

# High linearity GaN HEMT power amplifier with pre-linearization gate diode

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A high linearity MMIC RF power amplifier is reported in the AlGaIn/GaN HEMT technology. In order to obtain high linearity, a pre-linearization gate diode is added at the input to compensate the non-linear effect caused by the nonlinear input capacitance  $C_{gs}$  of the GaN HEMT device. Another single-ended Class B power amplifier without the gate diode is also designed for comparison. The circuit with the pre-linearization gate diode demonstrates at least 4dB improvement on IMD3 performance over the one without the diode up to its P1dB output power level in two-tone measurement.

## 1. Introduction.

According to our previous single-ended Class B power amplifier design in GaN HEMT, it has been proved that high linearity and high efficiency can be obtained simultaneously if the circuit is biased at the exactly the pinch off point (Class B configuration) [1].

In order to further improve the linearity performance, linearization techniques, for example feedback, feed forward, or predistortion, have to be used. Feedback is good for audio power amplifiers, but for RF power amplifiers the stability and efficiency become concerned. System level feed forward or predistortion can be useful for RF frequencies, but the overall efficiency will be decreased because extra components have to be added, which will also make it difficult for MMIC implementation.

Here in this work, three major sources of AlGaIn/GaN HEMT device nonlinearity are investigated: nonlinear I-V characteristic (transfer function), nonlinear  $G_{ds}$  and nonlinear  $C_{gs}$ . All the above nonlinear sources in the device will create the 3<sup>rd</sup> order intermodulation distortion (IMD3) either at the output or at the input of the circuit.

## 2. Nonlinear sources of GaN HEMT device.

It is obvious that the nonlinear I-V characteristic of the device will generate IMD3, which directly affect the linearity performance. It is the dominant nonlinear source when the input power is very high. But with moderate input power level, as we discussed in [2], best linearity performance can be obtained by biasing at Class B.

For GaN HEMT devices, the output conductance  $G_{ds}$  is a nonlinear function of the input and output signal. Moreover, substantial drain voltage dependent leakage current is observed in 0.3 $\mu$ m single gate devices, which is similar to the Drain-Induced Barrier Lowering (DIBL) effect in MOSFET. This results in a threshold voltage shift, which also creates 3<sup>rd</sup> IMD3. However, by using dual-gate device, the nonlinear  $G_{ds}$  effect can be minimized.

Finally, the input capacitance  $C_{gs}$  vs.  $V_{gs}$  characteristic of the AlGaIn/GaN HEMT device is not linear, and it can be proved that the nonlinear  $C_{gs}$  characteristic can generate intermodulation distortion at the input of the circuit. The distortion is amplified, also affecting the linearity of the circuit. The effect due to nonlinear  $C_{gs}$  can be minimized by adding a pre-linearization gate diode.

### 3. Pre-linearization gate diode

The nonlinear  $C_{gs}$  vs.  $V_{gs}$  characteristic can be modeled as a hyperbolic tangent function, which is an anti-symmetric function around the center point,  $V_c$  (shown in figure 1). Therefore, the idea of further improving linearity due to nonlinear  $C_{gs}$  is to compensate it with another nonlinear capacitance, which behaves exactly the opposite about  $V_c$ . Thus the total input capacitance of the circuit will be constant, no matter where we bias the circuit (as shown in figure 2). This idea can be easily implemented by adding another HEMT device at the input, whose source and drain are shorted, and the gate is biased at twice of the  $V_c$  (shown in figure 3).

### 4. Circuit design and simulation result.

The dual gate Class B power amplifier with the prelinearization gate diode is designed at 10GHz and simulated using Agilent ADS. The circuit schematic and IC layout are shown in Figure 3 and 4. Both the input and output matching networks are on chip. In the output matching network, the output capacitance of the device  $C_{out}$  is absorbed into the  $\Pi$  low pass filter. A big on-chip capacitor  $C_0$  is needed as close to the second gate as possible to provide a good AC ground. The prelinearization gate diode is beside the main device, both of which have the same gate area. Another single-ended Class B power amplifier without the gate diode is also designed for comparison. According to simulation using a model which only includes nonlinear  $C_{gs}$ , the IMD3 performance can be improved by about 4dB with the pre-linearization gate diode at all power levels (shown in Figure 5).

### 5. Measurement results.

All the MMIC Class B power amplifiers are fabricated on a SiC substrate in the standard AlGaIn/GaN HEMT technology and then tested. The 1.2mm dual gate GaN HEMT gives 1A/mm of  $I_{dss}$  and around 55V of break down voltage. The measured  $f_t$  for the 0.3 $\mu$ m  $L_g$  dual gate device is 50GHz [2].

The single tone and two tones measurement results of the two circuits are shown in figure 6, 7 and 8. For single tone measurement, the circuit without the gate diode demonstrates 30dBm output power at 1dB gain compression point ( $P_{1dB}$ ) with 9.5dB gain from 9GHz to 10GHz, while the circuit with the gate diode demonstrates 29.1dBm of  $P_{1dB}$  output power with 8.4 dB gain at 10GHz. For two-tone measurement around 10GHz, a peak of 51dBc IMD3 is obtained with the gate diode at around 21dBm per tone. A 4dB improvement in IMD3 is obtained for the whole power range up to this point.

### 6. Conclusions.

A high linearity MMIC RF power amplifier is reported in the AlGaIn/GaN HEMT technology. Three major nonlinear sources of the GaN HEMT device are identified and investigated. To obtain high linearity, a pre-linearization gate diode is added at the input to compensate the nonlinear effect of  $C_{gs}$ . The circuit with the pre-linearization gate diode demonstrates at least 4dB improvement on IMD3 performance over the useful power range in two-tone measurement.

### 7. Acknowledgement.

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## 8. References

[1] Shouxuan Xie, *et al.*, “High linearity of Class B Power Amplifiers in GaN HEMT technology.” *Microwave and Wireless Components Letters*, July 2003

[2] Vamsi Paidi, *et al.*, “High Linearity and High Efficiency of Class B Power Amplifiers in GaN HEMT Technology.” *IEEE Transactions on Microwave Theory and Techniques*, Vol. 51, No. 2, Feb. 2003

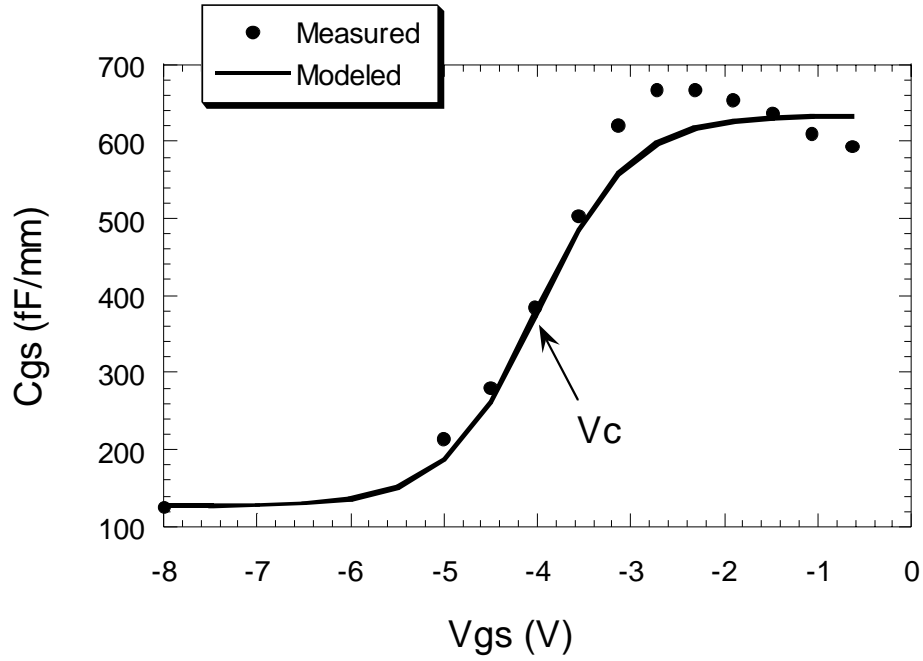


Figure 1: Nonlinear Cgs vs. Vgs characteristic of AlGaIn/GaN HEMT

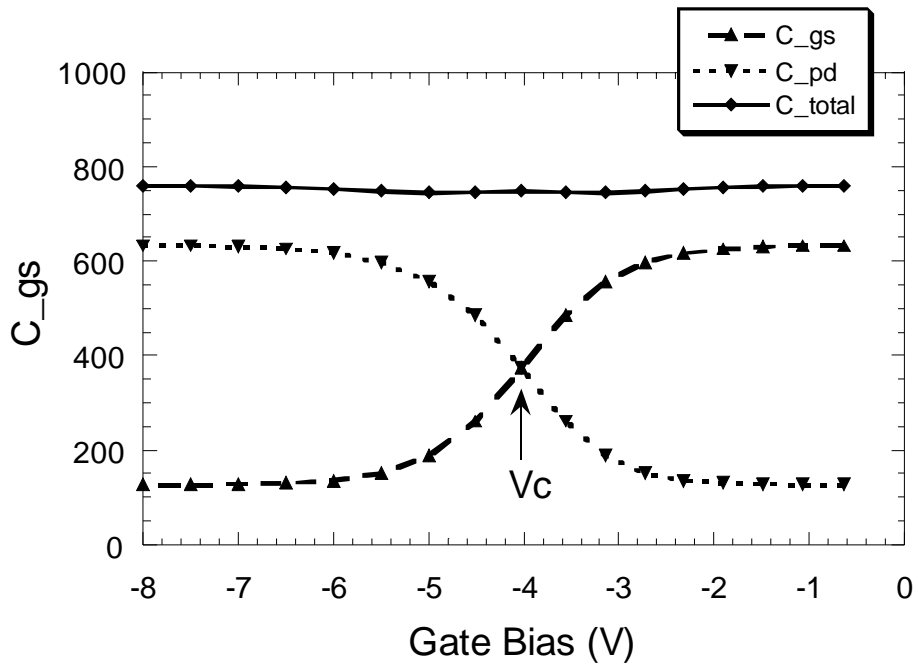


Figure 2: Pre-linearization gate diode to further improve linearity due to nonlinear Cgs

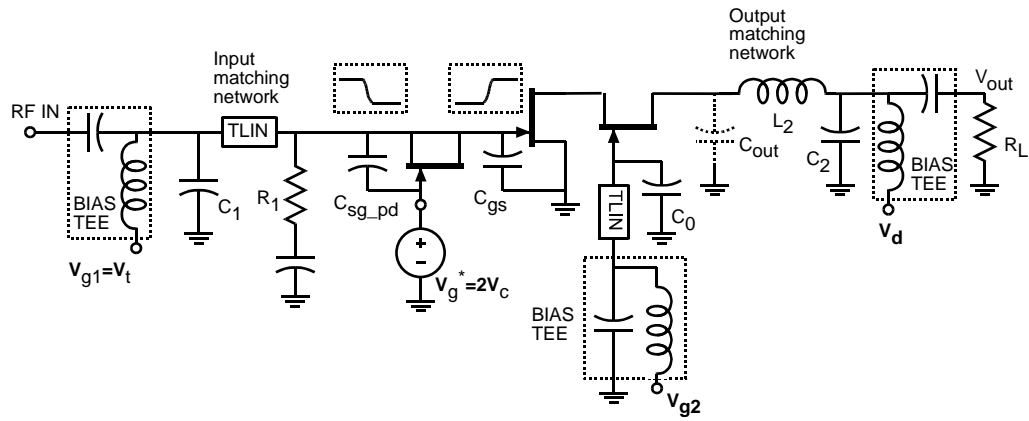


Figure 3: Circuit schematic of the dual-gate Class B power amplifier with the pre-linearization diode

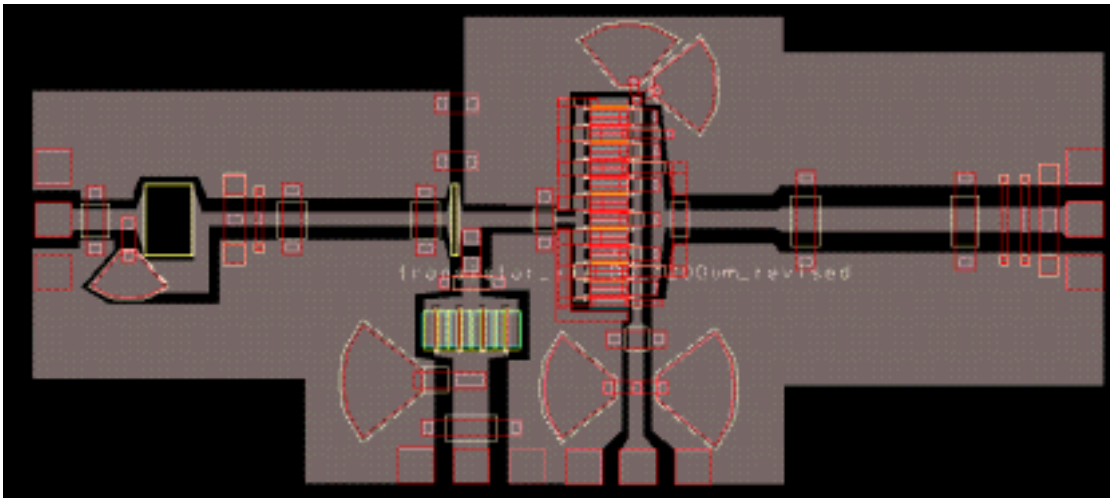


Figure 4: IC layout (dimensions 3mm x 1.5mm)

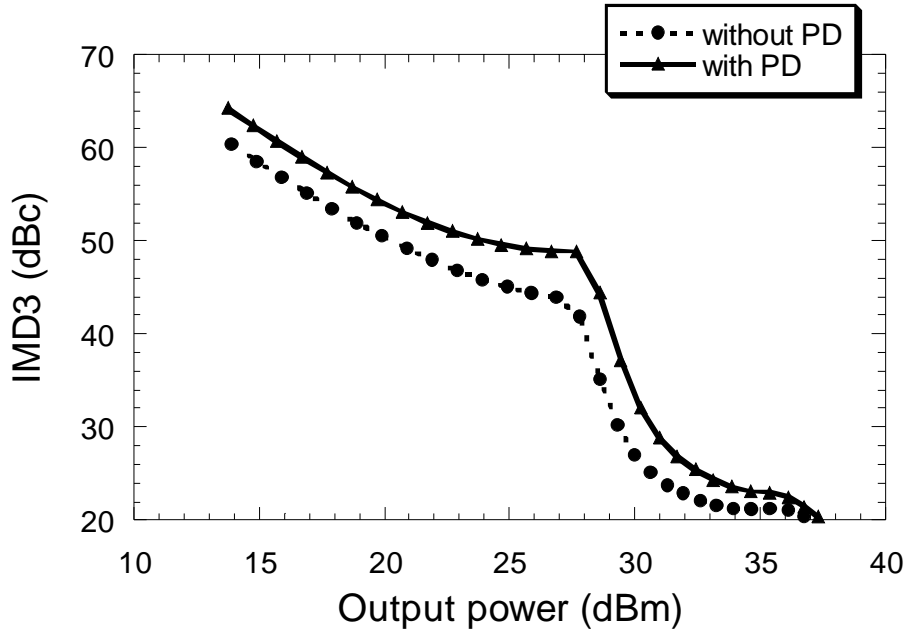


Figure 5: Simulation result on IMD3 improvement with the pre-linearization diode

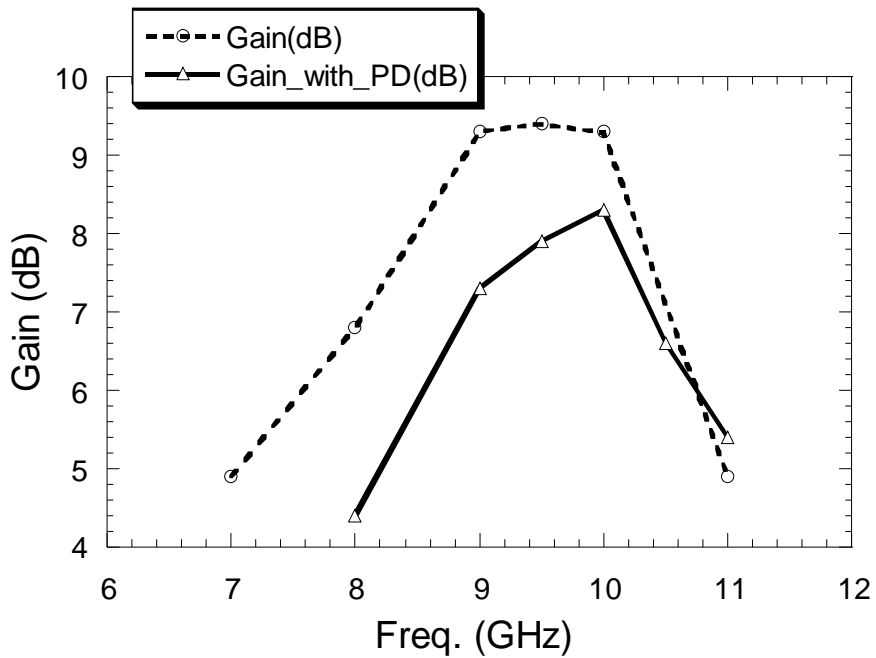


Figure 6: Measurement result: Gain vs. Freq.

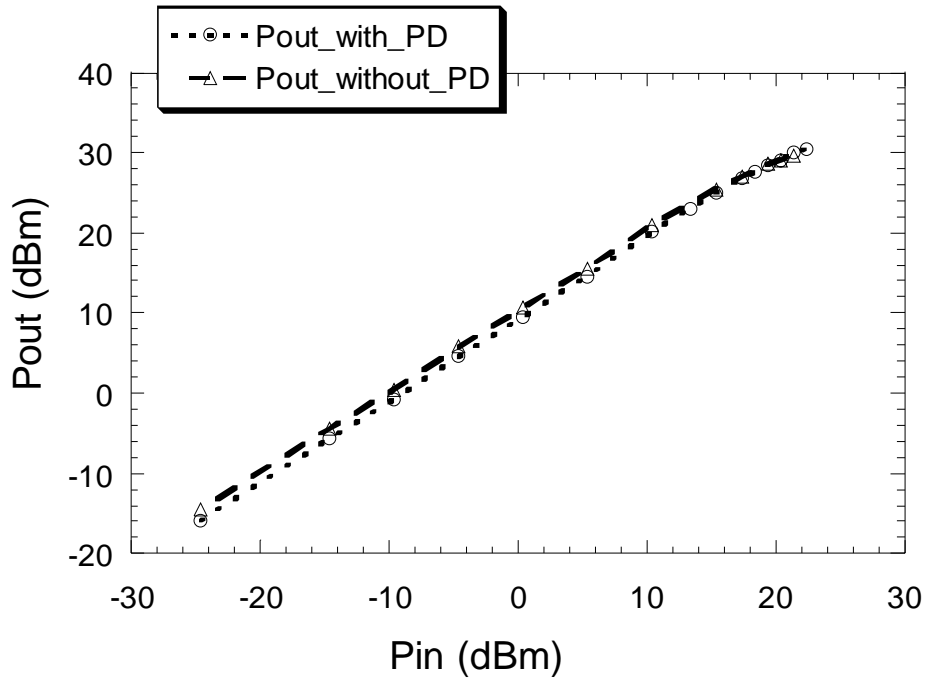


Figure 7: Single tone measurement result Pout vs. Pin

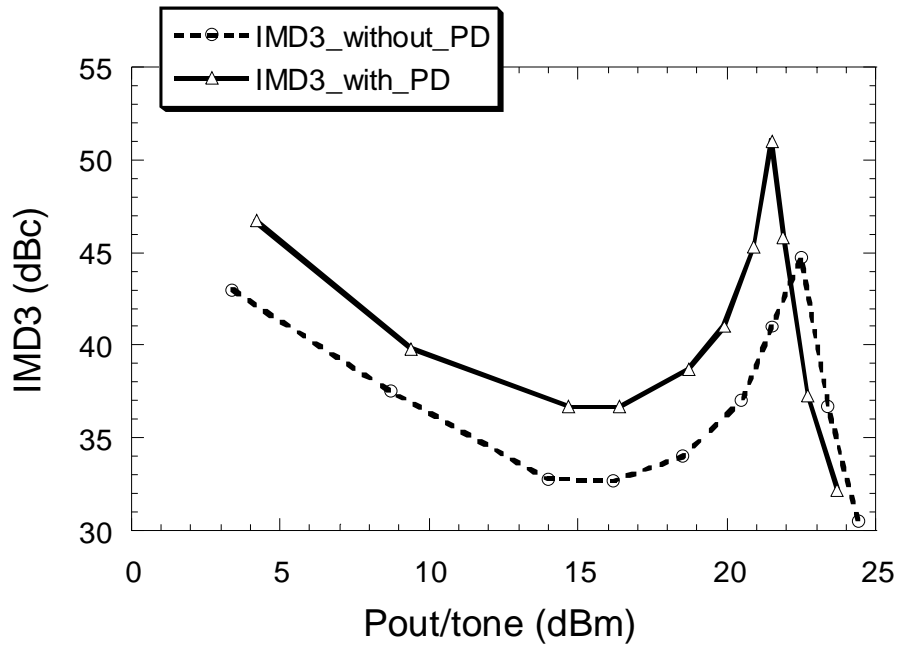


Figure 8: Two-tone measurement result IMD3 vs. Pout