

A hybrid silicon evanescent electroabsorption modulator

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Abstract: A new way to make high speed modulators using Si waveguides is demonstrated. The hybrid silicon evanescent electroabsorption modulator with offset AlGaInAs quantum wells has an extinction ratio over 10dB and modulation bandwidth over 16GHz.

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1. Introduction

Silicon-based modulators have attracted much attention with devices reported using the free carrier plasma dispersion in Mach-Zehnder interferometric form [1,2] or with resonator structure [3,4] to increase the interaction of light with the active material. Strained silicon also exhibits linear electro-optic refractive index modulation [5]. Recently electroabsorption modulator on silicon had been demonstrated based on the Franz-Keldysh effect in strained SiGe [6]. Here we present our approach of integration of modulators into silicon using wafer bonded hybrid silicon evanescent platform. The modulator described here can be integrated with lasers [7], amplifiers, and photodetectors [8] using quantum well intermixing [9]. High performance integrated high speed transmitters should be possible.

2. Device structure and fabrication

The silicon evanescent electroabsorption modulator (EAM) is a hybrid structure that consists of an offset multiple quantum well (MQW) region bonded to a silicon waveguide fabricated on a silicon-on-insulator (SOI) wafer as shown in Fig. 1. The III-V epitaxial structure is grown on an InP substrate. The structure is summarized in Table 1. InGaAlAs is chosen as the MQW material because it has larger ΔE_c , which provides a stronger carrier confinement and produce strong quantum confined stark effect (QCSE) with higher extinction ratio [10,11]. The MQW section contains 10 wells and 11 barriers with photoluminance (PL) at 1478nm. The silicon waveguide was fabricated with a height of 0.5 μm and slab thickness of 0.3 μm . The silicon waveguide has a width of 1.5 μm for passive segments, and width of 0.8 μm under III-V mesa for higher optical confinement. The width of the III-V mesa for the absorber is 4 μm at the top InP cladding layer and 2 μm at the SCH and MQW layers to reduce the capacitance of the device [11,12]. Figure 1b shows the transition between the passive silicon waveguide and the hybrid waveguide of the EAM. The width of the III-V mesa is tapered from 0 to 2 μm over a length of 60 μm to increase the coupling efficiency and to minimize reflection. The center of the absorption region is kept with width of 4 μm to avoid laterally affect the optical mode and reduce the voltage drop at InP cladding. The contact electrode pads are designed to be 100 μm apart from center to center to use a standard GSG RF probe for high speed testing. The hybrid device has a total length around 400 μm with 100 μm absorber and two 60 μm long tapers.

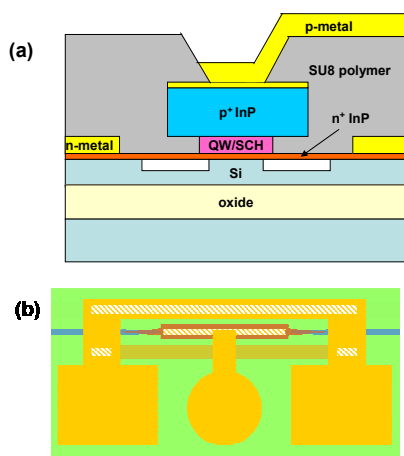


Fig. 1. Schematic diagrams of (a) device cross section and (b) hybrid waveguide and metal contacts.

| | Layer | Material and Composition | Doping | Thickness |
|---|--|---|----------|--------------------|
| 1 | P Contact | $\text{In}_{0.53}\text{Ga}_{0.47}\text{As}$ | P – 1e19 | 0.1 μm |
| 2 | Cladding | InP | P – 1e18 | 1.5 μm |
| 3 | SCH | $\text{In}_{0.520}\text{Al}_{0.160}\text{Ga}_{0.320}\text{As}$, -0.06%, 1.30 μm | P – 1e17 | 0.15 μm |
| 4 | MQW ($\lambda_{\text{PL}} \sim 1.48 \mu\text{m}$) | $\text{In}_{0.590}\text{Al}_{0.080}\text{Ga}_{0.330}\text{As}$, +0.41%, 1.55 μm (10x) | n. i. d. | 11 nm |
| | | $\text{In}_{0.470}\text{Al}_{0.200}\text{Ga}_{0.330}\text{As}$, -0.40%, 1.19 μm (11x) | n. i. d. | 7 nm |
| 5 | SCH | $\text{In}_{0.520}\text{Al}_{0.160}\text{Ga}_{0.320}\text{As}$, -0.06%, 1.30 μm | n. i. d. | 0.1 μm |
| 6 | N Contact | InP | N – 3e18 | 0.11 μm |
| 7 | Super lattice | $\text{In}_{0.85}\text{Ga}_{0.15}\text{As}_{0.327}\text{P}_{0.673}$ (2x) | N – 3e18 | 7.5 nm |
| | | InP (2x) | N – 3e18 | 7.5 nm |
| 8 | Bonding layer | InP | N – 3e18 | 10 nm |

Table 1. III-V epitaxial layer structure.

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The III-V epitaxial layers are transferred to the patterned SOI wafer through low temperature oxygen plasma assisted wafer bonding at a 300 °C annealing temperature under vacuum. The InP substrate is removed using a mixture of HCl/H₂O. The details of silicon waveguide fabrication and wafer bonding process are described in Ref. 7. The III-V back end processing starts with blanket deposition of Pd/Ti/Pd/Au p-contacts. The p metal serves as a hard mask for the self aligned process to form the III-V mesa [8]. The undercut profile is created by wet etch SCH and MQW layers. Ni/Au/Ge/Ni/Au alloy are deposited onto the exposed n-type InP layer to form ohmic contacts. The n-InP layer is selectively removed by RIE dry etch to expose the silicon input and output waveguides. A 4µm thick SU-8 polymer layer is used to minimize the parasitic capacitance between the p-probe pad and the n-type InP layer and to provide additional mechanical support to the thin n-InP layer over the silicon waveguide air gap. 2 µm Ti/Au probe pads are deposited and connected to contact metals for final electrical contact.

3. Device characteristics

Figure 2 shows the relative extinction at wavelength of 1550nm under various reverse biases. More than 10dB extinction can be achieved with 5V bias. The device has a series resistance around 30Ω and capacitance of 0.1pF measured from impedance test, which will results a cut-off frequency around 20GHz. It matches with the measured small signal modulation response as shown in Fig. 3.

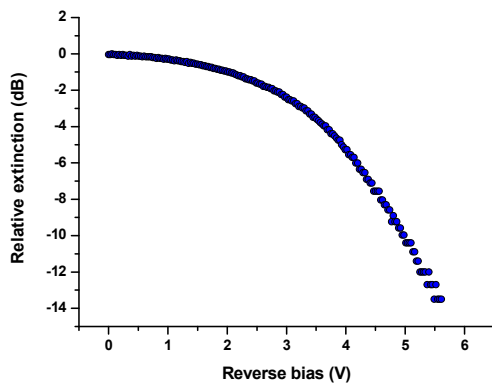


Fig. 2. Relative optical extinction at different DC bias.

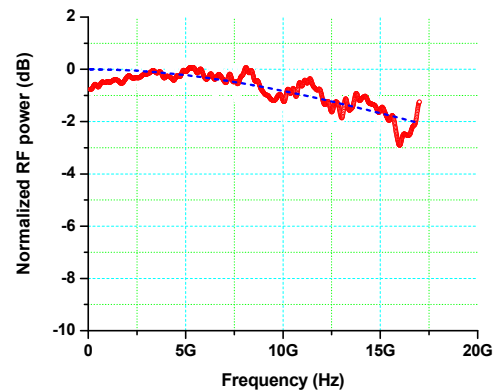


Fig. 3. Small signal response. Dashed line: calculated response using RC model.

To investigate the performance of large signal modulation, we drive our modulator with a $2^{31}-1$ pseudorandom bit sequence (PRBS). The device is biased at -3V with peak to peak drive voltage of 3.2V. The modulated light is collected with lensed fiber and amplified with EDFA. A 100GHz filter is used to reduce the ASE noise before the signal is detected by a 30GHz photodetector and sampled using an Agilent digital communication analyzer (DCA). Figure 4a shows eye diagrams measured at non-return-to-zero (NRZ) 10 Gb/s. The 10 Gb/s signal has an extinction ratio of 6.3 dB, which is slightly lower than the DC extinction due to microwave voltage drop at cladding and ohmic contacts. The eye is clearly open with quality factor (Q factor) close to 12. The rise and fall time of the signal is about 27ps, which is as expected faster than the driving signal as shown in Fig. 4b.

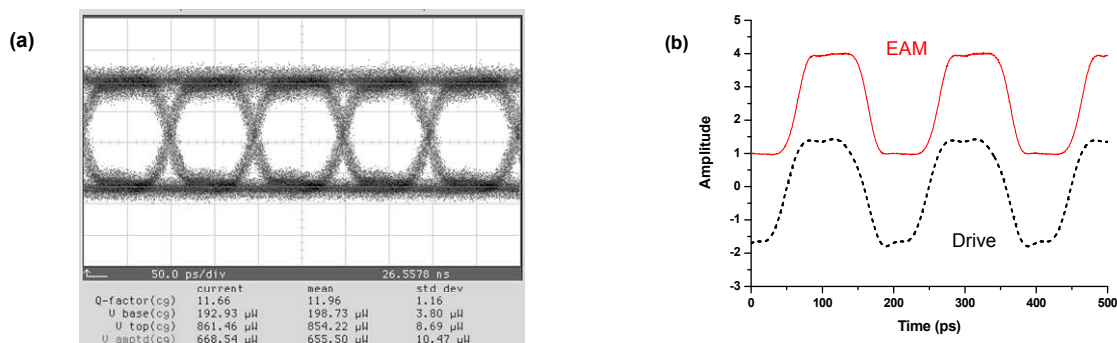


Fig. 4. (a) Measured 10G NRZ eye diagrams; (b) pulse train of drive signal and modulated signal. The drive signal has rise/fall time around 35ps. The modulated signal shows better rising/falling edge about 27ps.

4. Conclusion

We have demonstrated the first hybrid silicon evanescent electroabsorption modulator with offset AlGaInAs quantum well. The fabricated device has DC extinction ratio over 10dB at 5V bias. The small signal modulation bandwidth is over 16G Hz. We presented a clear eye opening at 10Gb/s with peak to peak drive voltage of 3.2V. The current device is RC limited to 20Ghz bandwidth. By employing travel wave electrode with longer absorber, we can further improve the bandwidth and extinction ratio. The approach developed here is not limited by the relatively weak, relatively slow response of carrier injection Si modulators.

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