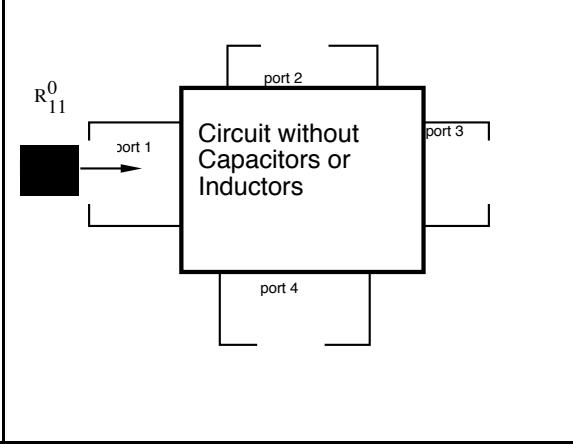
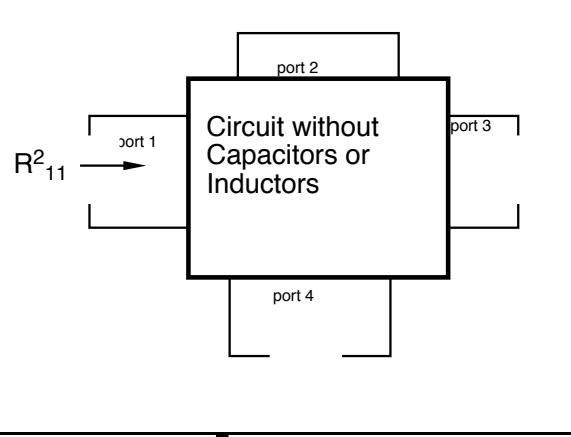
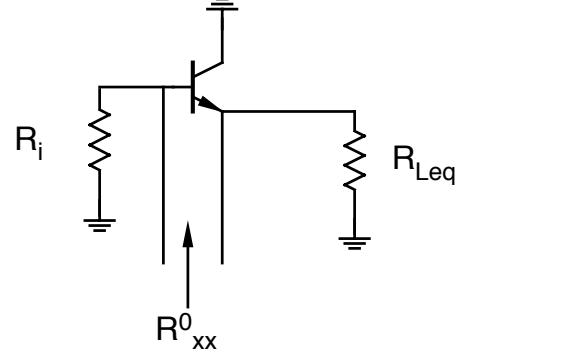
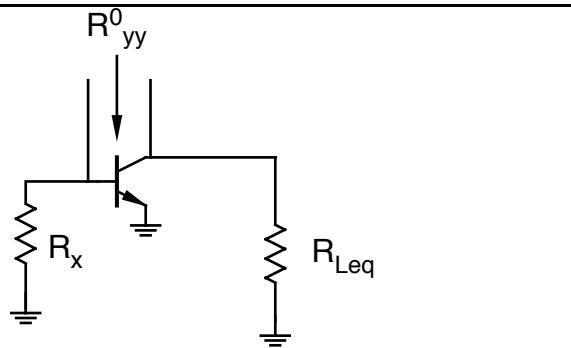
$$\frac{V_{out}}{I_{in}} = \left(\frac{V_{out}}{I_{in}} \right)_{mb} s^m \frac{1 + b_1s + b_2s^2 + \dots}{1 + a_1s + a_2s^2 + \dots}$$

...and the poles and zeroes are found by factoring the numerator and denominator. The separated-pole approximation, if applicable, makes this factoring easy.

5) To find the *impulse response*, do a partial-fraction expansion and then take the inverse LaPlace transform.

6) To find the sinusoidal frequency response, set $s = j\omega$.

General Solutions of Problems: Method of Time Constants

 <p>Circuit without Capacitors or Inductors</p>	 <p>Circuit without Capacitors or Inductors</p>
 <p>Circuit without Capacitors or Inductors</p>	$\frac{V_{out}}{V_{gen}} = \left(\frac{V_{out}}{V_{gen}} \right)_{mb} \frac{1 + b_1 s + b_2 s^2 + \dots}{1 + a_1 s + a_2 s^2 + \dots}$ $a_1 = R_{11}^0 C_1 + R_{22}^0 C_2 + R_{33}^0 C_3 + R_{44}^0 C_4$ $a_2 = R_{11}^0 R_{22}^1 C_1 C_2 + R_{11}^0 R_{33}^1 C_1 C_3 + R_{11}^0 R_{44}^1 C_1 C_4 + R_{22}^0 R_{33}^2 C_2 C_3 + R_{22}^0 R_{44}^2 C_2 C_4 + R_{33}^0 R_{44}^3 C_3 C_4$ <p>note that $R_{xx}^0 R_{yy}^x = R_{xx}^y R_{yy}^0$</p>
	$R_{xx}^0 = R_\pi \parallel (r_e \parallel R_{Leq} + R_i (1 - A_{vmb}))$ $A_{vmb} = \left(R_{Leq} / (r_e + R_{Leq}) \right)$
	$R_i = R_x \parallel R_\pi$ $R_{yy}^0 = R_i (1 + g_m R_{Leq}) + R_{Leq}$