

Compound Semiconductor IC Symposium 2010

Chart 1

A 204.8GHz Static Divide-by-8 Frequency Divider in 250nm InP HBT

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Why Static Frequency Dividers ?

Chart 2

MS flip-flops are very widely-used high speed digital circuits:

- Dividers are master-slave flip-flop with inverting feedback
- Connection as 2:1 frequency divider provides simple test method

Standard benchmark of logic speed:

- Performance comparisons across technologies

Dynamic, super-dynamic, frequency dividers:

- Higher maximum frequency than true static dividers
- Narrow-band operation → applications are limited

High speed technology performance for static dividers:

- 250nm InP HBT: NGAS **200.6GHz** (2009), TSC/UCSB **204.8GHz** (2010)
- Advanced SiGe HBT: Infineon **110+GHz**

Fast divider design – identifying dominant gate delays

Chart 3

Gate Delay Determined by :

Depletion capacitance charging
through the logic swing

$$\left(\frac{\Delta V_{LOGIC}}{I_C} \right) (C_{cb} + C_{be,\text{depletion}})$$

Depletion capacitance charging
through the base resistance

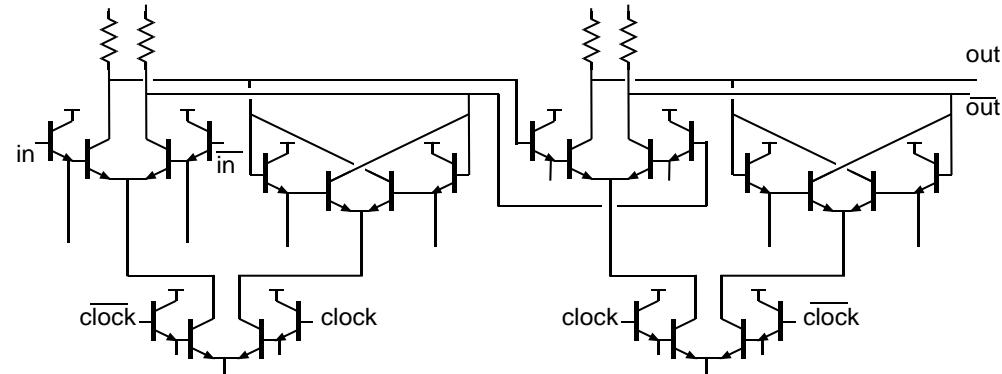
$$R_{bb} (C_{cb} + C_{be,\text{depl}})$$

Supplying base + collector
stored charge
through the base resistance

$$R_{bb} (\tau_b + \tau_c) \left(\frac{I_C}{\Delta V_{LOGIC}} \right)$$

The logic swing must be at least

$$\Delta V_{LOGIC} > 6 \left(\frac{kT}{q} + R_{ex} I_c \right)$$



Delay not well correlated with HBT delay $1/(2\pi\tau)$.

$(\Delta V_{LOGIC} / I_C) (C_{cb} + C_{be,\text{depl}})$ is 60%-80% of total.

Low (C_{cb} / I_c) is a key HBT design objective.

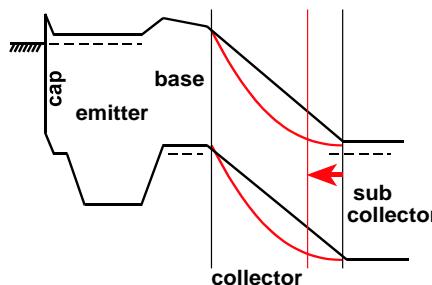
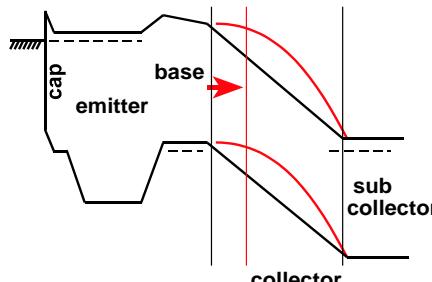
$$\frac{C_{cb} \Delta V_{LOGIC}}{I_C} = \frac{\Delta V_{LOGIC}}{2V_{CE,\min}} \left(\frac{A_{\text{collector}}}{A_{\text{emitter}}} \right) \left(\frac{T_C}{2v_{\text{effective}}} \right)$$

R_{ex} must be very low for low ΔV_{logic} at high J_e

...Need to design for clock speed, not f_T & f_{max}

200GHz dividers – collector design for 250nm HBTs

Chart 4



Collector Field Collapse (Kirk Effect)

$$V_{cb} + \phi > + (J / v_{sat} - qN_d)(T_c^2 / 2\epsilon)$$

Collector Depletion Layer Collapse

$$V_{cb,min} + \phi > + (qN_d)(T_c^2 / 2\epsilon)$$

$$\Rightarrow J_{max} = 2\epsilon v_{sat} (V_{ce} + V_{ce,min}) / T_c^2 \quad (1\text{-D collector current flow})$$

0.25um HBT, 200GHz divider – vertical, lateral scaling for $J_e = 10\text{mA}/\mu\text{m}^2$

0.5um HBT, 150GHz divider, $J_e = 5\text{mA}/\mu\text{m}^2$

$$C_{cb,1} \frac{\Delta V_{logic}}{I_C} = \frac{\epsilon_o \epsilon_r}{T_{C,1}} \frac{1}{J_{e,1} A_{e,1}} \frac{\Delta V_{logic}}{A_{c,1}}$$

$$C_{cb,2} \frac{\Delta V_{logic}}{I_C} = \frac{\epsilon_o \epsilon_r}{T_{C,1}} \frac{1}{2} A_{c,1} \frac{\Delta V_{logic}}{2 J_{e,1} \cdot \frac{1}{2} A_{e,1}} = \frac{3}{4} C_{cb,1} \frac{\Delta V_{logic}}{I_C}$$

33% reduction

$$C_{cb,2} \frac{\Delta V_{logic}}{I_C} = \frac{\epsilon_o \epsilon_r}{T_{C,1}} \frac{1}{2} A_{c,1} \frac{\Delta V_{logic}}{2 J_{e,1} \cdot \frac{1}{2} A_{e,1}} = \frac{1}{2} C_{cb,1} \frac{\Delta V_{logic}}{I_C}$$

Lateral scaling, current spreading for $J_e = 10\text{mA}/\mu\text{m}^2$

Key HBT Scaling Limit → Emitter Resistance

Chart 5

ECL delay not well correlated with f_τ or f_{max}

Largest delay is charging C_{cb}

$$C_{cb} \frac{\Delta V_{logic}}{I_c} = \frac{\epsilon_0 \epsilon_r A_{collector}}{T_c} \frac{\Delta V_{logic}}{J_e A_{emitter}} ; \text{ where } J_{e,max} \propto 1/T_c^2.$$

→ $J_e \approx 10 \text{ mA}/\mu\text{m}^2$ needed for 200 GHz clock rate

Voltage drop of emitter resistance becomes excessive

$$R_{ex} I_c = \rho_{ex} J_e = (15 \Omega \cdot \mu\text{m}^2) \cdot (10 \text{ mA}/\mu\text{m}^2) = 150 \text{ mV}$$

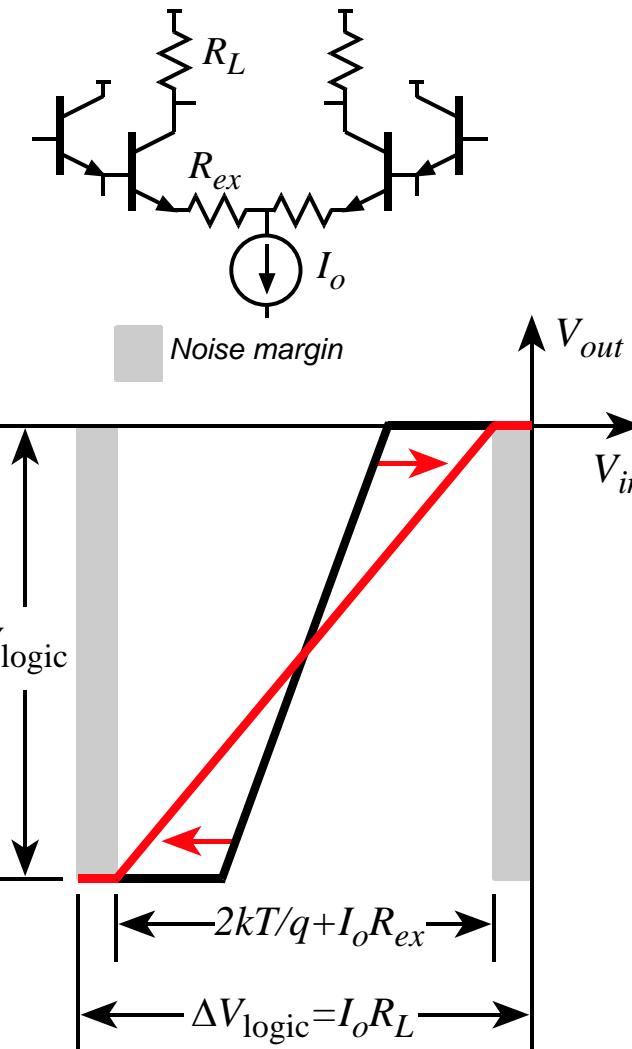
→ considerable fraction of $\Delta V_{logic} \approx 300 \text{ mV}$

Degrades logic noise margin

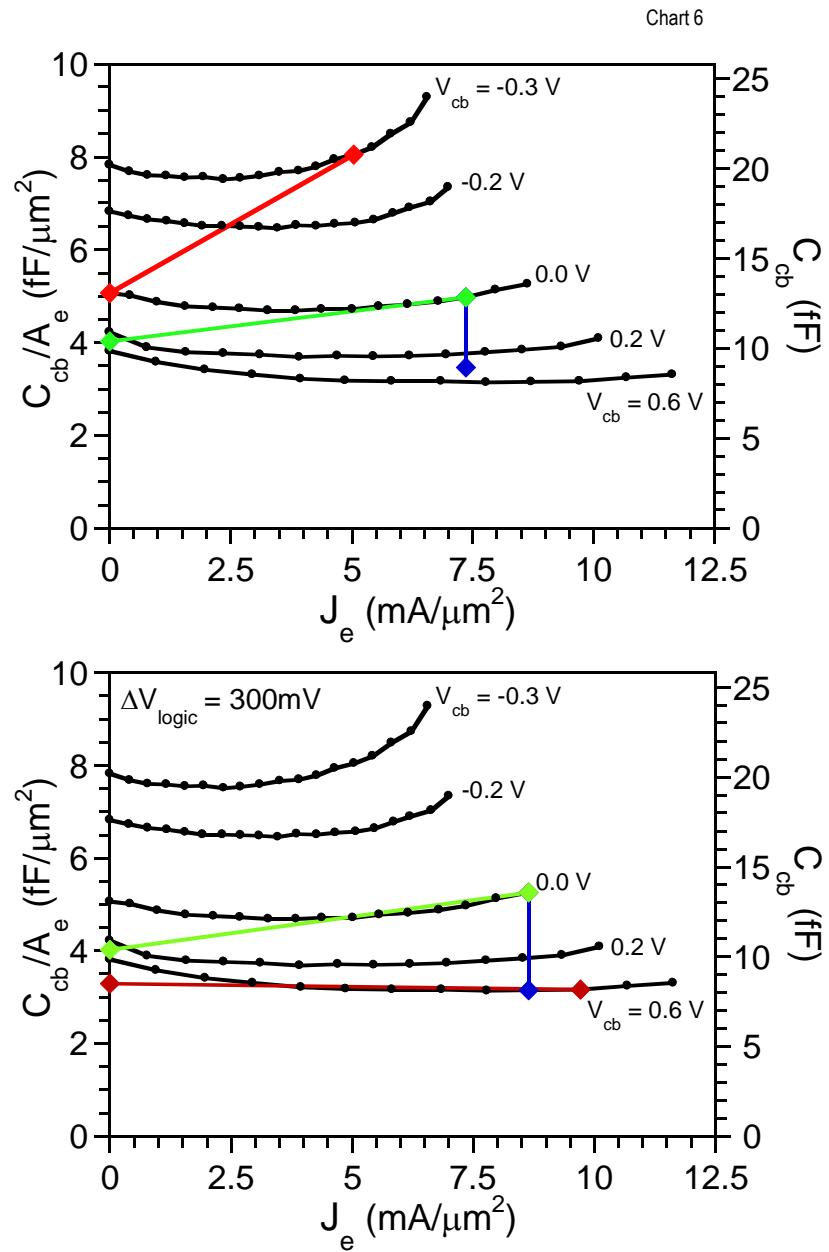
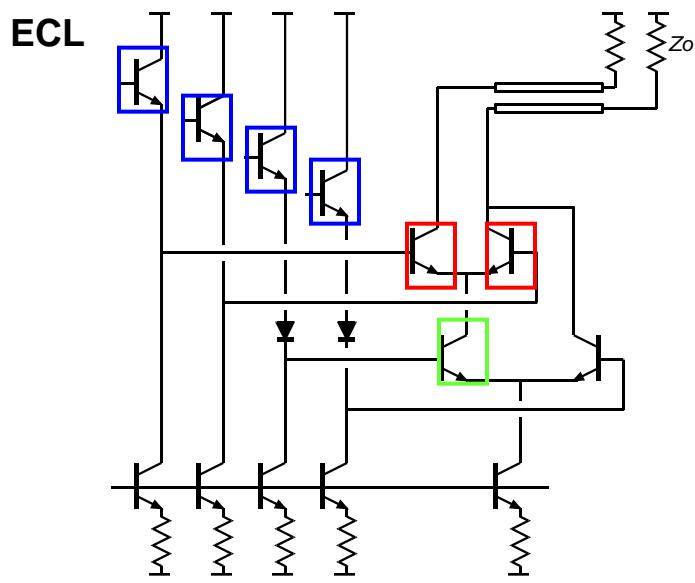
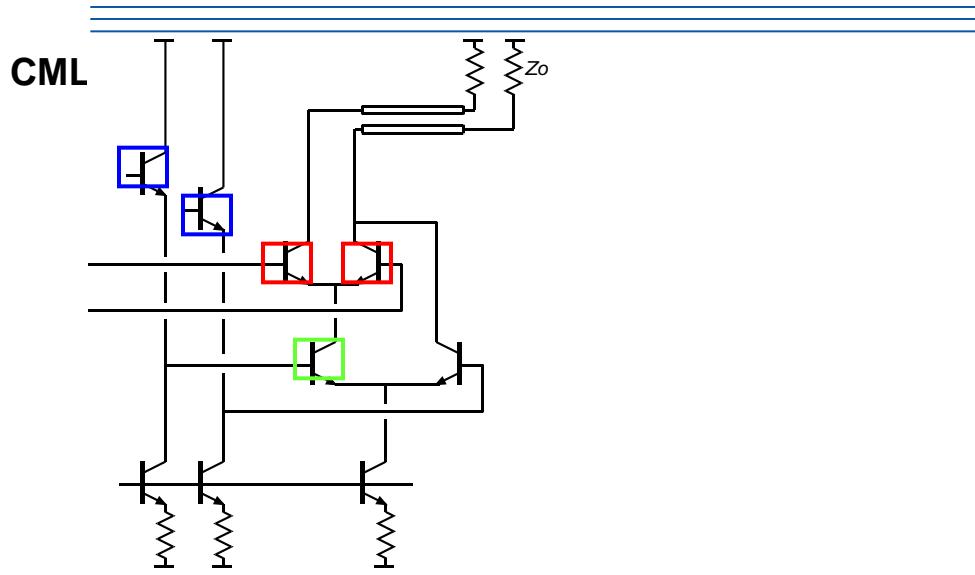
→ $\rho_{ex} \leq 7 \Omega \cdot \mu\text{m}^2$ needed for 200 GHz clock rate

This slide presented at BCTM 2004 for phase-I 150GHz divider.

HBT metrics here invoked to demonstrate the phase-III 200GHz divider.



C_{cb}/I_c Charging Rate: ECL delays lower than CML

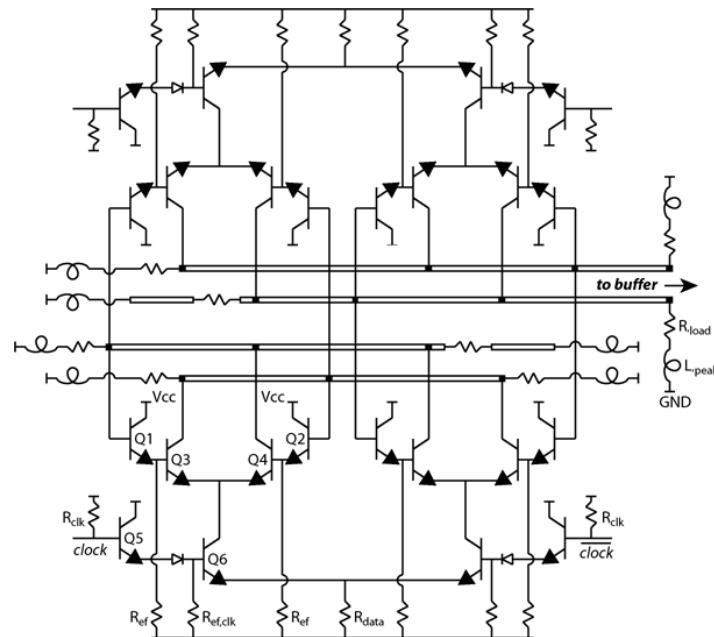
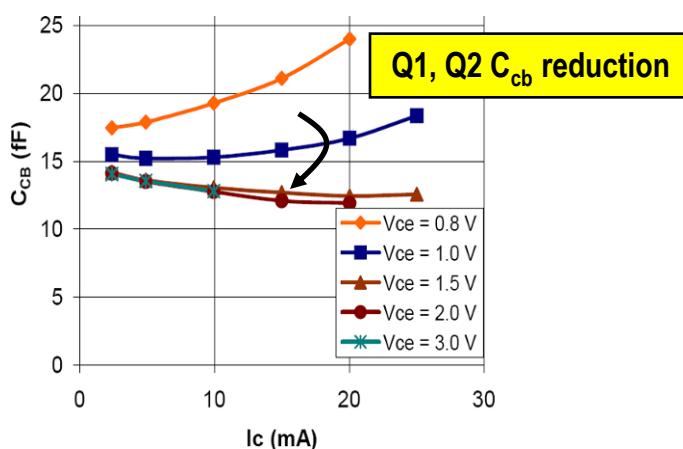


Design approach for 200GHz logic

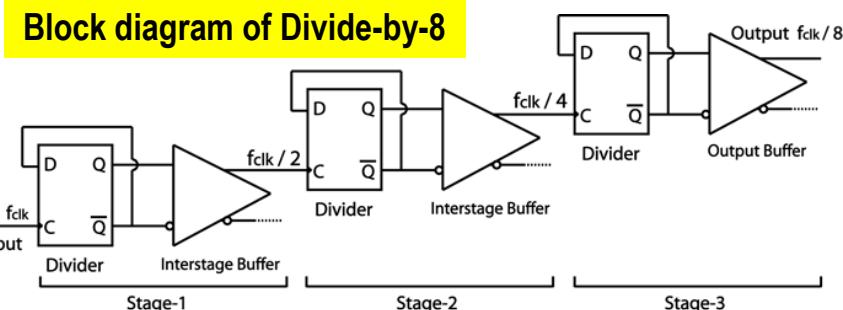
Chart 7

Approach: (new design elements presented in bold)

- Emitter coupled logic (ECL) topology
- Faster HBTs with lower C_{cb} and lower R_{ex} ($\Omega \cdot \mu\text{m}^2$)
 - **Scaled device from 0.5um to 0.25um**
 - 150nm collector, 30nm base (400GHz f_t , 650GHz f_{max})
- Reduce signal bus and loading delays
 - **Decreased device-to-device spacing**
- Thin-film microstrip with low loss $\epsilon_r = 2.7$
- Resistive pulldown voltage biasing
- Small peaking inductance L_{peak}
- **Emitter-follower HBTs having reduced C_{cb} (Q1, Q2)**
 - Collector-base DC voltage V_{cb} increased



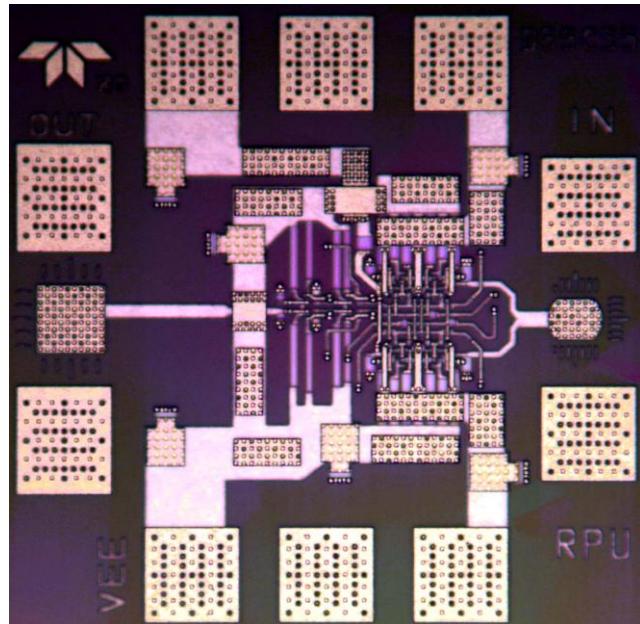
Schematic of a flip-flop configured as a static divider



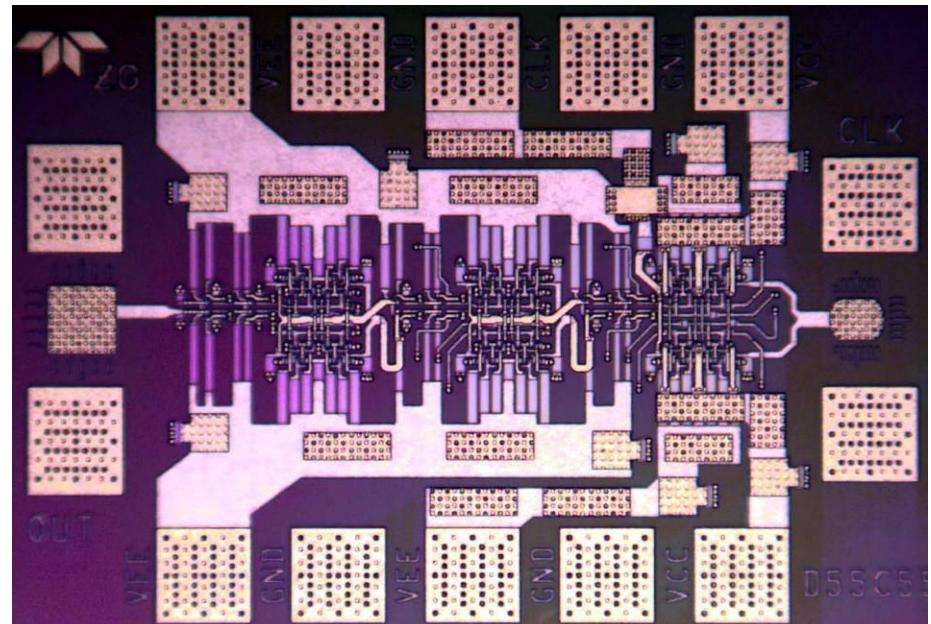
IC micrographs of the TSC 200GHz Static Frequency Dividers

Chart 8

Final fabrication, top-metal ground plane omitted

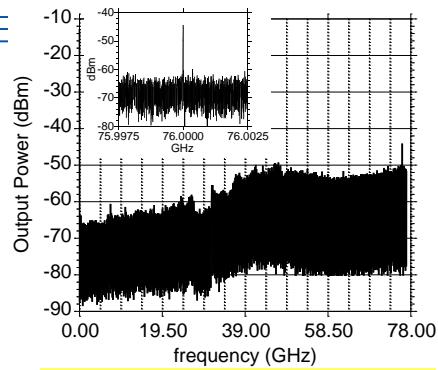
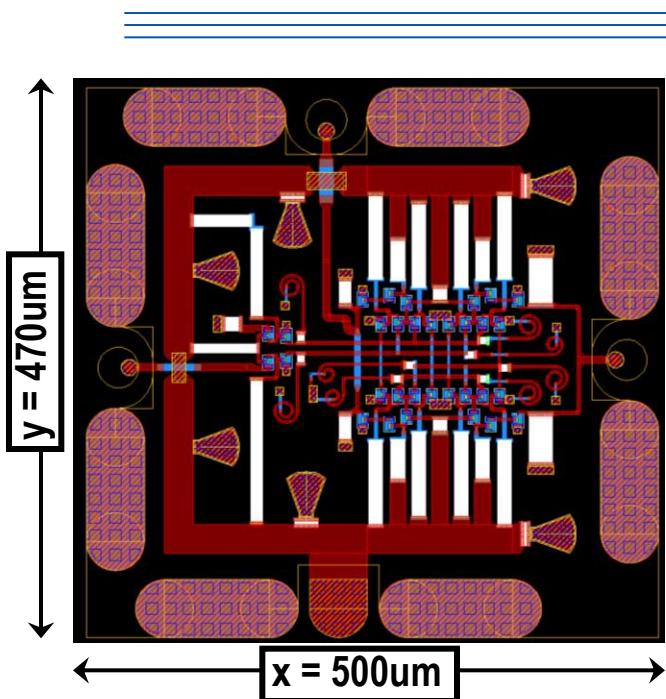


Divide-by-2 circuit, 36 HBTs (0.42×0.41-mm²)



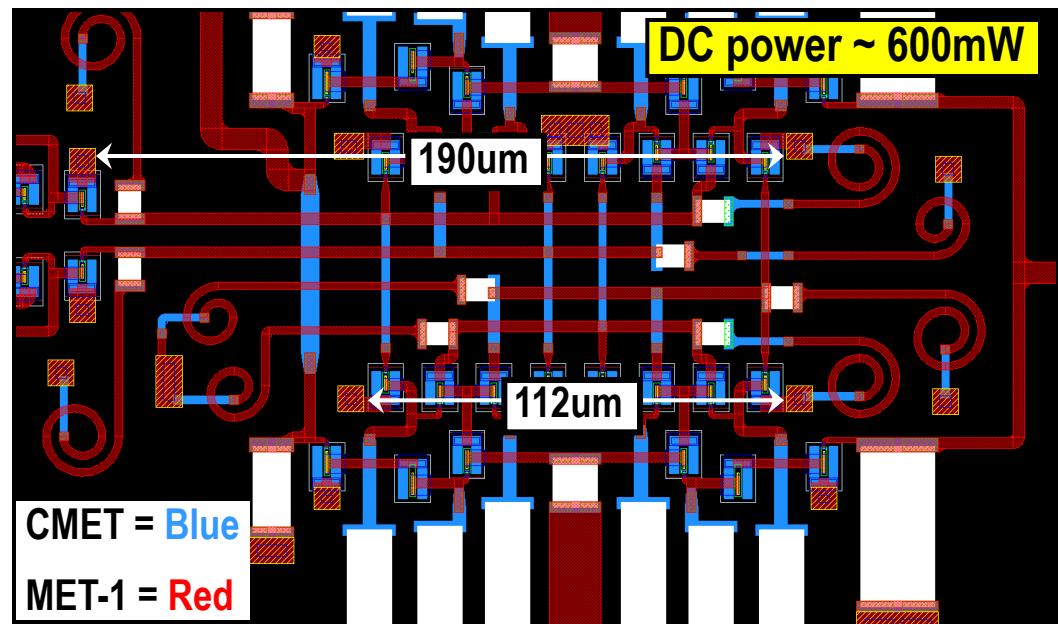
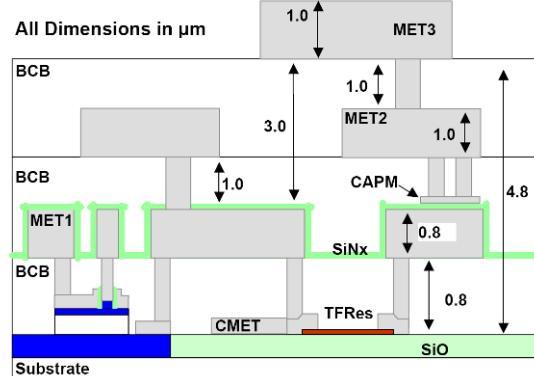
Divide-by-8 circuit, 108 HBTs (0.68×0.45-mm²)

TSC/UCSB/GSC 150GHz divider (September 2004)



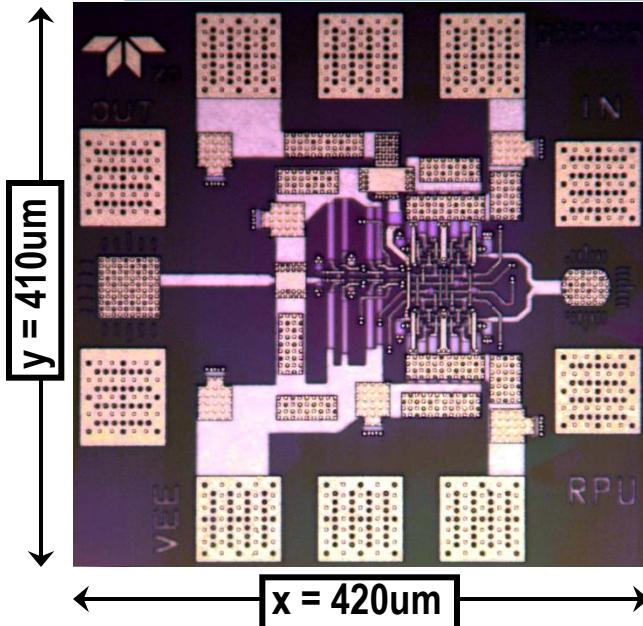
Phase-I divider @ 152GHz

Technology cross-section, phase-I

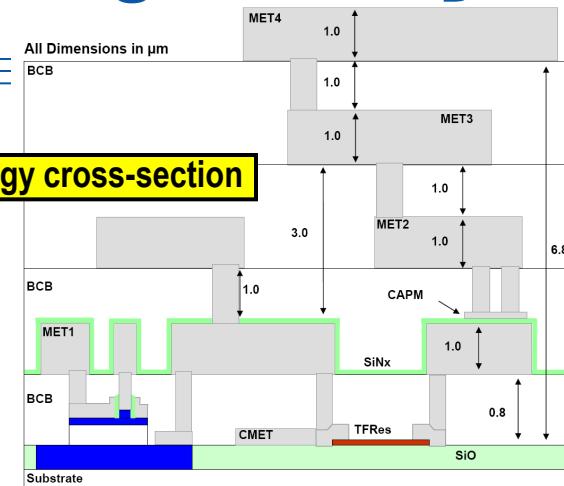


Close-up view of flip-flop interconnect, configured for divide-by-2

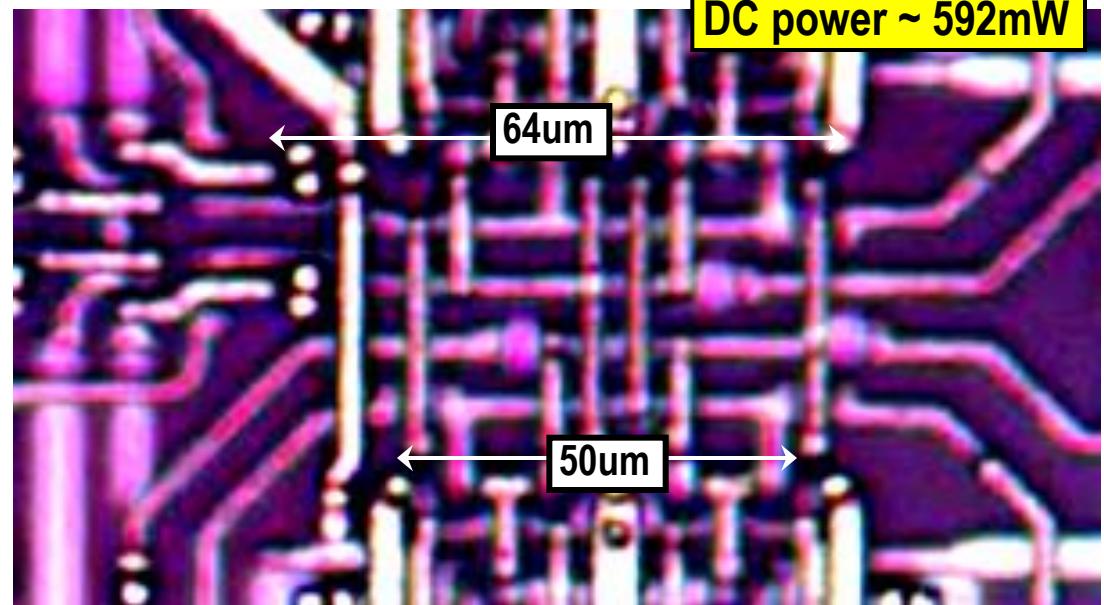
TSC/UCSB 200GHz divider – scaling summary



TSC mixed-signal technology cross-section



DC power $\sim 592\text{mW}$

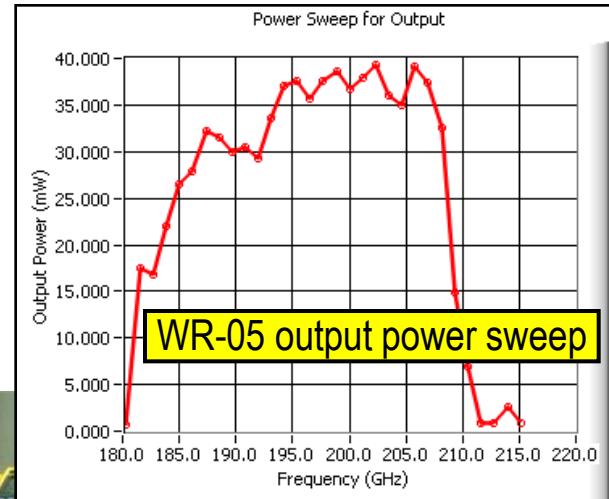
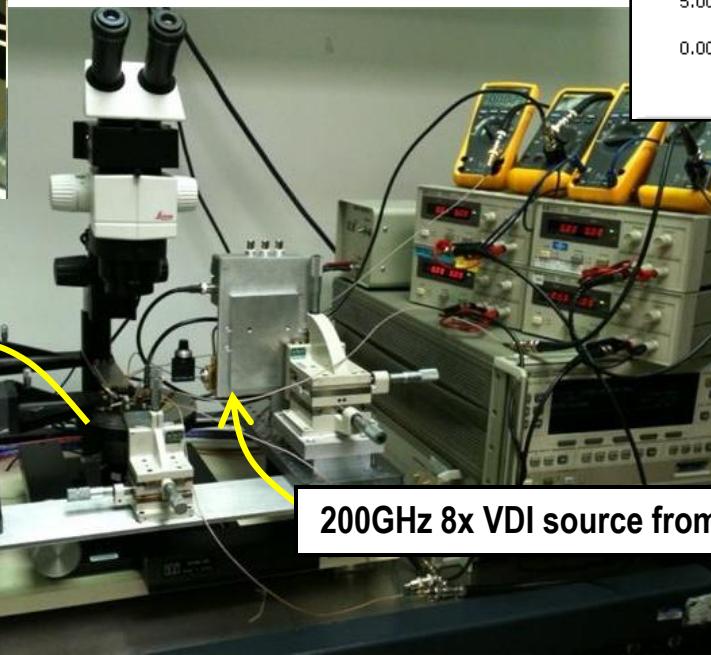
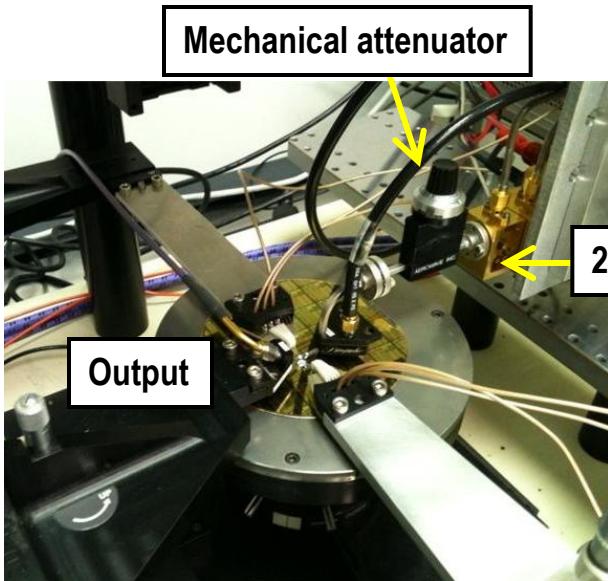


Close-up view of flip-flop interconnect, configured for divide-by-2

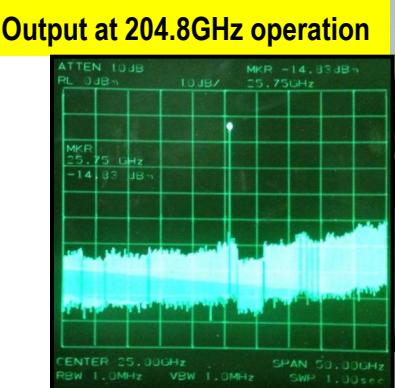
Simulated CLK rate, 213GHz

Probe-station for 200GHz divider testing

Chart 11



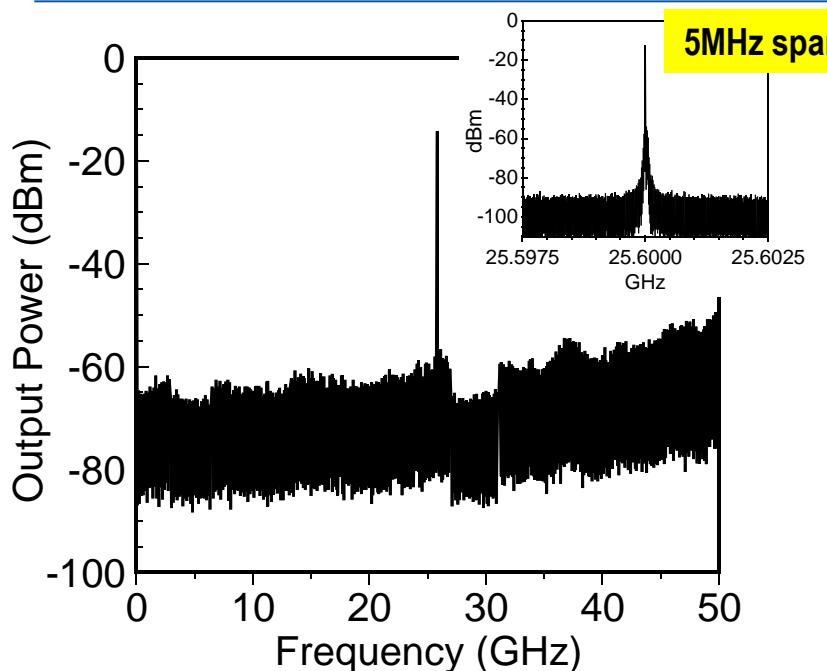
Close-up showing wafer probes



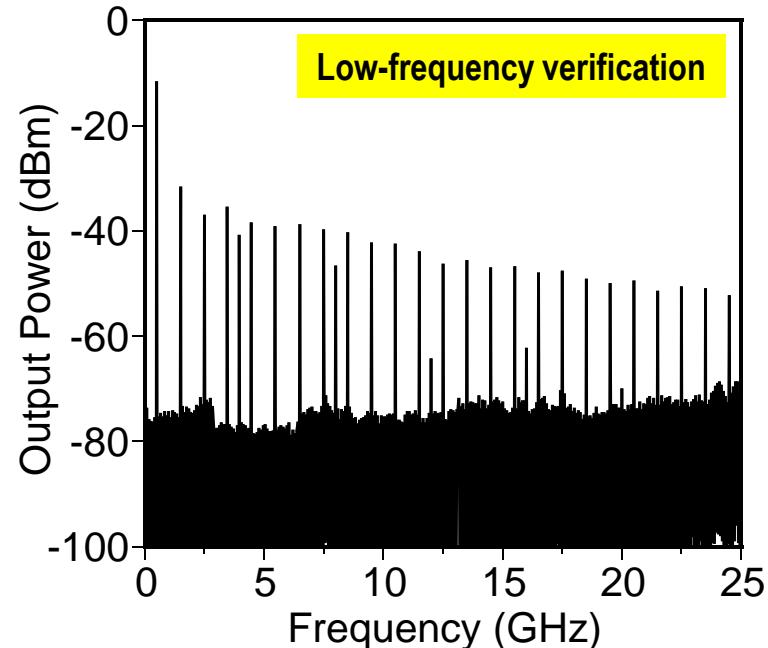
Probe station for 200GHz testing

Divide-by-8 static divider operating to 204.8GHz

Chart 12



Divider output – $f_{\text{clk}} = 204.8\text{GHz}$, $f_{\text{out}} = 25.60\text{GHz}$

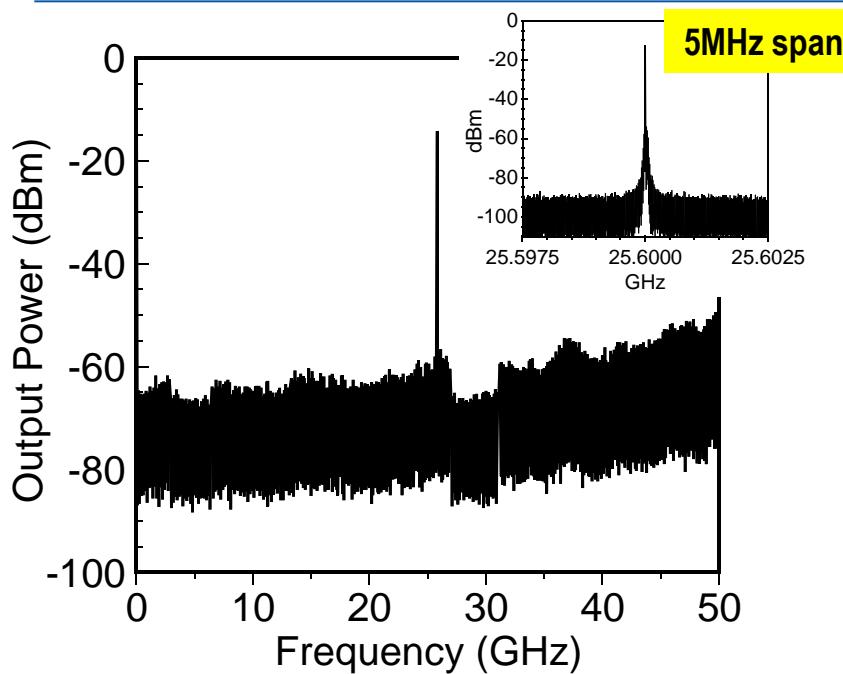


Divider output – $f_{\text{clk}} = 4.0\text{GHz}$, $f_{\text{out}} = 500\text{MHz}$

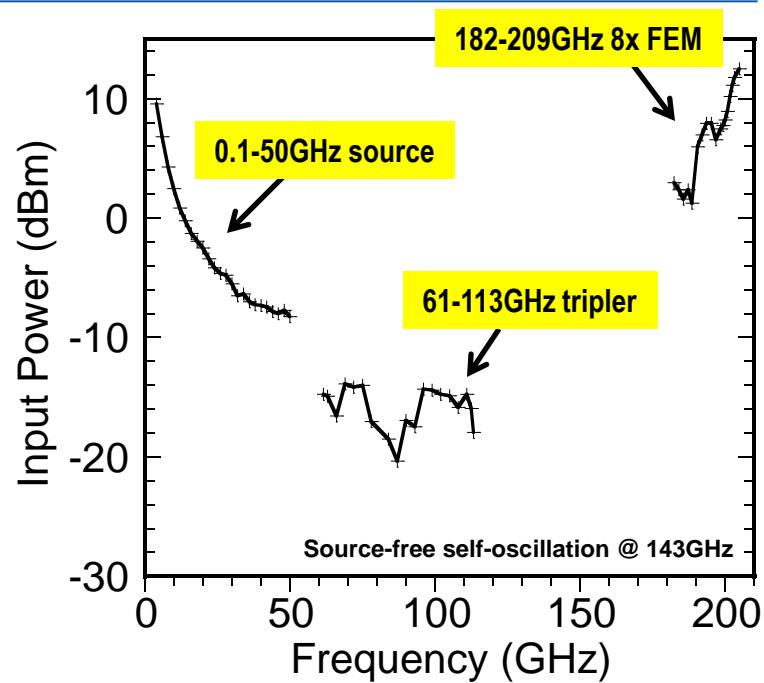
- Peak divider toggle rate is 204.8GHz
 - Expected output at 25.60GHz, no spectral content at lower frequencies
- Input divider operational down to 4.0GHz to confirm static operation at all frequencies
 - 3rd-stage divider is operating at 1.0GHz clock (differential 350mV_{p-p}), 500MHz final output
- P_{DC} of divide-by-8 circuit = 1.82W
 - Input divider operating at 204.8GHz, $P_{\text{DC}} = 592\text{mW}$

Sensitivity plot of the 204.8GHz static divider

Chart 13



Divider output – $f_{\text{clk}} = 204.8\text{GHz}$, $f_{\text{out}} = 25.60\text{GHz}$



Sensitivity plot, 204.8GHz static divider

- Sensitivity plot of the divider: 0.1-50GHz, 61.5-113.25GHz, 182.4-204.8GHz
- Expected trends of input power sensitivity versus frequency observed
- Source-free self oscillation (no input signal) reference to the input is 143GHz

Summary

Chart 14

- A record static divide-by-8 frequency divider has been demonstrated
 - 108 HBTs, all having 250nm features
 - TSC 4-metal layer, mixed-signal interconnect
 - Operational from 4.0GHz to 204.8GHz
 - Total $P_{DC} = 1.82W$, input divider only (no buffers) = 592mW

SUMMARY OF THE FASTEST REPORTED STATIC FREQUENCY DIVIDERS

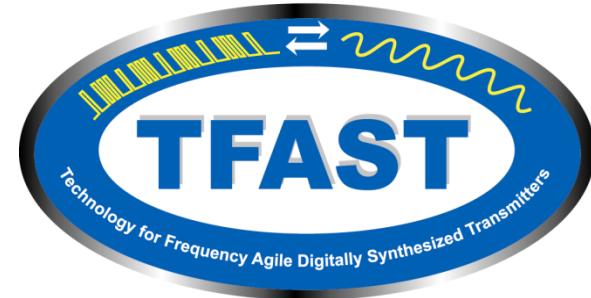
Max. Clock Freq. (GHz)	Division Rate	Technology	Scale (nm)	Reference
110	4	SiGe HBT	140	Infinion [3]
151.6	4	InP HBT	400	HRL [4]
152.0	2	InP HBT	500	Teledyne [1]
152	4	InP HBT	500	Lucent [5]
200.6	2	InP HBT	250	NGAS [6]
204.8	8	InP HBT	250	Teledyne, this work

- Continued increases to static divider toggle rate require balanced reductions to HBT base R_{bb} and emitter resistance R_{ex} , and junction capacitances C_{je} , C_{cb} .
 - Presentation (Tues-F1) by M. Urteaga discusses recent HBT developments

Acknowledgement

Chart 15

- This work was supported under the DARPA TFAST program, Sanjay Raman program manager.



Thank you!!