

# A 200 GHz InP HBT Direct-Conversion LO-Phase-Shifted Transmitter/Receiver with 15 dBm Output Power

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# Outline

- Motivation
- Overview
- Transceiver circuit design
- Measured results
- Summary

# Wireless Communication @ 200 GHz

- **Motivation**

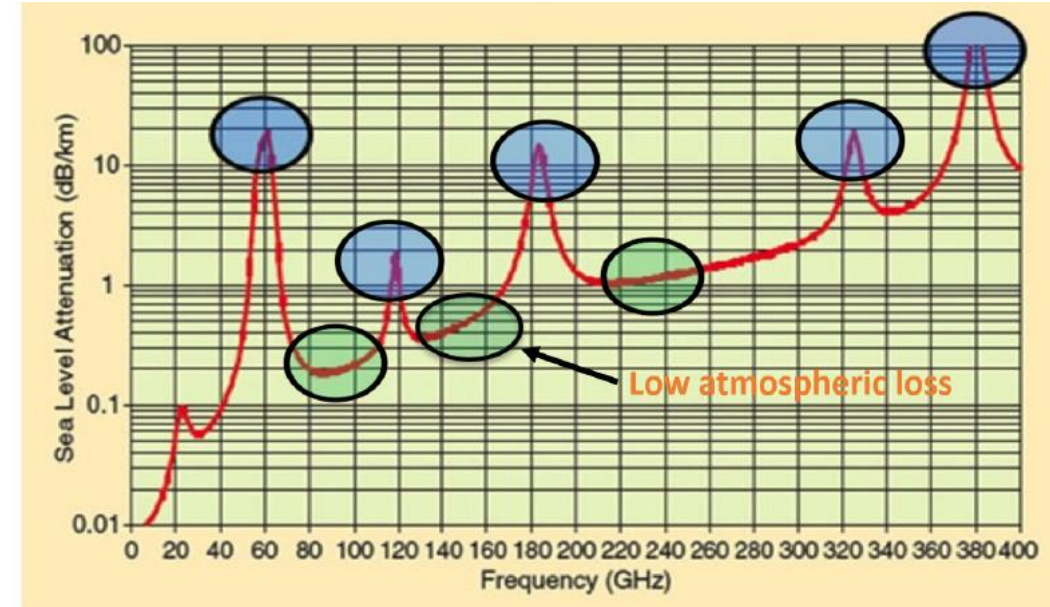
- Large available BW → High data rate (6G)
- Low atmospheric loss @ 200 GHz band

- **Challenges**

- Short wavelength → High path loss
- Low transistor gain → Low efficiency → Low battery life

- **Proposed 200 GHz transceiver**

- InP-HBT → High  $P_{out}$  & high efficiency
- Mixed use of normal & inverted microstrip
- Integrated LO phase shifter → Phased-array



**Normal microstrip**

1.1 dB/mm @200GHz 😊

Ground holes 😞

PA & LNA



**Inverted microstrip**

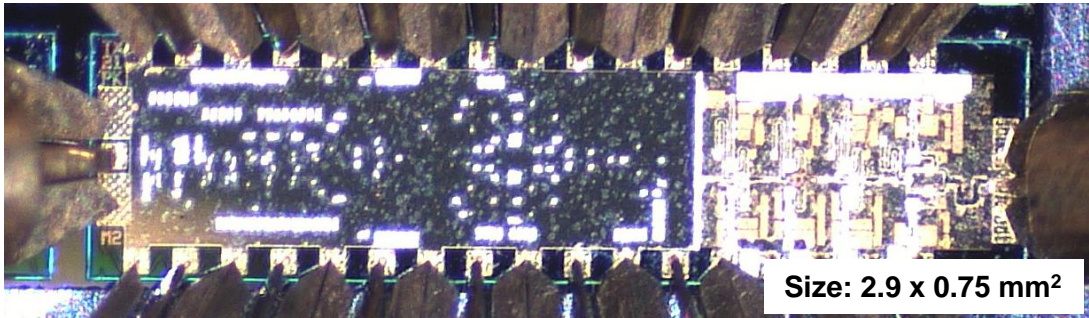
2.5 dB/mm @200GHz 😞

Continuous GND 😊

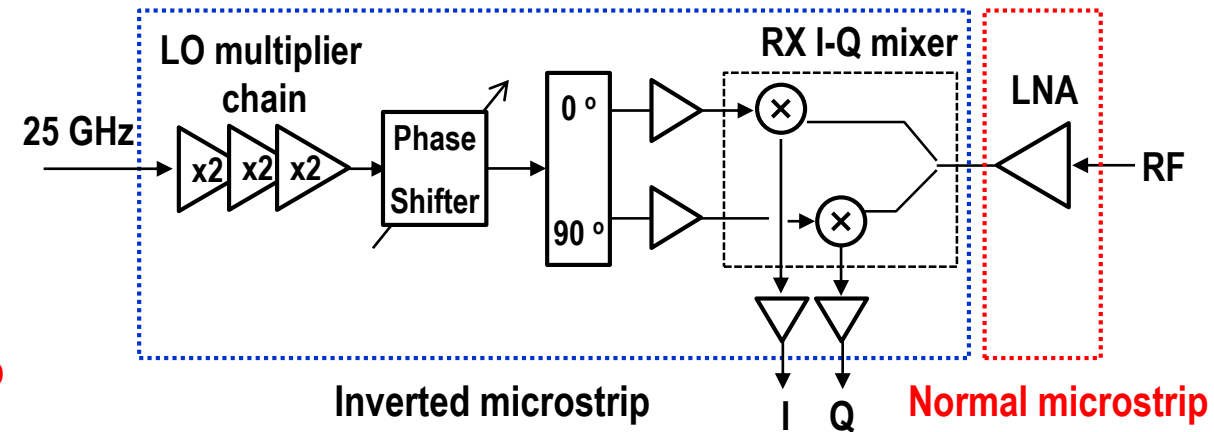
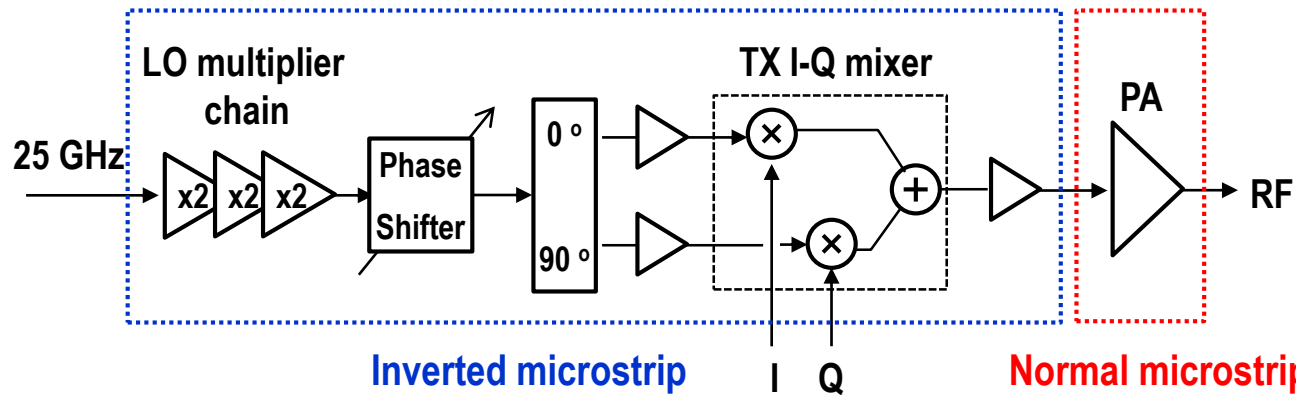
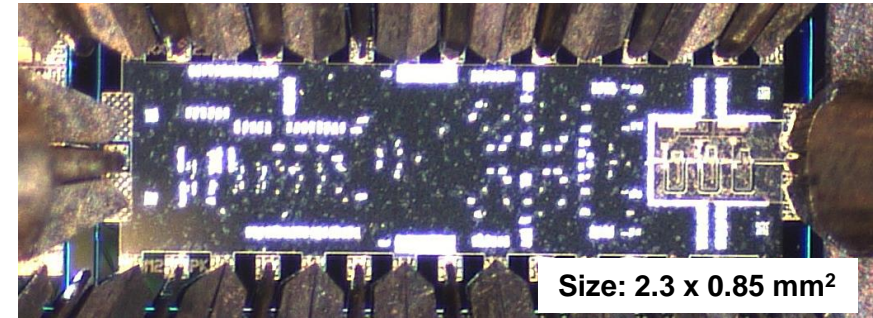
High-density blocks

# Proposed 200 GHz Transmitter / Receiver

## 200 GHz direct-conversion TX



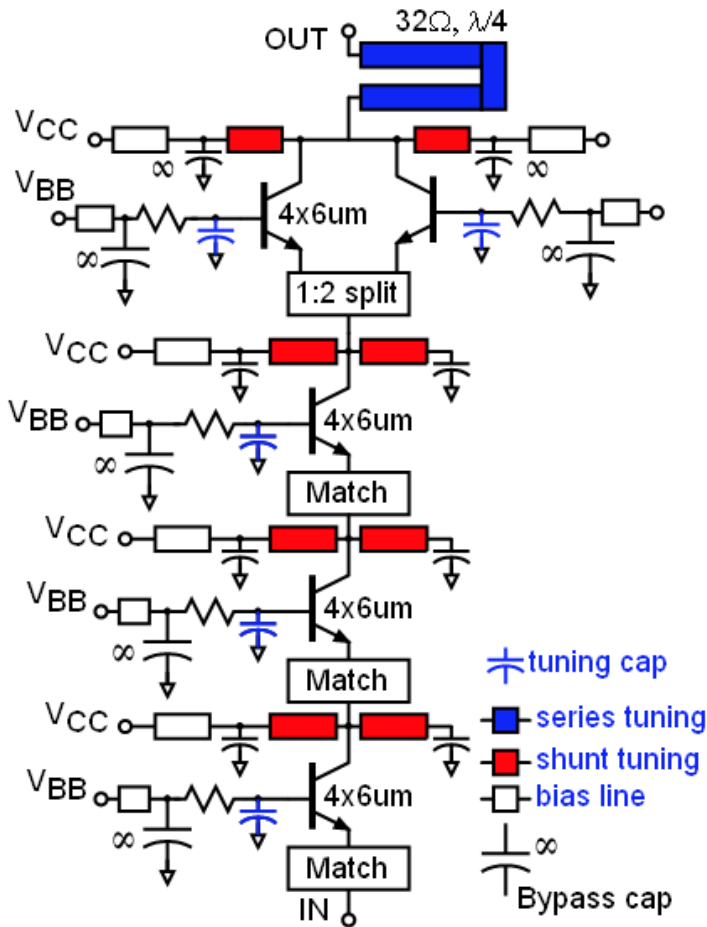
## 200 GHz direct-conversion RX



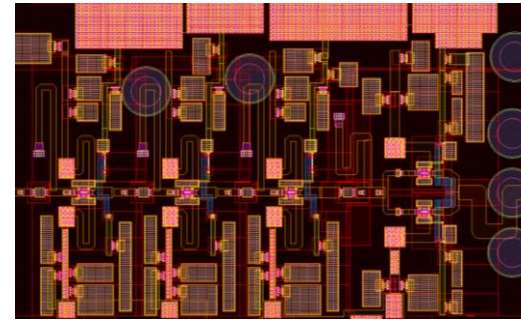
- PA & LNA: Normal microstrip for best PAE and lowest NF
- Mixer, LO multiplier, phase shifter: Inverted microstrip for low-inductance ground
- Integrated LO phase shifter enables phased-array operation of multiple ICs

# 200 GHz PA Design

## PA schematic



## PA layout

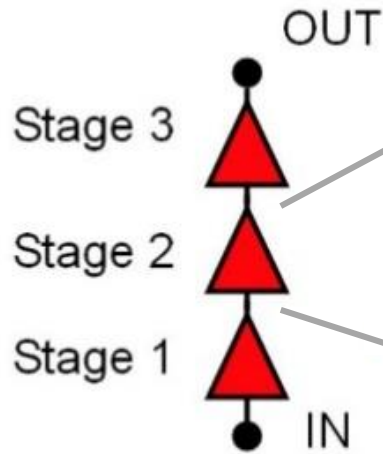


Size: 850 x 550  $\mu\text{m}^2$

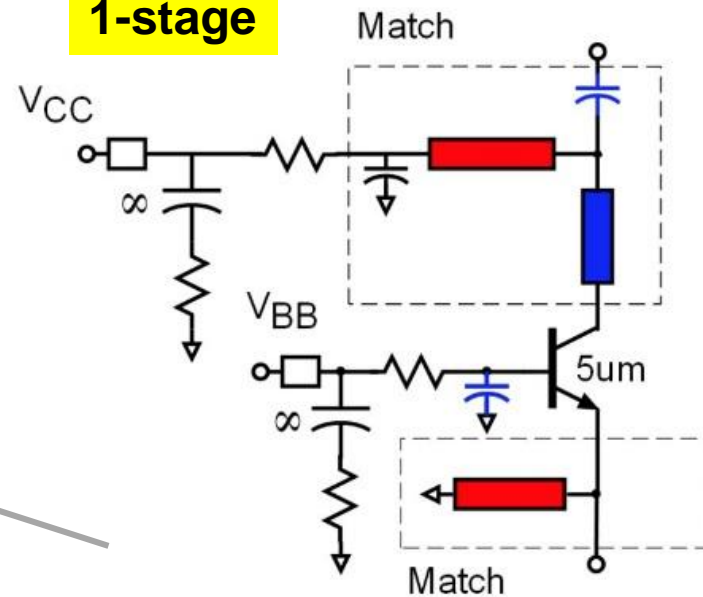
- 4-stage common-base w/  $C_{\text{base}}$ 
  - Higher efficiency @OP1dB than common-emitter
  - Higher efficiency @OP1dB than common-base with no  $C_{\text{base}}$
- Low-loss 2:1 combiner w/ a single  $\lambda/4$  line & shunt L
- Sim:  $P_{\text{sat}} = 17\text{dBm}@200\text{GHz}$ ,  $S_{21} > 20\text{dB}$ ,  $P_{\text{DC}} = 450\text{mW}$

# 200 GHz LNA Design

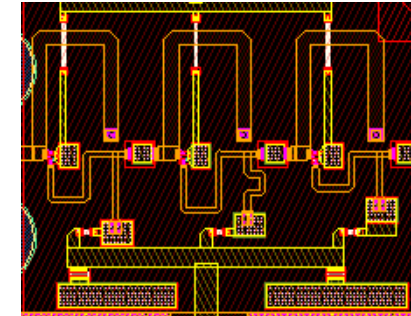
## 3-stage LNA



## 1-stage



## 3-stage LNA layout

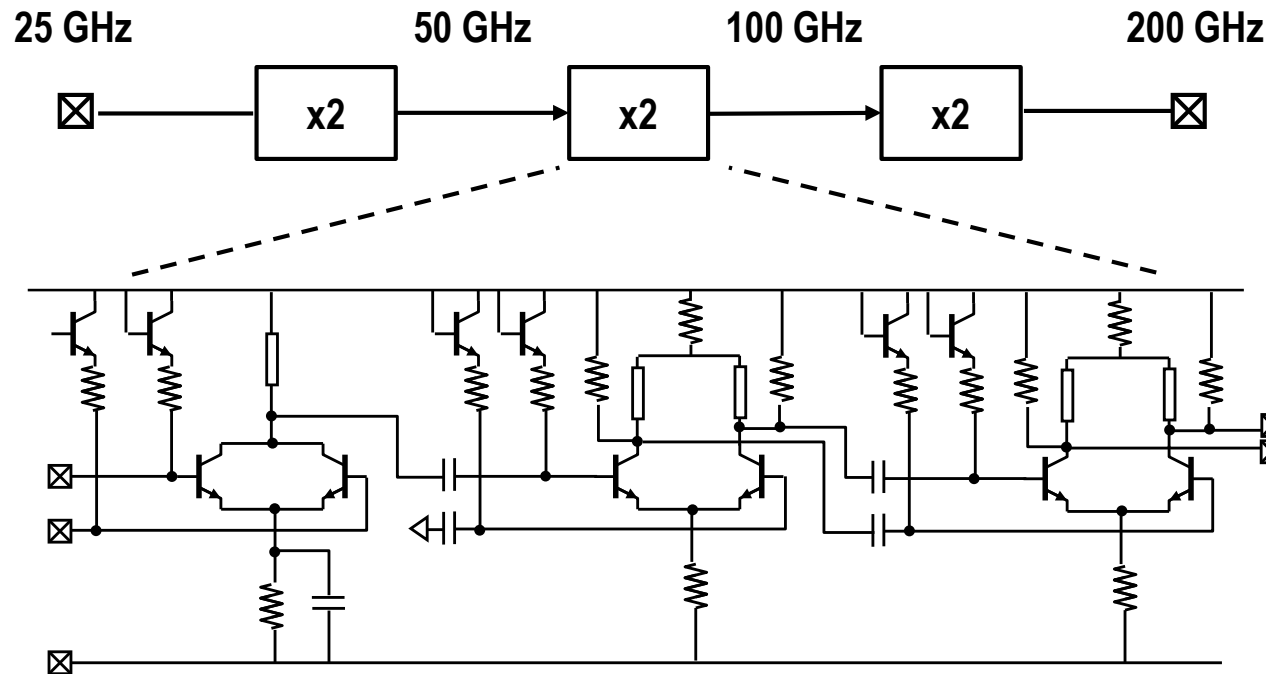


Size: 350 x 250  $\mu\text{m}^2$

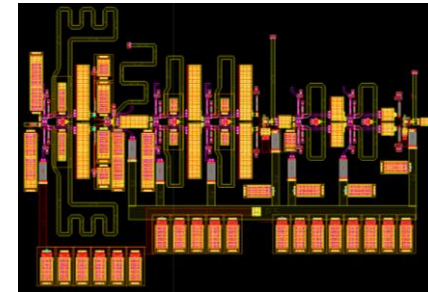
- 3-stage common-base (CB)
- Base cap. adjusted for simultaneous noise &  $S_{11}$  matching
- Emitter length scaled for minimum input matching loss
- Simulation:  $S_{21} = 15\text{dB}$ , 3-dB BW = 35GHz,  $P_{\text{DC}} = 14\text{mW}$

# LO Frequency Multiplier Design

**x8 LO multiplier schematic**



**Multiplier layout**

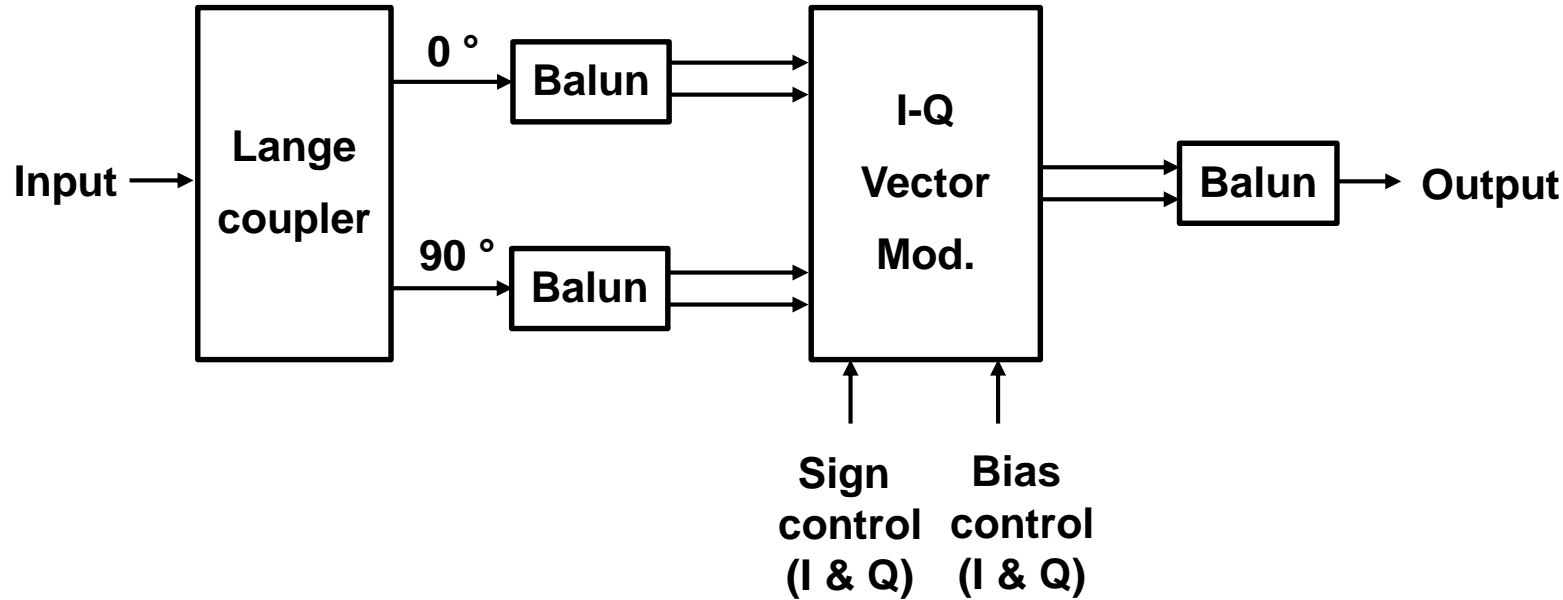


**Size: 580 x 400  $\mu\text{m}^2$**

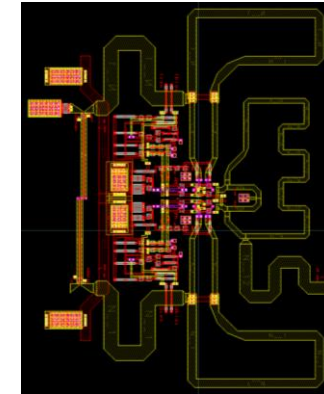
- Cascade of three push-push doublers  $\rightarrow$  x8 LO multiplier
- Capacitive emitter degeneration  $\rightarrow$  Operates with wider ranges of  $P_{in}$
- Simulation:  $P_{out} > 0\text{dBm}$  for 180-230GHz (BW = 50GHz),  $P_{DC} = 250\text{mW}$

# 200 GHz LO Phase Shifter

Phase shifter schematic



Phase shifter layout

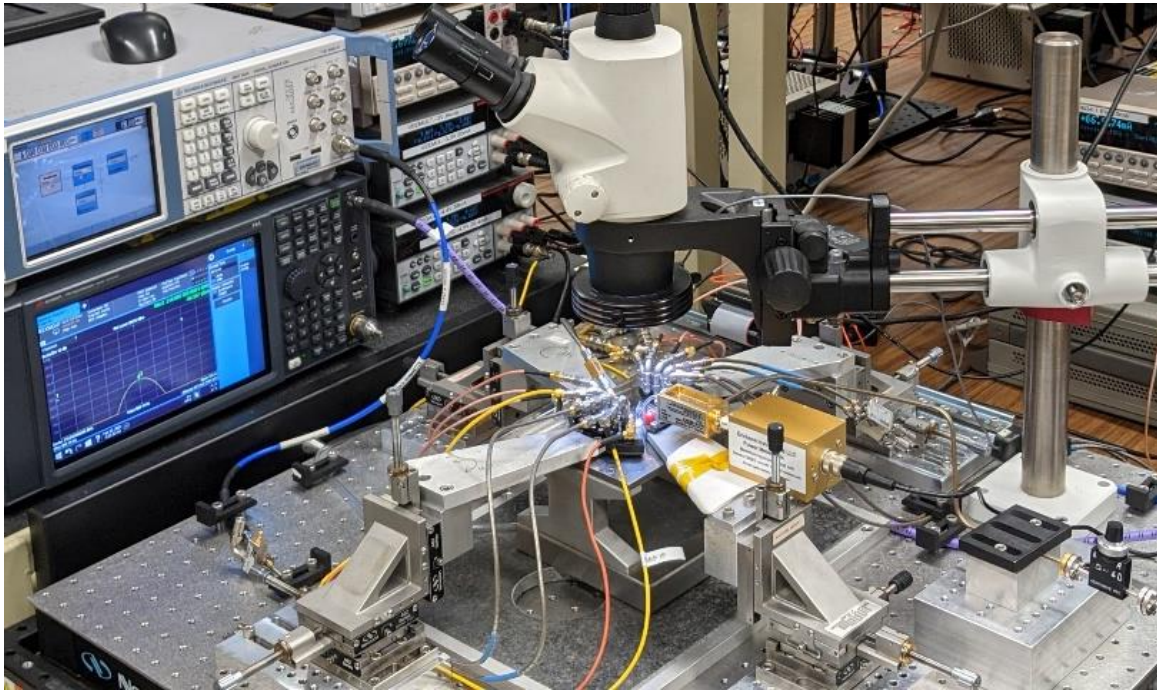
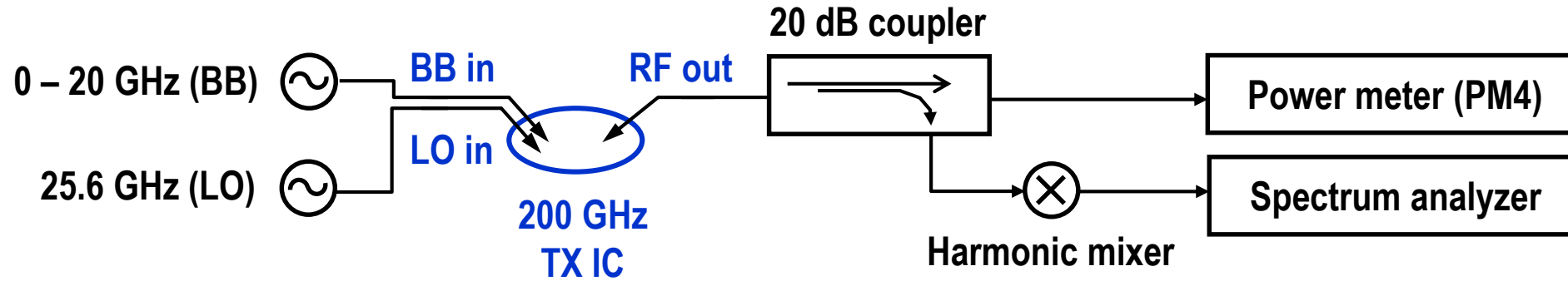


Size: 300 x 400  $\mu\text{m}^2$

- Vector-modulator-based phase shifter
- Wideband operation by using Lange coupler
- Sim: I/Q phase error < 2deg, mag. error < 0.3dB for 170-250GHz,  $P_{DC} = 100\text{mW}$



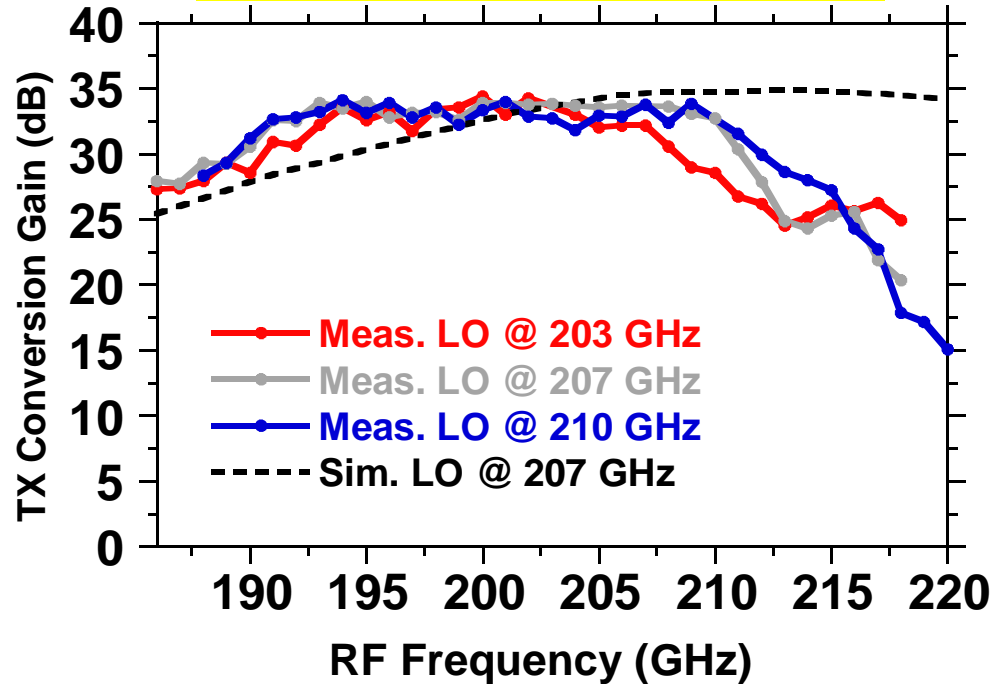
# Transmitter Testing Setup



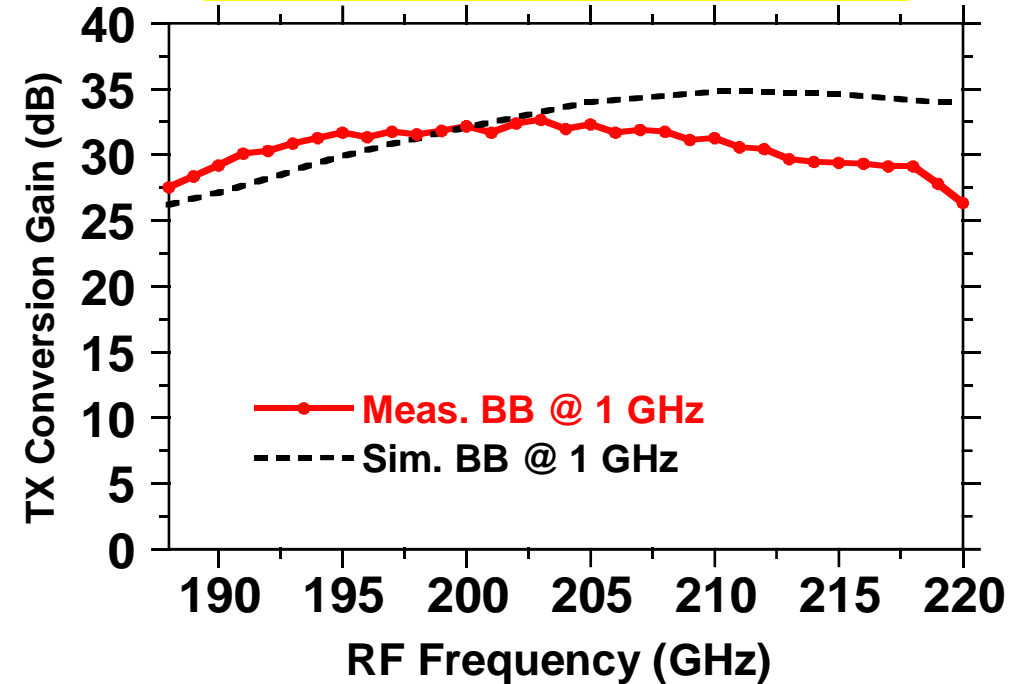
- 140-220 GHz (WR5) on-wafer testing
- Simultaneous freq. & power testing
- TX used as a calibration reference

# Measured TX Conversion Gain

Conversion Gain @ fixed  $f_{LO}$



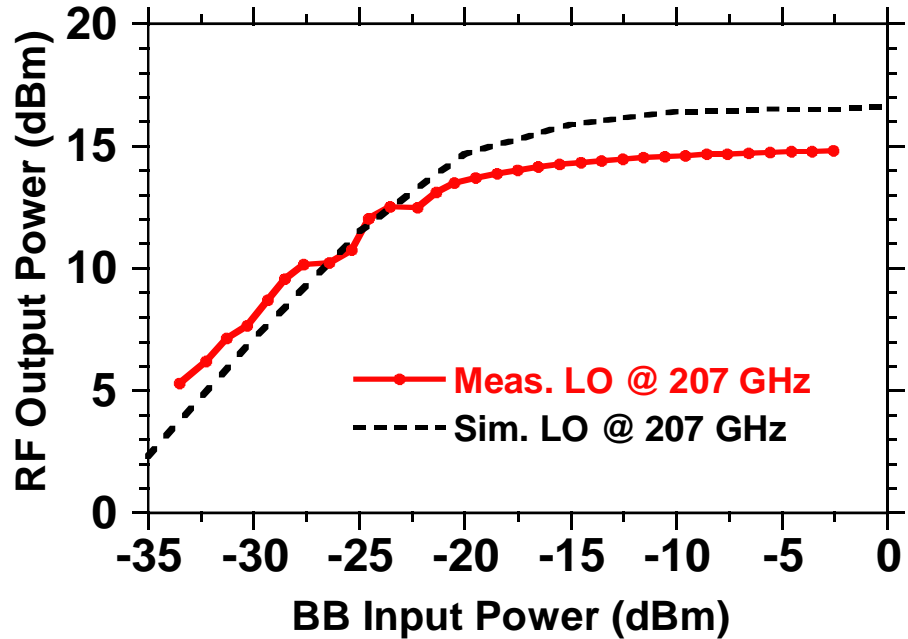
Conversion Gain @ fixed  $f_{BB}$



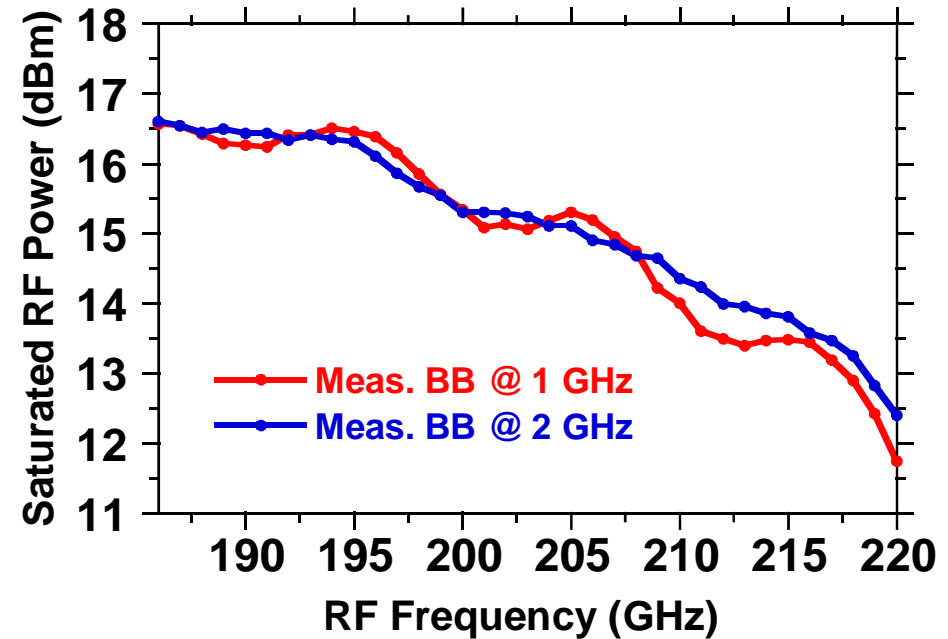
- Peak conversion gain = 34 dB
- 3-dB bandwidth > 20 GHz
- LO multiplier tuning bandwidth > 30 GHz

# Measured TX Output Power

$P_{out}$  vs  $P_{in}$  @  $f_{LO}=207$  GHz ( $f_{BB}=1$  GHz)

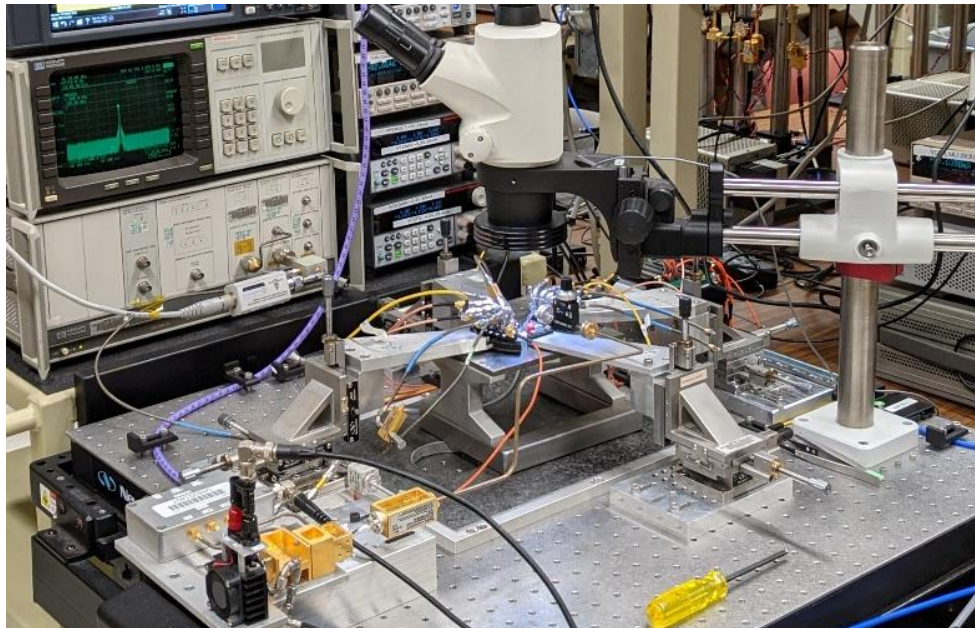
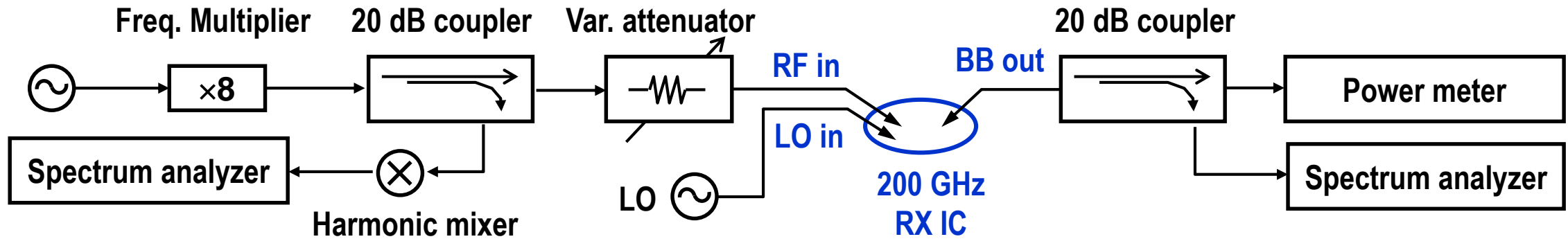


$P_{sat}$  vs  $f_{RF}$



- $P_{sat} = 16.5$  dBm @  $f_{RF} = 195$  GHz,  $15.3$  dBm @  $f_{RF} = 200$  GHz
- $P_{DC} = 1,250$  mW

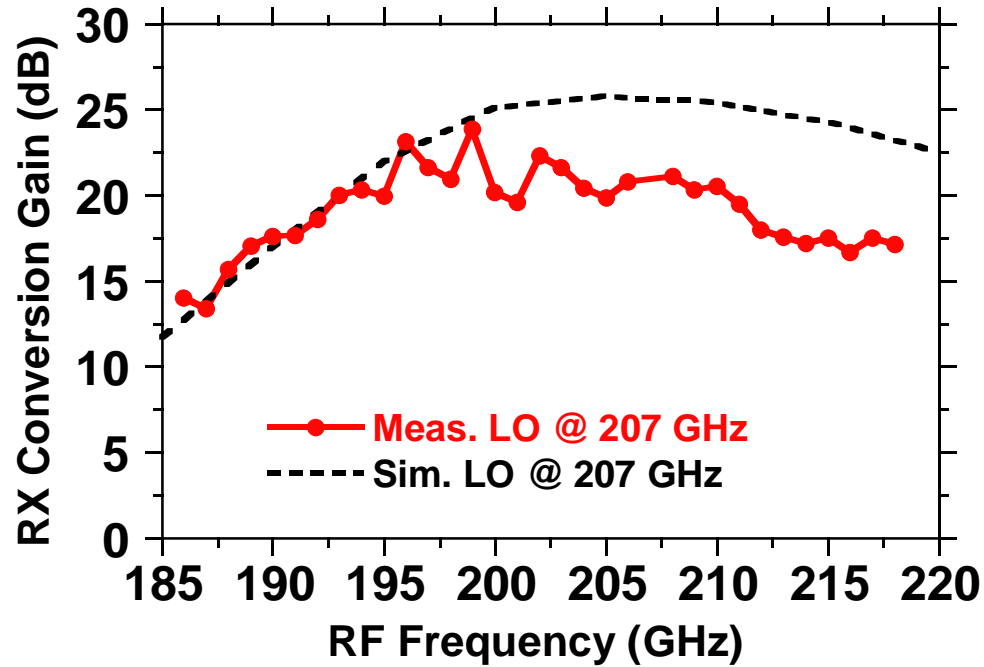
# Receiver Testing Setup



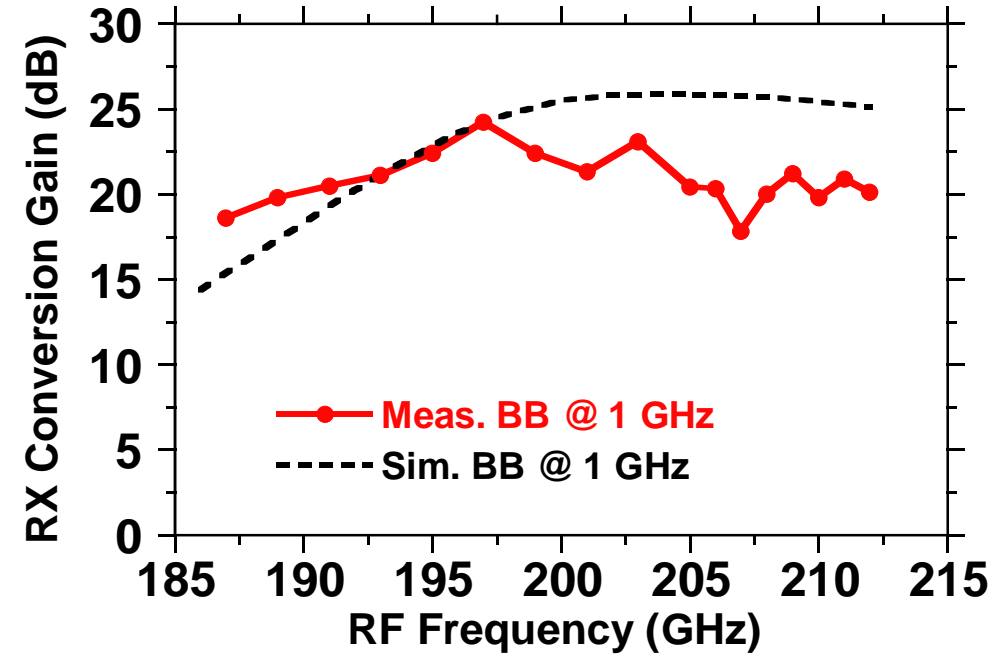
- 140-220 GHz (WR5) on-wafer testing
- Simultaneous freq. & power testing
- RX driven by multiplier & variable attenuator

# Measured RX Conversion Gain

Conversion Gain @ fixed  $f_{LO}$



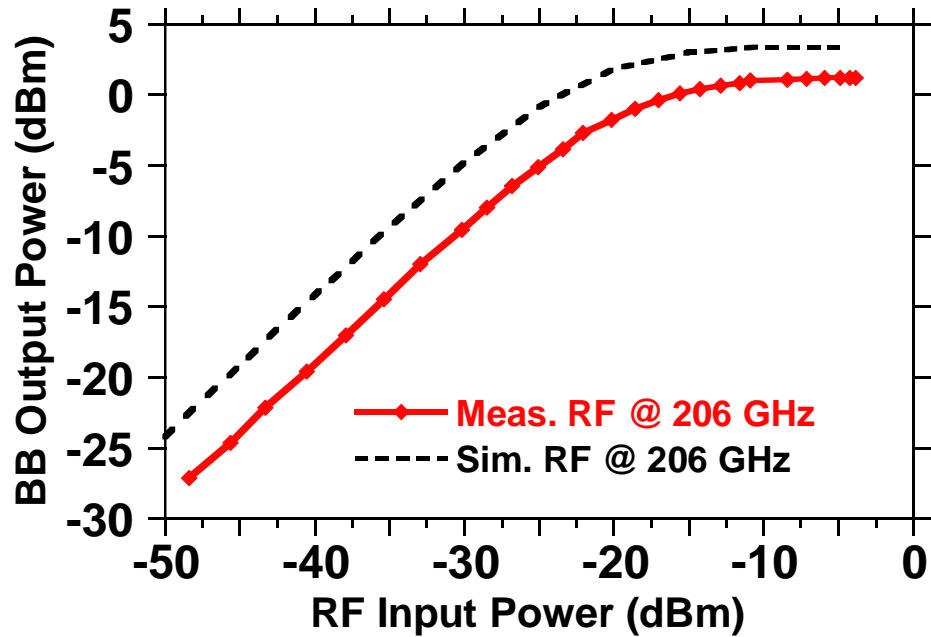
Conversion Gain @ fixed  $f_{BB}$



- Peak conversion gain = 25 dB
- LO multiplier tuning bandwidth > 25 GHz

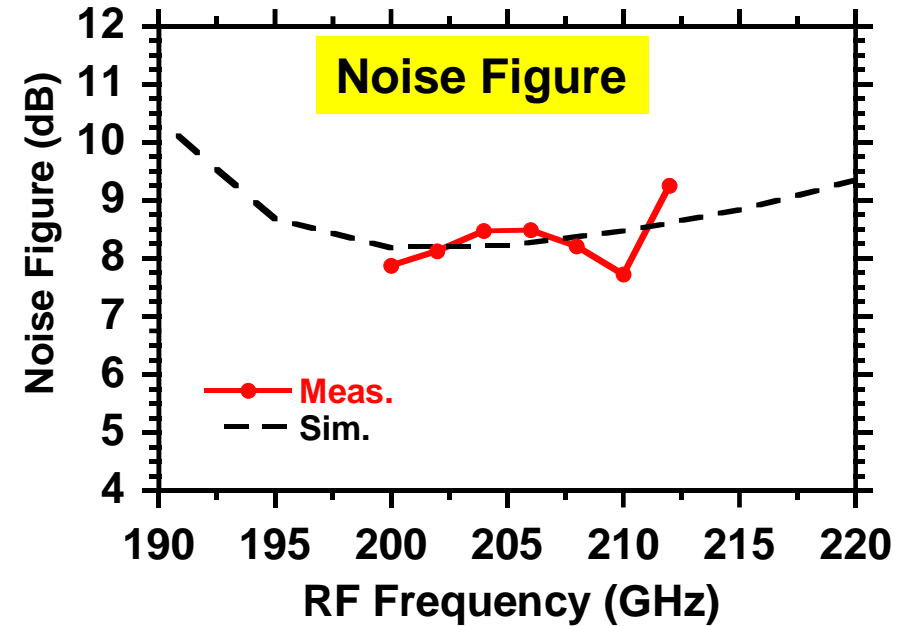
# Measured RX Power & Noise Figure

$P_{out}$  vs  $P_{in}$  @  $f_{LO}=206$  GHz ( $f_{BB}=1$  GHz)



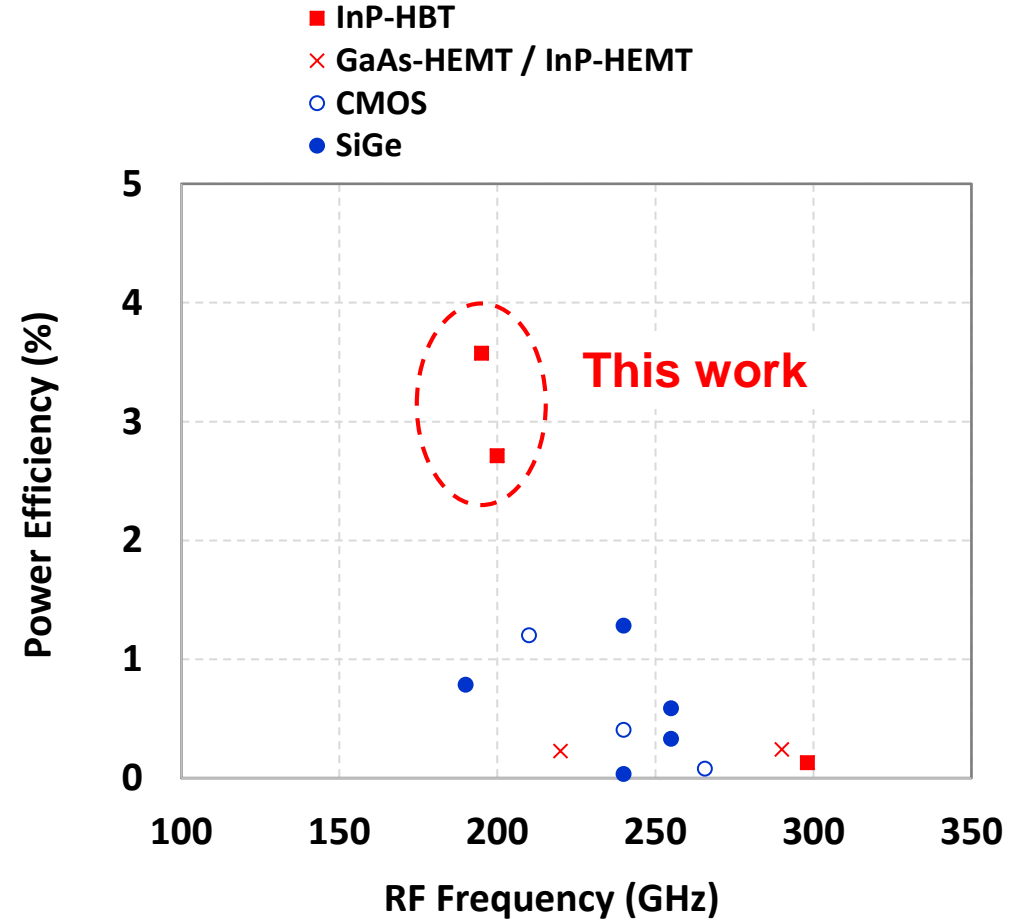
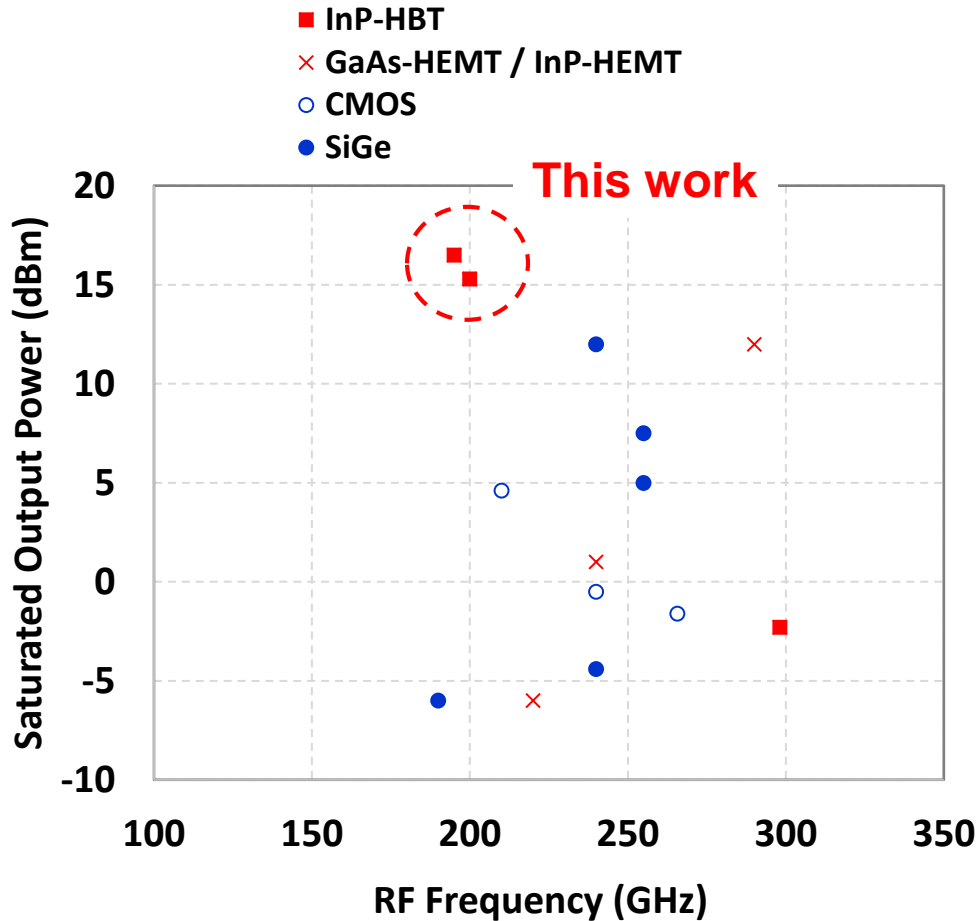
- Input  $P_{1dB} = -24$  dBm
- $P_{sat} = +1$  dBm
- $P_{DC} = 825$  mW

VDI-WR5.1-NS



- NF = 7.7 – 9.3 dB (200-212 GHz)

# Performance Comparison of Transmitter



$$\left( \text{Power efficiency} = \frac{P_{sat}}{P_{DC}} \right)$$



# Summary

- 200 GHz direct-conversion transmitter / receiver in InP HBT
- Highest  $P_{out}$  and efficiency, among all integrated TX beyond 200 GHz
- Modulated testing is under way





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Thank you very much!



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# Performance Comparison

Ref.	Technology	Integrated TX circuit blocks	Freq. (GHz)	$P_{\text{sat}}$ (dBm)	$P_{\text{DC}}$ (mW)	Efficiency (%)
[2]	0.1 $\mu\text{m}$ GaAs mHEMT	IF-mixer, LO multiplier ( $\times 2$ ), PA, antenna	220	-6	110	0.23
[3]	50nm GaAs mHEMT	IF-mixer, PA	240	1	N/A	N/A
[4]	32nm SOI CMOS	LO VCO, OOK mod, PA, antenna	210	4.6	240	1.20
[5]	65nm CMOS	IQ-mixer, tripler	240	-0.5	220	0.41
[6]	250nm InP-HBT	IF-mixer, LO driver, LO oscillator	298.1	-2.3	452	0.13
[7]	130nm SiGe	IQ-mixer, LO multiplier ( $\times 16$ ), PA	240	-4.4	1,033	0.04
[8]	130nm SiGe	Mixer, LO driver, antenna	190	-6	32 <sup>1</sup>	0.78
[9]	40nm CMOS	IQ-mixer, LO multiplier ( $\times 3$ )	265.68	-1.6	890	0.08
[10]	130nm SiGe	IQ-mixer, LO multiplier ( $\times 16$ ), PA	220-255	5	960	0.33
[11]	130nm SiGe	IQ-mixer, LO multiplier ( $\times 16$ ), PA	225-255	7.5	960 <sup>2</sup>	0.59
[12]	130nm SiGe	IQ-mixer, LO multiplier ( $\times 8$ ), PA	240	12 <sup>4</sup>	1,237	1.28
[13]	80nm InP-HEMT	IF-mixer, LO driver, PA <sup>3</sup>	290	12	6,600	0.24
This work	250nm InP-HBT	IQ-mixer, LO multiplier ( $\times 8$ ), phase shifter, PA	195	16.5	1,250	3.57
			200	15.3	1,250	2.71

<sup>1</sup> $P_{\text{DC}}$  not including LO generator at 190 GHz    <sup>2</sup> $P_{\text{DC}}$  for 1-channel I-Q TX+LO    <sup>3</sup>Individually packaged, not integrated    <sup>4</sup>Measured from PA breakout