

1.0 THz f_{\max} InP DHBTs in a refractory emitter and self-aligned base process for reduced base access resistance

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We report 220 nm InP double heterojunction bipolar transistors (DHBTs) demonstrating $f_{\tau} = 480$ GHz and $f_{\max} = 1.0$ THz. Improvements in the emitter and base processes have made it possible to achieve a 1.0 THz f_{\max} even at 220 nm wide emitter-base junction with a 1.1 μm wide base-collector mesa. A vertical emitter metal etch profile, wet-etched thin InP emitter semiconductor with less than 10 nm undercut and self-aligned base contact deposition reduces the emitter semiconductor-base metal gap (W_{gap}) to ~ 10 nm, thereby significantly reducing the gap resistance term (R_{gap}) in the total base access resistance (R_{bb}), enabling a high f_{\max} device. Reduction in the total collector base capacitance (C_{cb}) through undercut in the base mesa below base post further improved f_{\max} . These devices employ a Mo/W/TiW refractory emitter metal contact which allows biasing the transistors at high emitter current densities (J_e) without problems of electromigration or contact diffusion under electrical stress [1].

Improved bandwidth for the HBTs can be achieved through epitaxial scaling of base (T_b) and collector (T_c) thicknesses for reduced transit delays; and lithographic scaling with lower contact resistivities for reduced RC delays [2]. For the DHBTs reported here, emitter design includes a 10 nm thick highly doped n-In_{0.53}Ga_{0.47}As cap ($N_d > 5 \times 10^{19} \text{ cm}^{-3}$) for reduced contact resistivity and a thin (30 nm) InP layer for controlled emitter undercut and reduced emitter depletion region resistance [3]. InGaAs base is 30 nm thick having a $9 - 5 \times 10^{19} \text{ cm}^{-3}$ doping gradient and T_c is 100 nm. The base-collector grade includes a 13.5 nm InGaAs setback and a 16.5 nm InGaAs/InAlAs chirped-superlattice grade. The epitaxial structure was grown by IQE Inc. on a 4" semi-insulating InP substrate [4]. Extrinsic base, in the emitter-base gap (W_{gap}), has a higher sheet resistance ($R_{\text{sh,ex}}$) than intrinsic base due to surface depletion from Fermi level pinning and surface damage from processing – $R_{\text{sh,ex}} = 920 \text{ } \Omega/\text{sq}$ and $R_{\text{sh,int}} = 710 \text{ } \Omega/\text{sq}$ measured from pinched and non-pinched TLM measurements. Thus, $R_{\text{gap}} = R_{\text{sh,ex}} \cdot W_{\text{gap}} / 2 \cdot L_e$ becomes a dominant component of R_{bb} for large W_{gap} [2]. For these HBTs, dry etch for Mo/W/TiW (10% Ti by weight) stack is optimized to obtain a vertical emitter metal profile; thin (30 nm) InP emitter layer is wet-etched for controlled semiconductor undercut (< 10 nm) and self-aligned base contact (Pt/Ti/Pd/Au) lift-off process is used. These features greatly reduce W_{gap} , and therefore R_{gap} , consequently increasing f_{\max} . This reduction in R_{bb} made it possible to achieve 1.0 THz f_{\max} even at 220 nm wide emitter with a 1.1 μm wide, misaligned base mesa. Fabrication details are as in [4].

1-67 GHz measurements of HBTs embedded in a ground-signal-ground pad structure were carried out after performing a standard line-reflect-reflect-match (LRRM) calibration on an Agilent E8361A PNA, bringing the reference planes to the probe tips. On wafer, short and open circuit pad structures identical to those used by the devices were measured after calibration to de-embed associated transistor pad parasitics. The same calibration and de-embedding procedures were used for 80-105 GHz measurements on Agilent 8510XF system. Peak RF performance for HBTs with $A_{je} = 0.22 \times 2.7 \text{ } \mu\text{m}^2$ was obtained at $I_c = 12.1 \text{ mA}$ and $V_{ce} = 1.64 \text{ V}$ ($V_{cb} = 0.7 \text{ V}$, $J_e = 20.4 \text{ mA}/\mu\text{m}^2$, $P = 33.4 \text{ mW}/\mu\text{m}^2$). Extrapolations from single-pole fit to the measured current gain H_{21} and Mason's Unilateral gain U indicate cut off frequencies $f_{\tau} = 480$ GHz and $f_{\max} = 1.0$ THz. Total emitter access resistivity $\rho_{\text{ex}} \sim 4.2 \text{ } \Omega \cdot \mu\text{m}^2$ was extracted from RF data. HBTs with an emitter junction width of 220 nm (W_e) show peak DC common emitter current gain $\beta = 17$ and common emitter breakdown voltage $V_{\text{BR,CEO}} = 3.7 \text{ V}$ ($J_e = 0.1 \text{ mA}/\mu\text{m}^2$). The Kirk effect is observed at $J_e = 23 \text{ mA}/\mu\text{m}^2$ ($V_{cb} = 0.7 \text{ V}$) when f_{τ} falls to 95% of its peak value.

A linear fit to the extracted C_{cb} variation with emitter length (L_e) has ~ 0 fF intercept suggesting negligible capacitance contribution from the base post. This is also evident from weak dependence of f_{τ} on L_e ; peak f_{τ} changes from 480 GHz to 465 GHz for L_e increase from 3 μm to 5 μm . For low R_{bb} , base metal resistance $R_{\text{metal}} = R_{\text{sh,m}} \cdot L_e / 6 \cdot W_{\text{bc}}$ [2] becomes a significant fraction of total R_{bb} and thus f_{\max} decreases with increase in L_e . Further improvement in f_e/f_{\max} can be achieved through reduced emitter and base-collector junction areas and lower contact resistivities.

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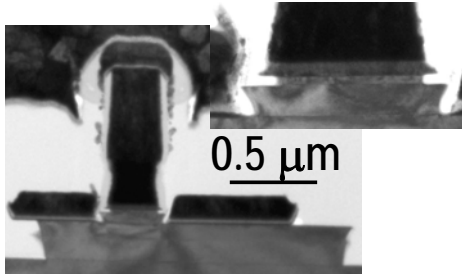


Fig. 1. Cross-sectional TEM of emitter mesa of DHBT showing the emitter profile with 220 nm wide emitter-base junction and 1.1 μm wide, non-symmetric base-collector mesa. Magnified view of the emitter mesa shows the small undercut in InP emitter and narrow base-emitter gap ($W_{gap} \sim 10$ nm)

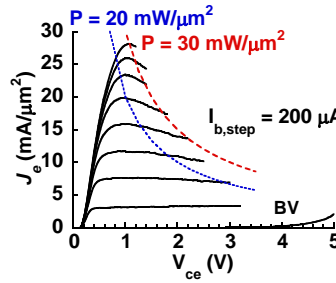


Fig. 2. Common-Emitter current density-voltage (J_e - V) characteristics of a DHBT with $A_{je} = 0.22 \times 4.7 \mu\text{m}^2$

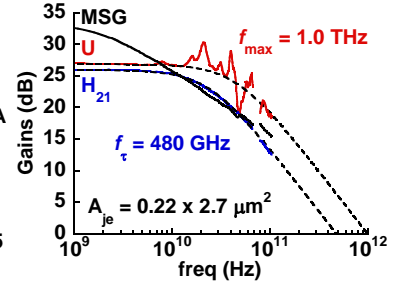


Fig. 3. Measured RF gains for the DHBT in 1 - 67 GHz and 80-105 GHz bands using off-wafer LRRM calibration in a lumped pad structure. The DHBT was biased at $I_c = 12.1$ mA, $V_{ce} = 1.64$ V

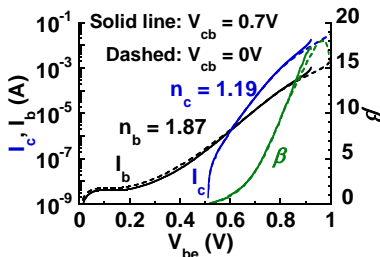


Fig. 4. Gummel Plot of a DHBT with $A_{je} = 0.22 \times 4.7 \mu\text{m}^2$

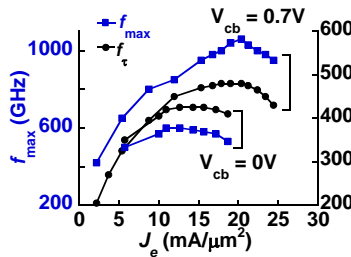


Fig. 5. f_{τ}/f_{max} dependence on V_{cb} and J_e

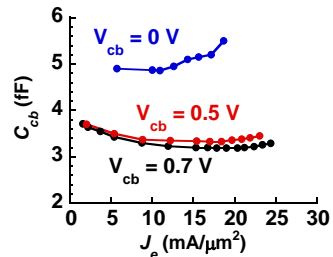


Fig. 6. Variation in C_{cb} with V_{cb} and J_e

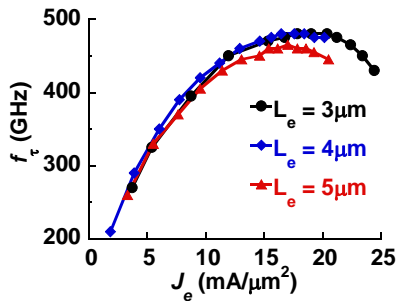


Fig. 7. Variation in f_{τ} with J_e for different L_e at $V_{cb} = 0.7$ V for DHBTs having $W_e = 220$ nm and same base-collector mesa width

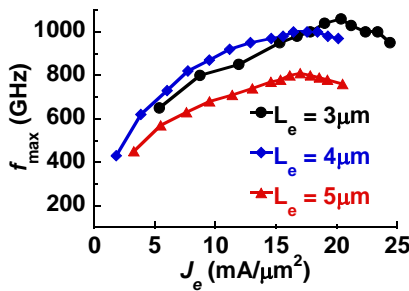


Fig. 8. Variation in f_{max} with J_e for different L_e at $V_{cb} = 0.7$ V for DHBTs having $W_e = 220$ nm and same base-collector mesa width

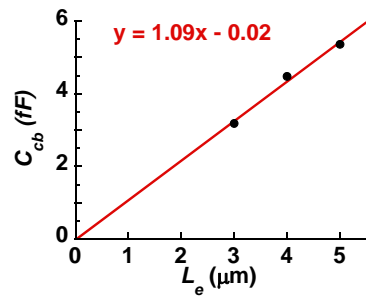


Fig. 9. Variation in extracted C_{cb} with L_e for $W_e = 220$ nm and same base-collector mesa width

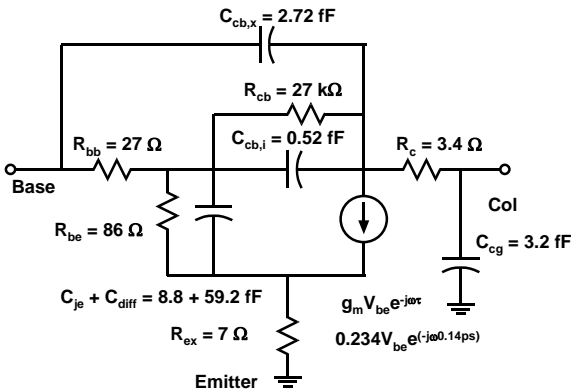


Fig. 10. Hybrid- π equivalent circuit at peak RF performance from 1 - 67 GHz RF data for the bias conditions: $I_c = 12.1$ mA, $V_{ce} = 1.64$ V

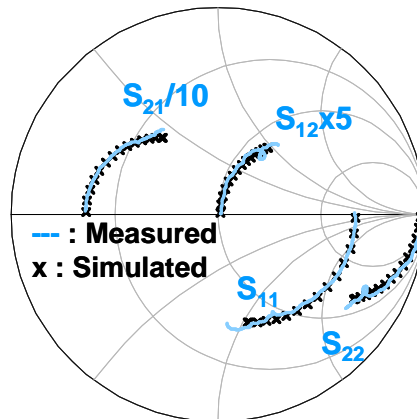


Fig. 11. 1 - 67 GHz measured and simulated S-Parameters from equivalent circuit model in Fig 10