Switched Systems:
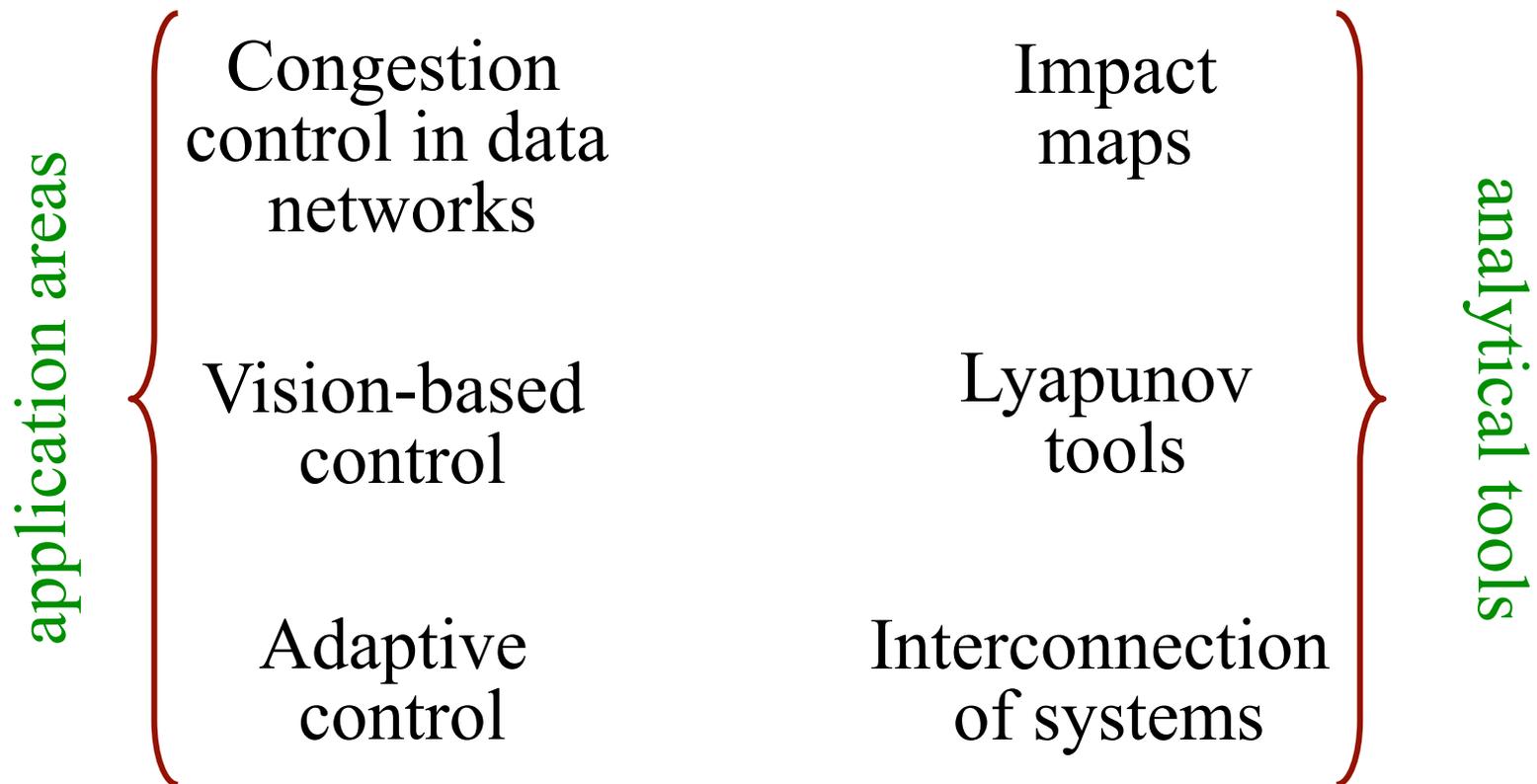# Mixing Logic with
Differential Equations

João P. Hespanha
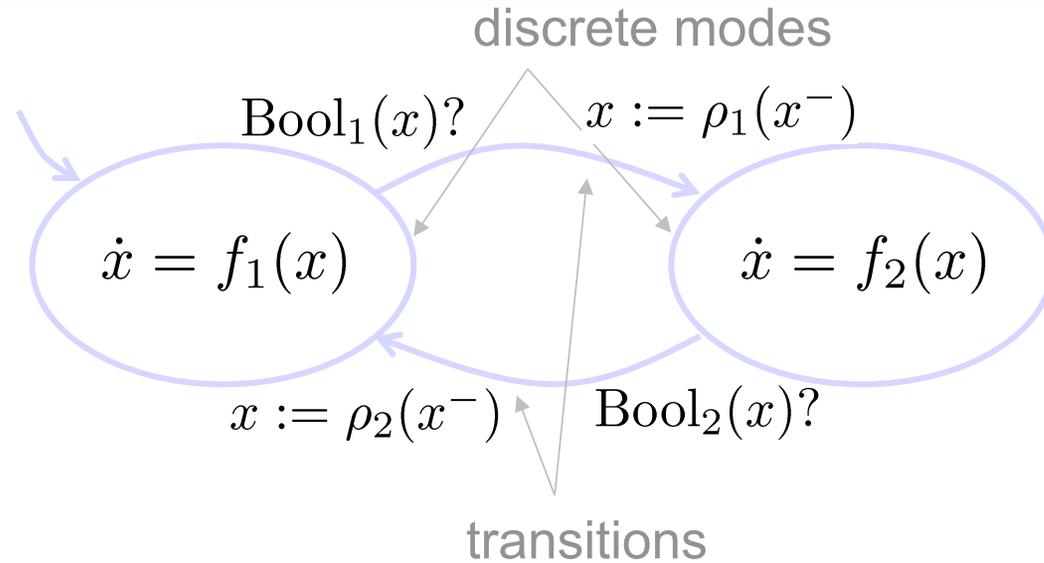
Center for Control
Dynamical Systems and Computation

UC SANTA BARBARA
engineering

CCDC
Center for Control, Dynamical Systems and Computation

Logic-based switched systems framework

application areas

Congestion
control in data
networks

Vision-based
control

Adaptive
control

Impact
maps

Lyapunov
tools

Interconnection
of systems

analytical tools

discrete modes

$$\text{Bool}_1(x)? \qquad x := \rho_1(x^-)$$

hybrid automaton representation

$$\dot{x} = f_1(x) \qquad\qquad \dot{x} = f_2(x)$$

$$x := \rho_2(x^-) \qquad \text{Bool}_2(x)?$$

transitions

hybrid automaton representation

$$\text{Bool}_1(x)? \qquad x := \rho_1(x^-)$$

$$\dot{x} = f_1(x) \qquad \dot{x} = f_2(x)$$

$$x := \rho_2(x^-) \qquad \text{Bool}_2(x)?$$

$$x := \rho_1(x^-) \qquad x := \rho_2(x^-) \qquad x := \rho_1(x^-)$$
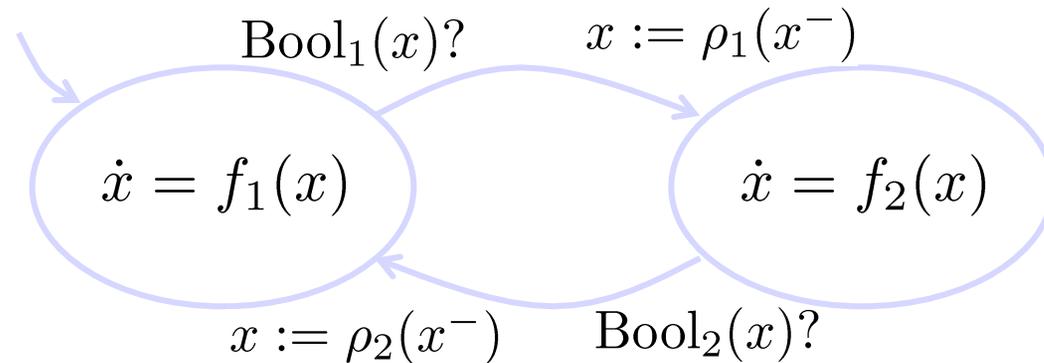
$$\dot{x} = f_1(x) \qquad \dot{x} = f_2(x) \qquad \dot{x} = f_1(x) \qquad \dot{x} = f_2(x)$$

hybrid automaton representation

$$\text{Bool}_1(x)? \qquad x := \rho_1(x^-)$$

$$\dot{x} = f_1(x) \qquad \dot{x} = f_2(x)$$

$$x := \rho_2(x^-) \qquad \text{Bool}_2(x)?$$

switching times

$$\sigma(t) \equiv \text{switching signal}$$

2

1

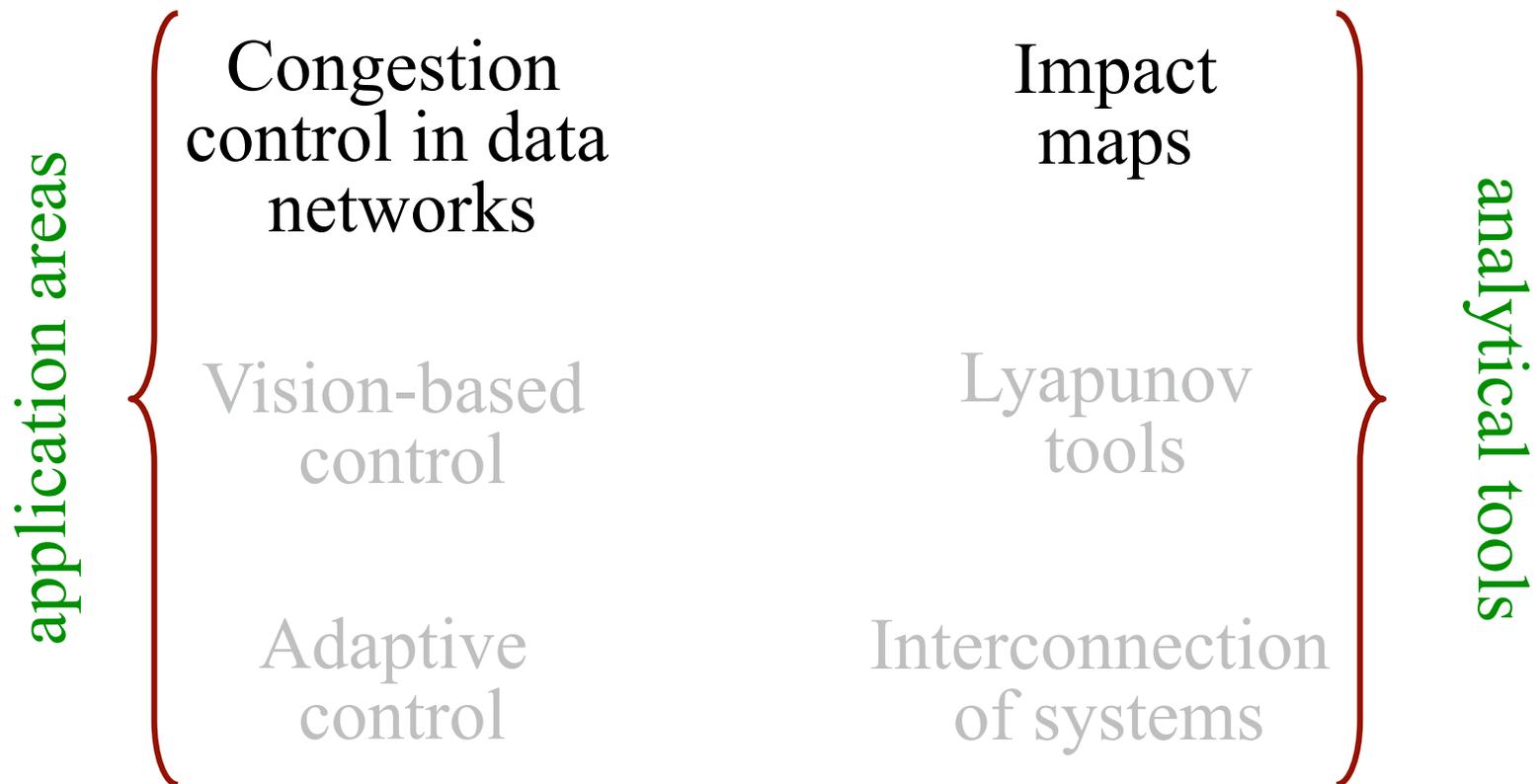$$\dot{x} = f_1(x) \qquad \dot{x} = f_2(x) \qquad \dot{x} = f_1(x) \qquad \dot{x} = f_2(x)$$
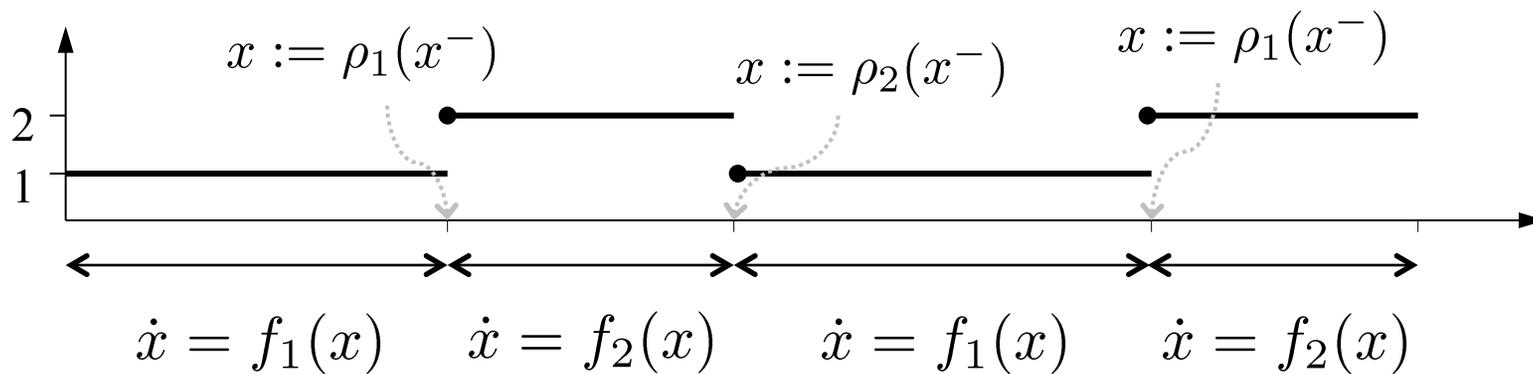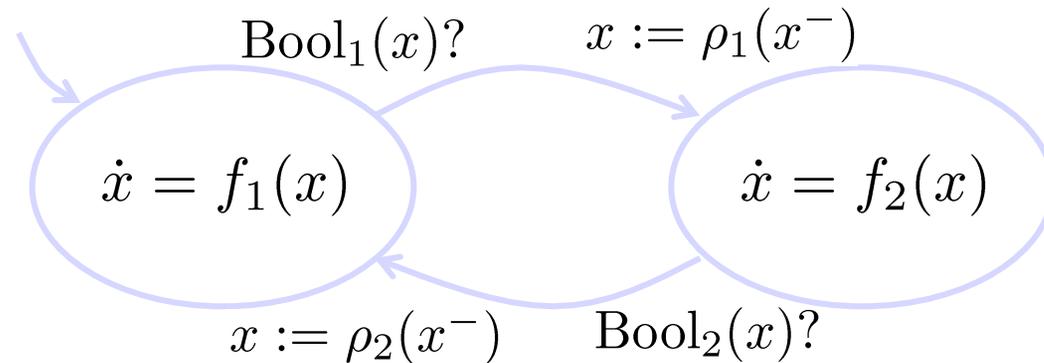
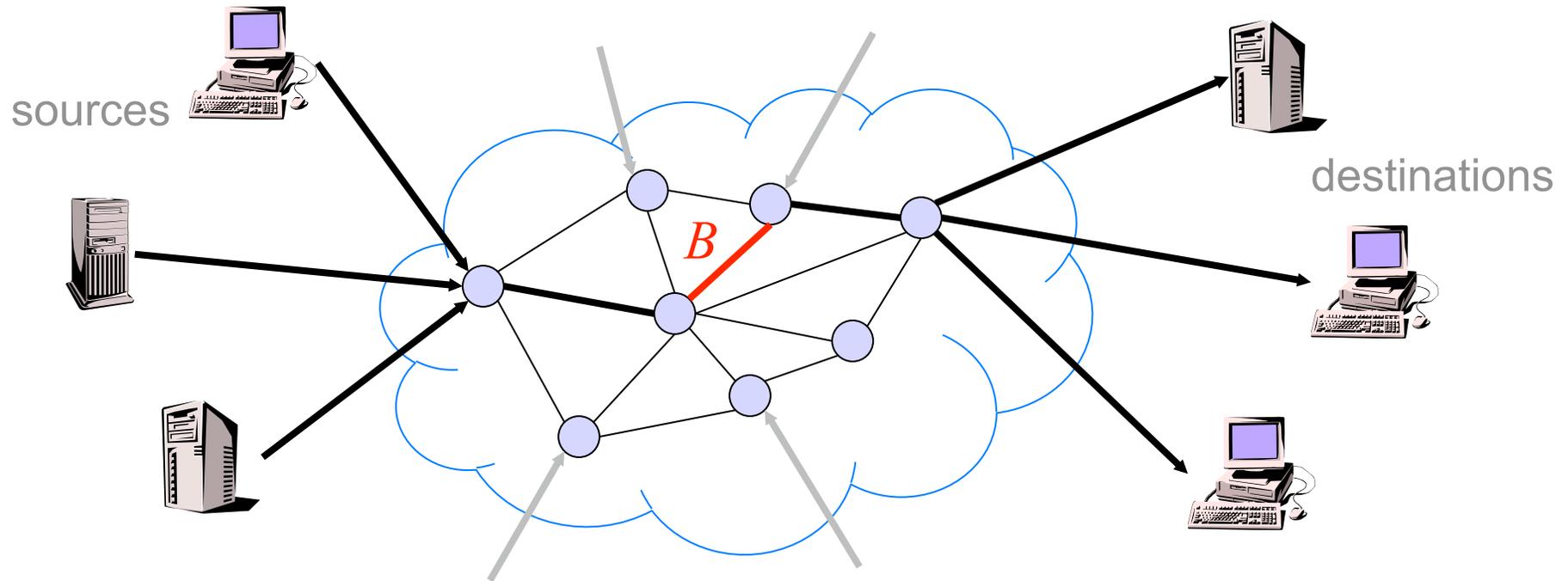**dynamical system representation**

$$\begin{cases} \dot{x} = f_\sigma(x) & \text{differential equation} \\ (\sigma, x) = \phi(\sigma^-, x^-) & \text{discrete transition} \end{cases}$$

$$\phi(s, z) = \begin{cases} (2, \rho_1(z)) & s = 1,\ \text{Bool}_1(z) \\ (1, \rho_2(z)) & s = 2,\ \text{Bool}_2(z) \\ s & \text{otherwise} \end{cases}$$

Logic-based switched systems framework

application areas

Congestion
control in data
networks

Vision-based
control

Adaptive
control

Impact
maps

Lyapunov
tools

Interconnection
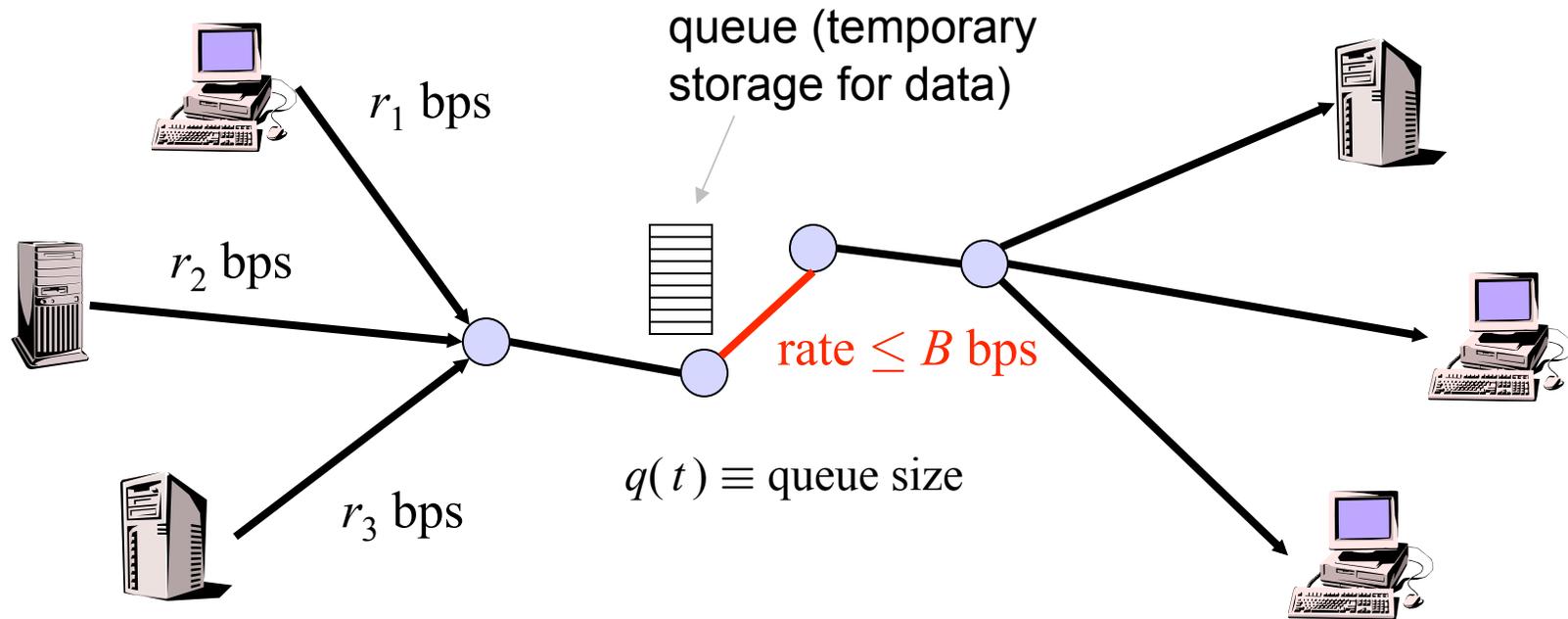of systems

analytical tools

sources

destinations

B

Congestion control problem:
How to adjust the sending rates of the data sources to make sure
that the bandwidth *B* of the bottleneck link is not exceeded?

B is unknown to the data sources and possibly time-varying

queue (temporary storage for data)

r_1 bps

r_2 bps

rate $\leq B$ bps

r_3 bps

$q(t) \equiv$ queue size

When $\sum_i r_i$ exceeds B the queue fills and data is lost (drops)

$$\dot{q} = \begin{cases} \sum_i r_i - B & 0 \leq q \leq q_{max} \\ 0 & \text{otherwise} \end{cases}$$

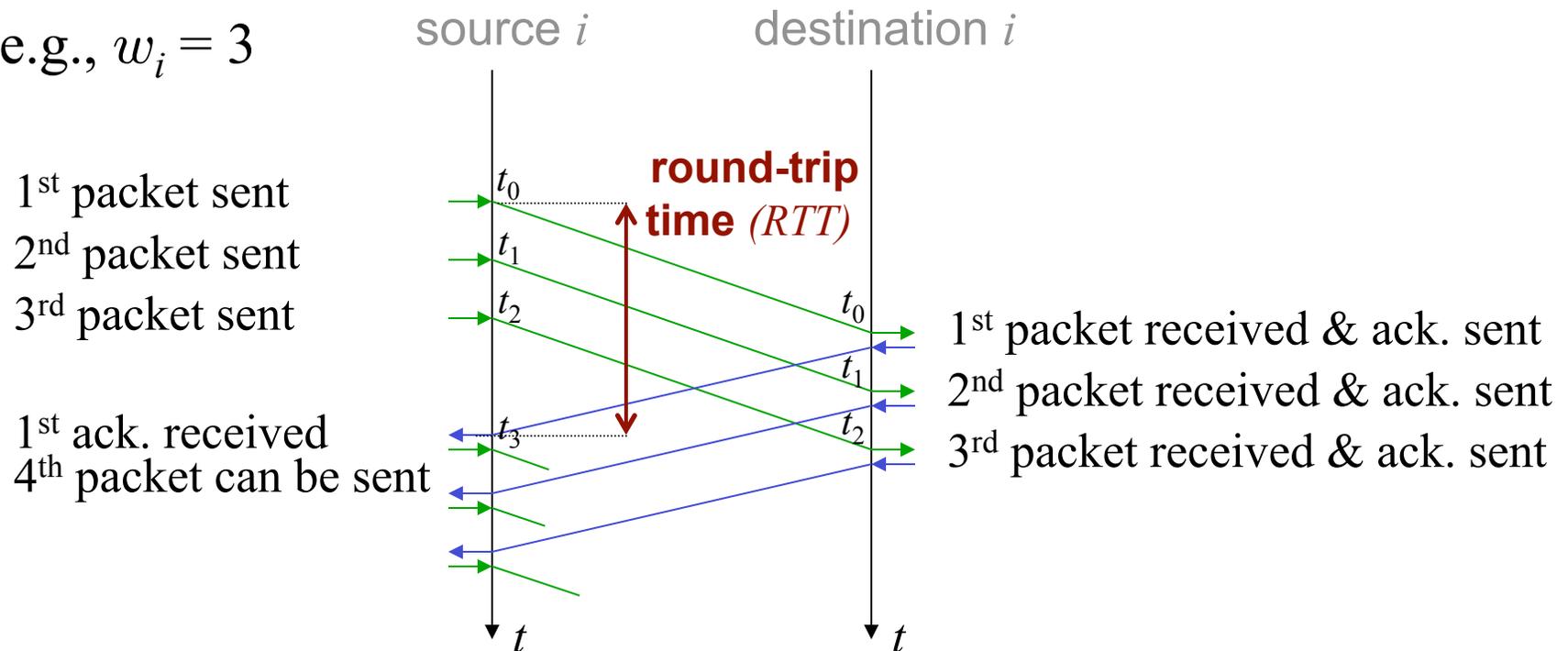$$q = q_{max}, \quad \sum_i r_i > B \quad \Rightarrow \quad \textbf{drop} \quad \text{(discrete event)}$$

Event-based control:
The sources adjust their rates based on the detection of drops

w_i (window size) $\equiv$ number of packets that can remain
unacknowledged for by the destination

e.g., $w_i = 3$

source i destination i

1st packet sent
2nd packet sent
3rd packet sent

round-trip
time (RTT)

t_0
t_1
t_2

t_0
t_1
t_2

1st packet received & ack. sent
2nd packet received & ack. sent
3rd packet received & ack. sent

1st ack. received
4th packet can be sent

t_3

t t

w_i effectively determines the sending rate r_i :

$$r_i(t) = \frac{w_i(t)}{RTT(t)}$$

$\longleftarrow$ round-trip time
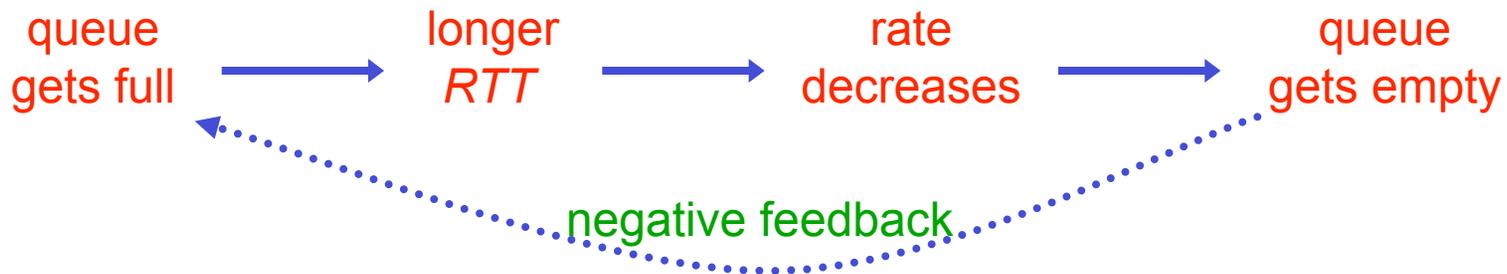
w_i (window size) $\equiv$ number of packets that can remain unacknowledged for by the destination

$$r_i(t) = \frac{w_i(t)}{RTT(t)} \equiv \text{sending rate}$$

per-packet transmission time

$$RTT(t) = T_{\mathrm{p}} + \frac{1}{B}q(t)$$

total round-trip time

propagation delay

time in queue until transmission

queue gets full → longer *RTT* → rate decreases → queue gets empty

negative feedback

This mechanism is still not sufficient to prevent a catastrophic collapse of the network if the sources set the w_i too large

1. While there are no drops, increase w_i by 1 on each *RTT*
2. When a drop occurs, divide w_i by 2

   (congestion controller constantly probes the network for more bandwidth)

Network/queue dynamics

Reno controllers

$$\dot{q} = \begin{cases} \sum_i r_i - B & 0 \leq q \leq q_{\max} \\ 0 & \text{otherwise} \end{cases}$$

$$RTT = T_p + \frac{q}{B}$$

$$\dot{w}_i = \frac{1}{RTT}$$

$$r_i = \frac{w_i}{RTT}$$

$$q = q_{\max}$$
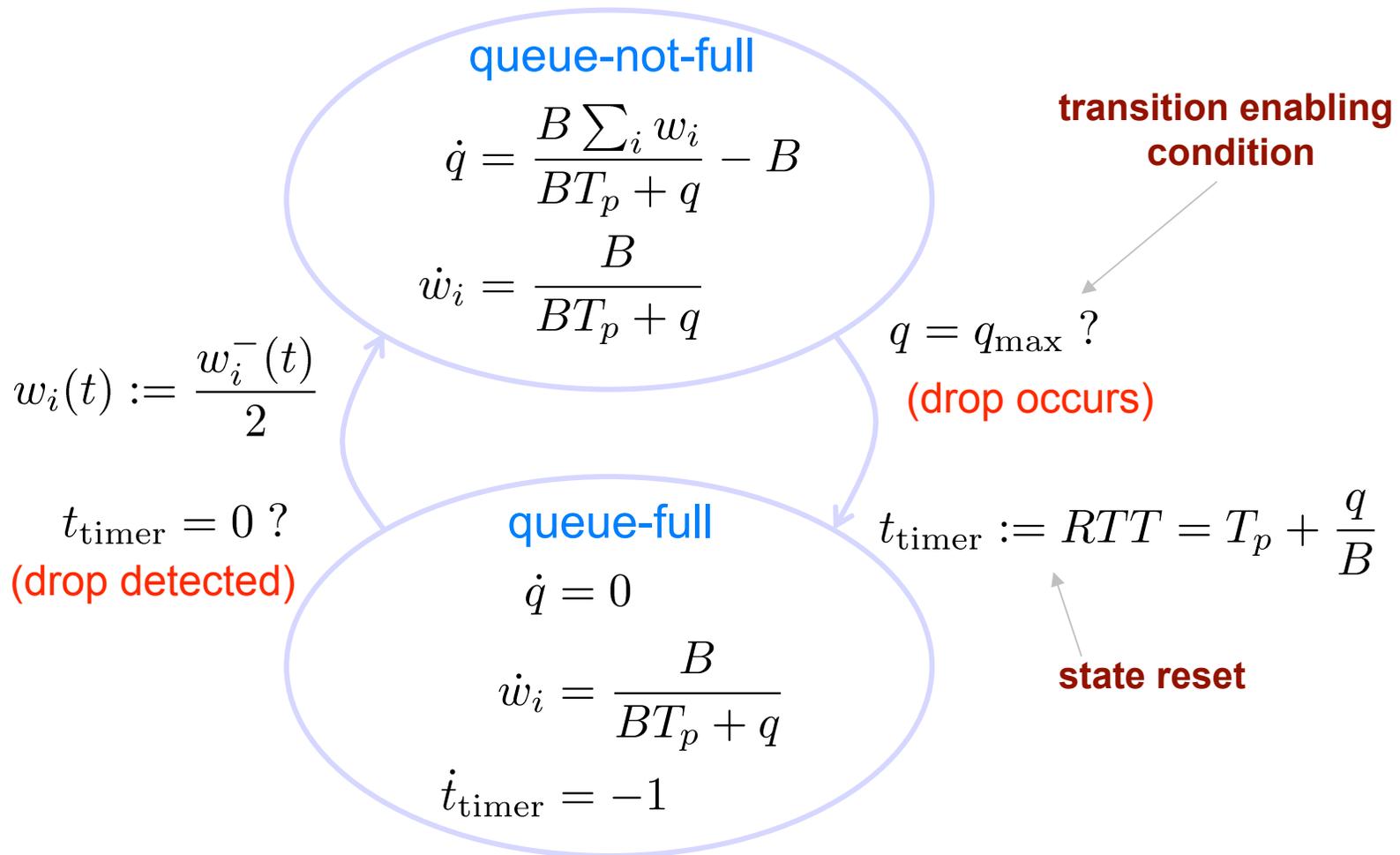
$\Downarrow$

drop occurs

drop detected
(one RTT after occurred)

$\Downarrow$
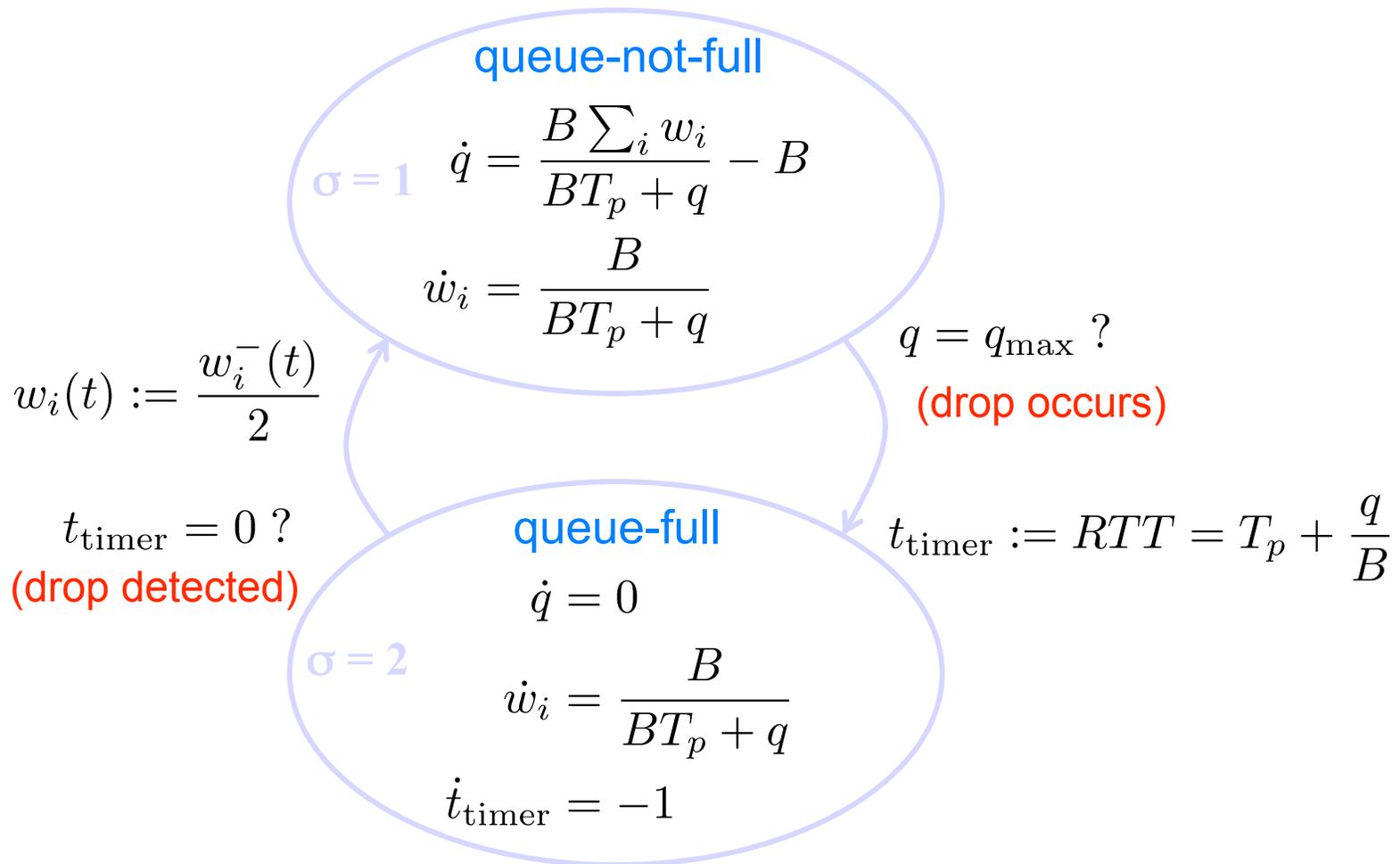
$$w_i \to \frac{w_i}{2}$$

disclaimer: this is a simplified version of Reno that ignores several interesting phenomena…

UC SANTA BARBARA
engineering

queue-not-full

$$\dot{q} = \frac{B \sum_i w_i}{BT_p + q} - B$$

$$\dot{w}_i = \frac{B}{BT_p + q}$$

transition enabling condition

$$q = q_{\max} \; ?$$

(drop occurs)

$$w_i(t) := \frac{w_i^-(t)}{2}$$

$$t_{\text{timer}} = 0 \; ?$$

(drop detected)

queue-full

$$\dot{q} = 0$$

$$\dot{w}_i = \frac{B}{BT_p + q}$$

$$\dot{t}_{\text{timer}} = -1$$

$$t_{\text{timer}} := RTT = T_p + \frac{q}{B}$$

state reset

queue-not-full

$\sigma = 1$

$$\dot{q} = \frac{B \sum_i w_i}{BT_p + q} - B$$

$$\dot{w}_i = \frac{B}{BT_p + q}$$

$$w_i(t) := \frac{w_i^-(t)}{2}$$

$q = q_{\max}$?

(drop occurs)

$t_{\text{timer}} = 0$?

(drop detected)

queue-full

$$\dot{q} = 0$$

$\sigma = 2$

$$\dot{w}_i = \frac{B}{BT_p + q}$$

$$\dot{t}_{\text{timer}} = -1$$

$$t_{\text{timer}} := RTT = T_p + \frac{q}{B}$$

alternatively…

$$x := \begin{bmatrix} q & w_1 & w_2 & \cdots & w_n & t_{\text{timer}} \end{bmatrix}'$$

$$\sigma \in \{1, 2\}$$

$$\begin{cases} \dot{x} = f_\sigma(x) & \text{continuous dynamics} \\ (\sigma, x) = \phi(\sigma^-, x^-) & \text{discrete dynamics} \end{cases}$$

$$x_1 \xrightarrow{\quad T \quad} x_2$$

$t_0 \qquad\qquad t_1 \quad t_2 \qquad\qquad t_3 \quad t_4 \qquad\qquad t_5 \qquad t_6$

queue-not-full $\quad$ queue full $\quad$ queue-not-full $\quad$ queue full $\quad$ queue-not-full $\quad$ queue full

$$\dot{x} = f_1(x) \qquad\qquad \dot{x} = f_1(x) \qquad\qquad \dot{x} = f_1(x)$$

$$\dot{x} = f_2(x) \qquad\qquad \dot{x} = f_2(x) \qquad\qquad \dot{x} = f_2(x)$$

$x_k := x(t_{2k}) \quad \equiv k^{\text{th}}$ time the system enters the queue-not-full mode

state space

$$x_{k+1} = T(x_k)$$

impact map

$$x_1 \xrightarrow{\qquad T \qquad} x_2$$

$t_0 \qquad\qquad t_1 \quad t_2 \qquad\qquad\qquad t_3 \quad t_4 \qquad\qquad\qquad t_5 \qquad t_6$

queue-not-full   queue full   queue-not-full   queue full   queue-not-full   queue full

$$\dot{x} = f_1(x) \qquad\qquad \dot{x} = f_1(x) \qquad\qquad \dot{x} = f_1(x)$$
$$\dot{x} = f_2(x) \qquad\qquad \dot{x} = f_2(x) \qquad\qquad \dot{x} = f_2(x)$$

$x_k := x(t_{2k}) \quad \equiv k^{\text{th}}$ time the system enters the queue-not-full mode

Theorem [1]**:** The function T is a contraction. In particular,
$$\|T(a) - T(b)\|_* \le \tfrac{1}{2}\|a - b\|_*, \quad \forall a, b$$
Therefore
- $x_k \to x_\infty$ as $k \to \infty$ $x_\infty \equiv$ constant
- $x(t) \to x_\infty(t)$ as $t \to \infty$ $x_\infty(t) \equiv$ periodic limit cycle

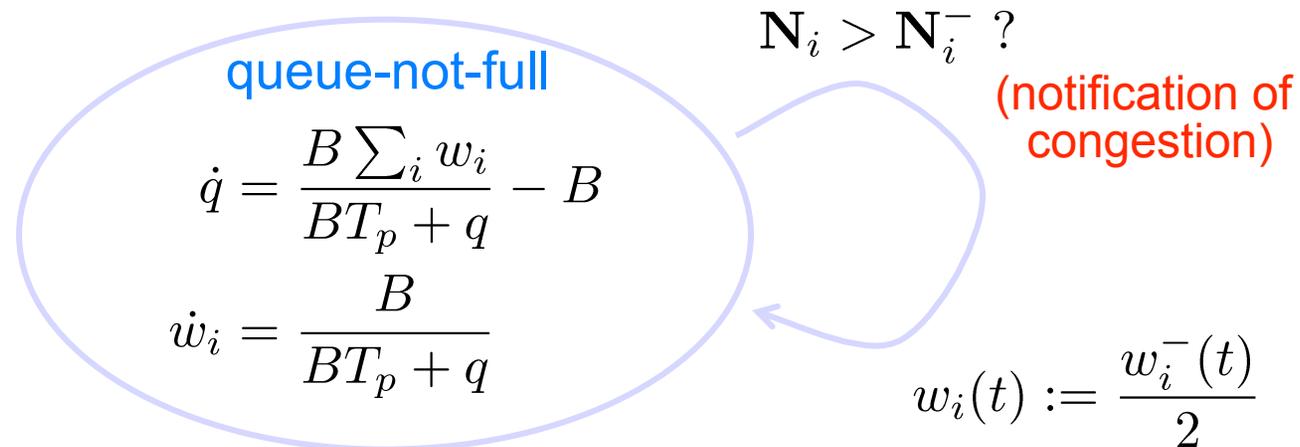[J. Grizzle et al. has applied similar tools to the design of walking robots]

NS-2 simulation results

UC SANTA BARBARA
engineering
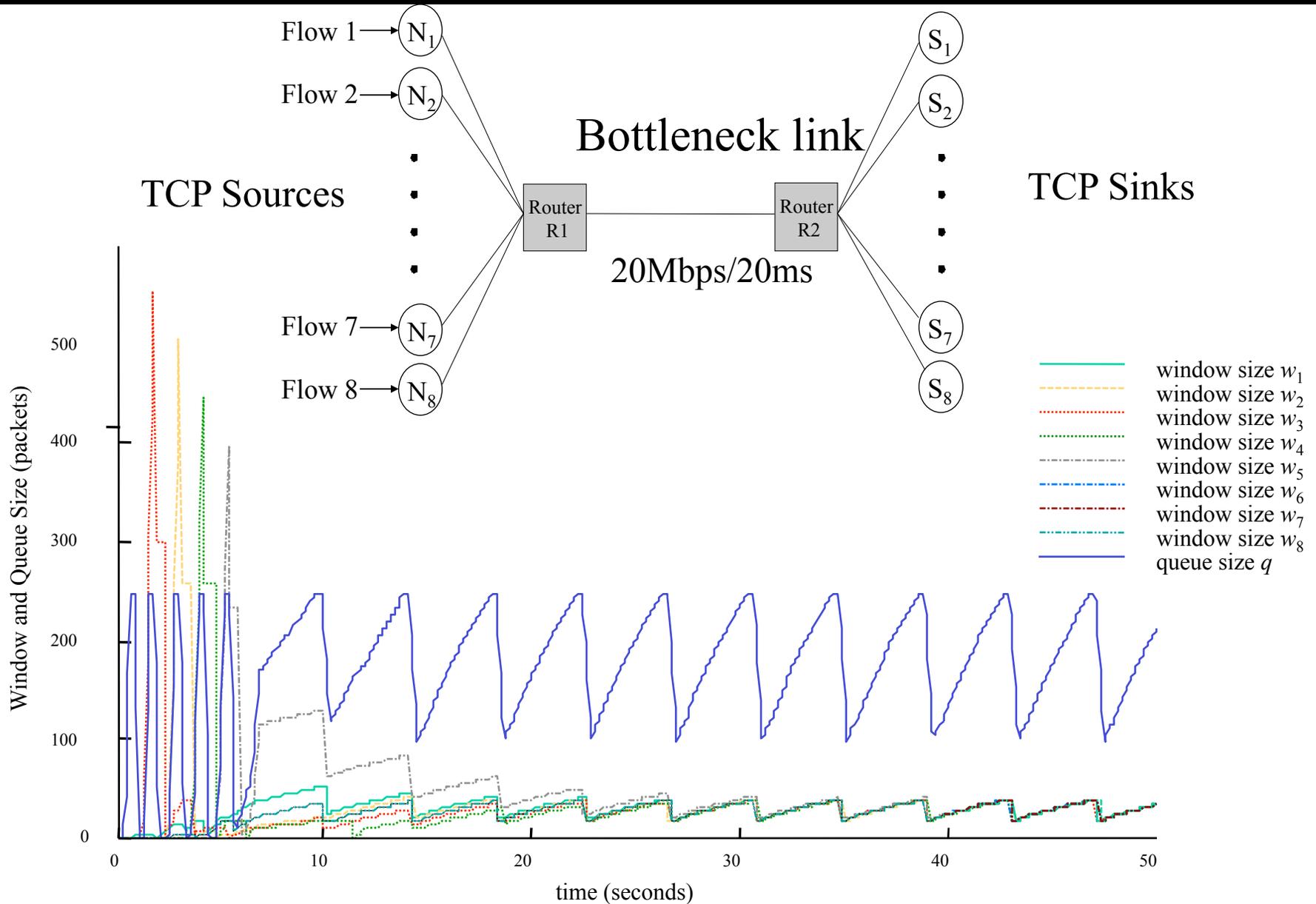
*Performance could be improved if the congestion controllers were notified of congestion **before** a drop occured*

queue-not-full

$\mathbf{N}_i > \mathbf{N}_i^- \ ?$

(notification of congestion)

$$\dot{q} = \frac{B \sum_i w_i}{B T_p + q} - B$$

$$\dot{w}_i = \frac{B}{B T_p + q}$$

$$w_i(t) := \frac{w_i^-(t)}{2}$$

$\mathbf{N}_i \equiv$ notification counter (incremented whenever a notification of congestion arrives)

In RED, $\mathbf{N}$ is a *random variable* with

function to be adjusted

$$\lim_{dt \downarrow 0} \frac{\mathrm{P}\left(\mathbf{N}_i(t) - \mathbf{N}_i(t - dt) = n\right)}{dt} = \begin{cases} \dfrac{w_i}{RTT} \gamma(q) & n = 1 \\ 0 & n > 1 \end{cases}$$

Stochastic switched system (leading to a stochastic impact map)

$$x_{k+1} = T(x_k)$$

impact map
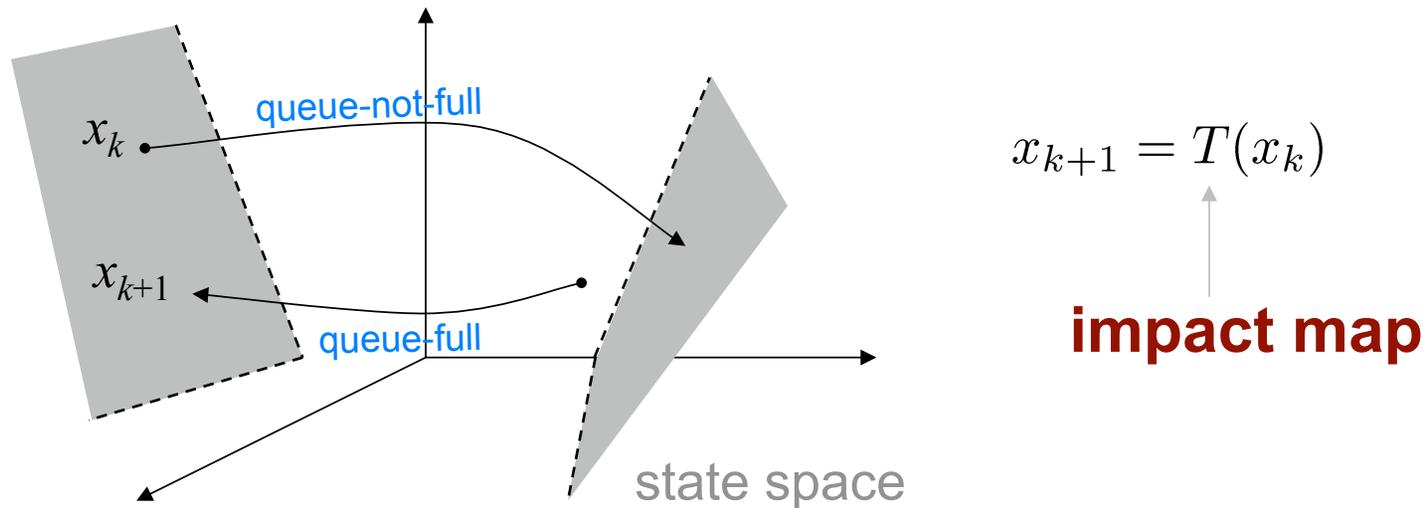
Impact maps are difficult to compute because their computation requires:

Solving the differential equations on each mode (in general only possible for linear dynamics)

Intersecting the continuous trajectories with a surface (often transcendental equations)

It is often possible to prove that T is a contraction without an explicit formula for T...

UC SANTA BARBARA
engineering

Logic-based switched systems framework

application areas

Congestion control in data networks

Vision-based control

Adaptive control

Impact maps

Lyapunov tools

Interconnection of systems

analytical tools

*flexible manipulator*
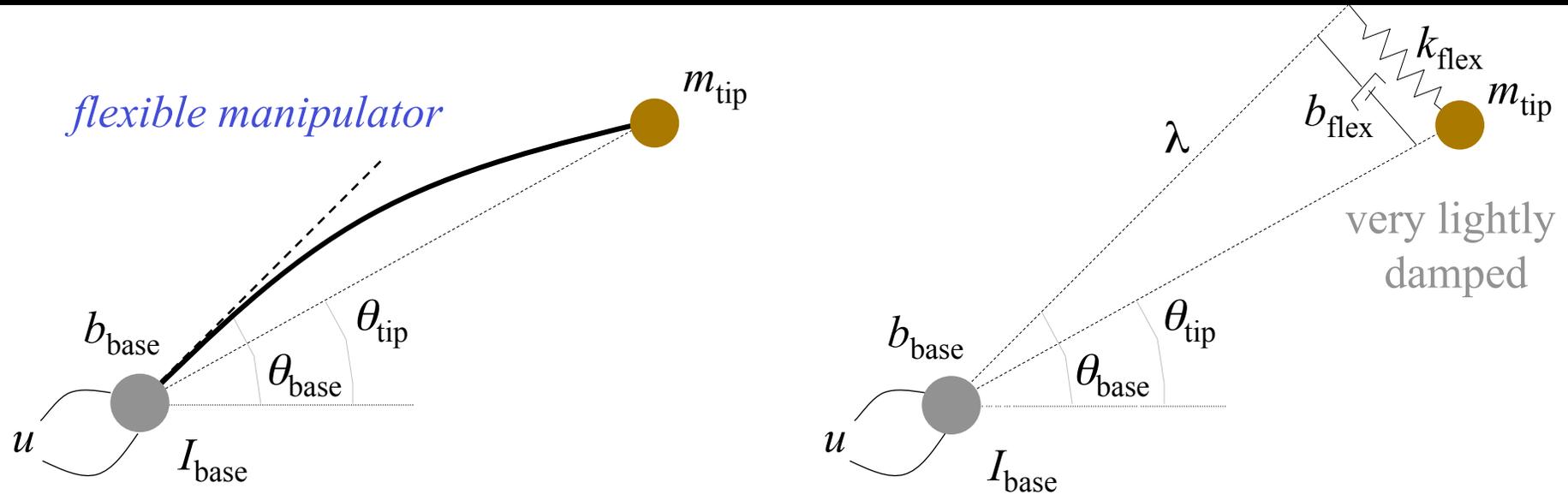
4th dimensional small-bending approximation

very lightly damped

$$m_{\text{tip}}\ell^2\ddot{\theta}_{\text{tip}} = \ell k_{\text{flex}}(\theta_{\text{base}} - \theta_{\text{tip}}) + \ell b_{\text{flex}}(\dot{\theta}_{\text{base}} - \dot{\theta}_{\text{tip}})$$

$$I_{\text{base}}\ddot{\theta}_{\text{base}} = -b_{\text{base}}\dot{\theta}_{\text{base}} + \ell k_{\text{flex}}(\theta_{\text{tip}} - \theta_{\text{base}}) + \ell b_{\text{flex}}(\dot{\theta}_{\text{tip}} - \dot{\theta}_{\text{base}}) + k_{\text{motor}}u$$

Control objective: drive θ_{tip} to zero, using feedback from

$\theta_{\text{base}} \rightarrow$ encoder at the base

$\theta_{\text{tip}} \rightarrow$ machine vision (essential to increase the damping of the flexible modes in the presence of noise)
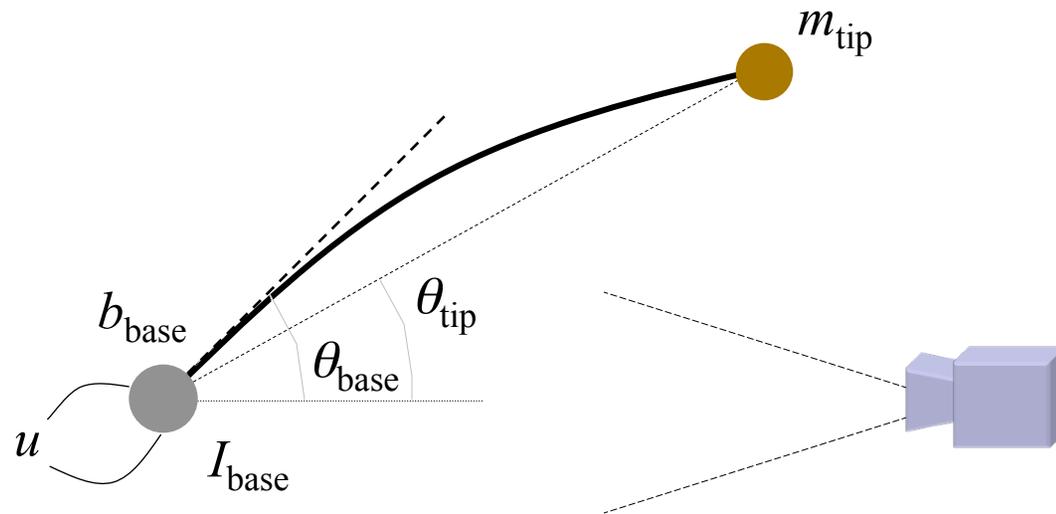
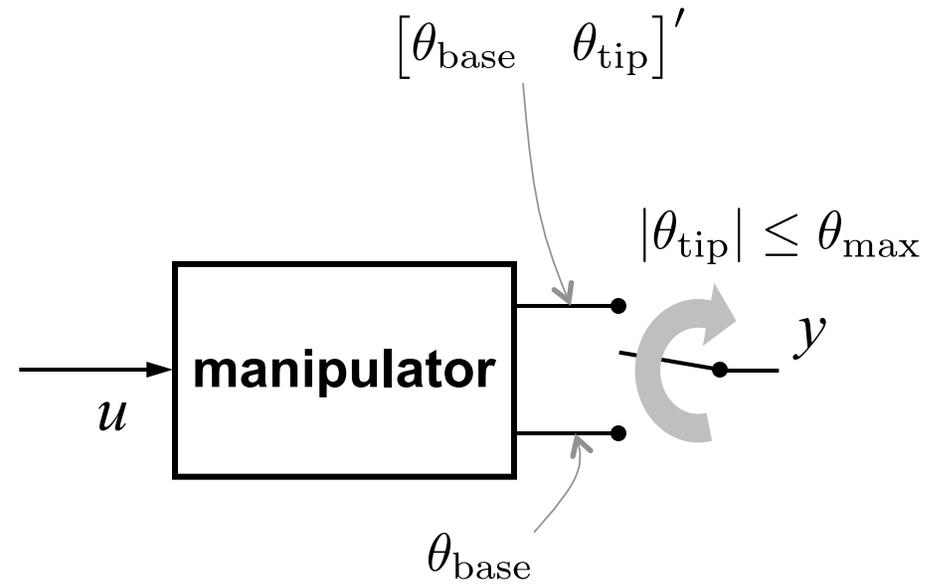To achieve high accuracy in the measurement of q_{tip} the camera must have a *small field of view*

feedback output: $\quad y := \begin{cases} \begin{bmatrix} \theta_{\mathrm{base}} & \theta_{\mathrm{tip}} \end{bmatrix}' & |\theta_{\mathrm{tip}}| \leq \theta_{\max} \\ \theta_{\mathrm{base}} & |\theta_{\mathrm{tip}}| > \theta_{\max} \end{cases}$

Control objective: drive θ_{tip} to zero, using feedback from
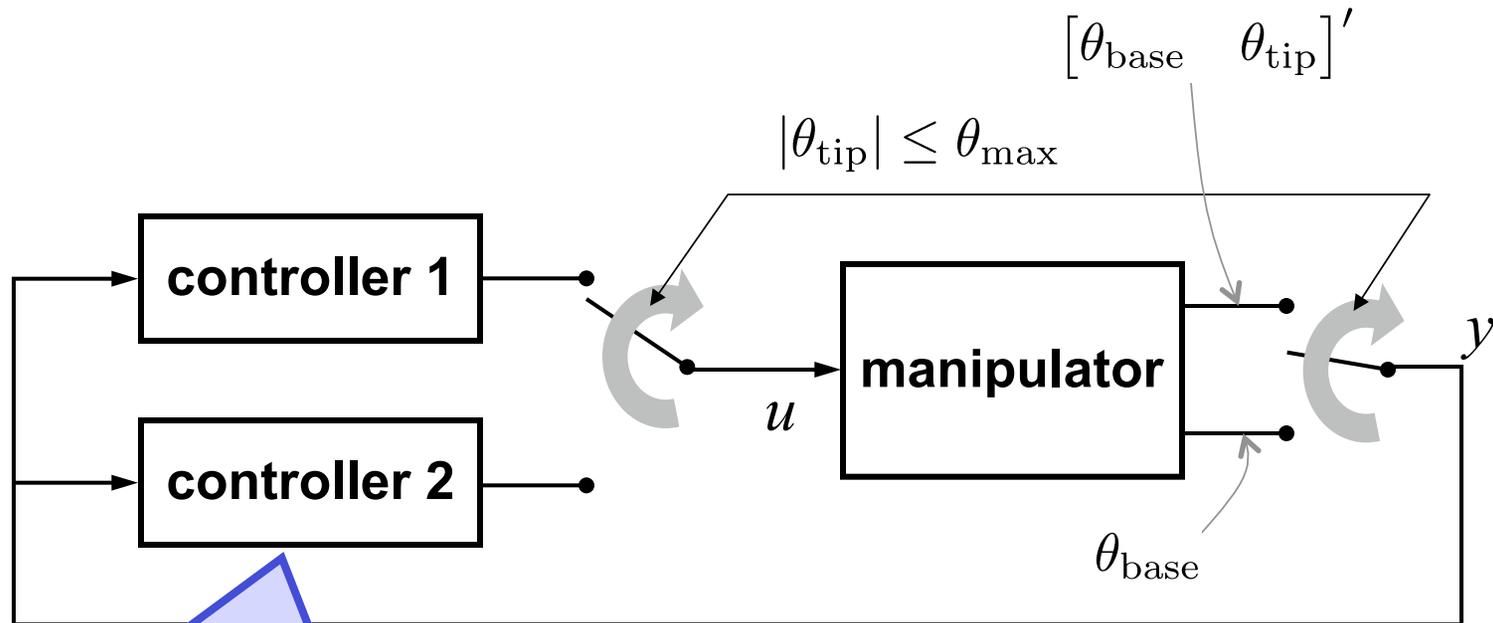
$\theta_{\mathrm{base}} \rightarrow$ encoder at the base

$\theta_{\mathrm{tip}} \rightarrow$ machine vision (essential to increase the damping of the flexible modes in the presence of noise)
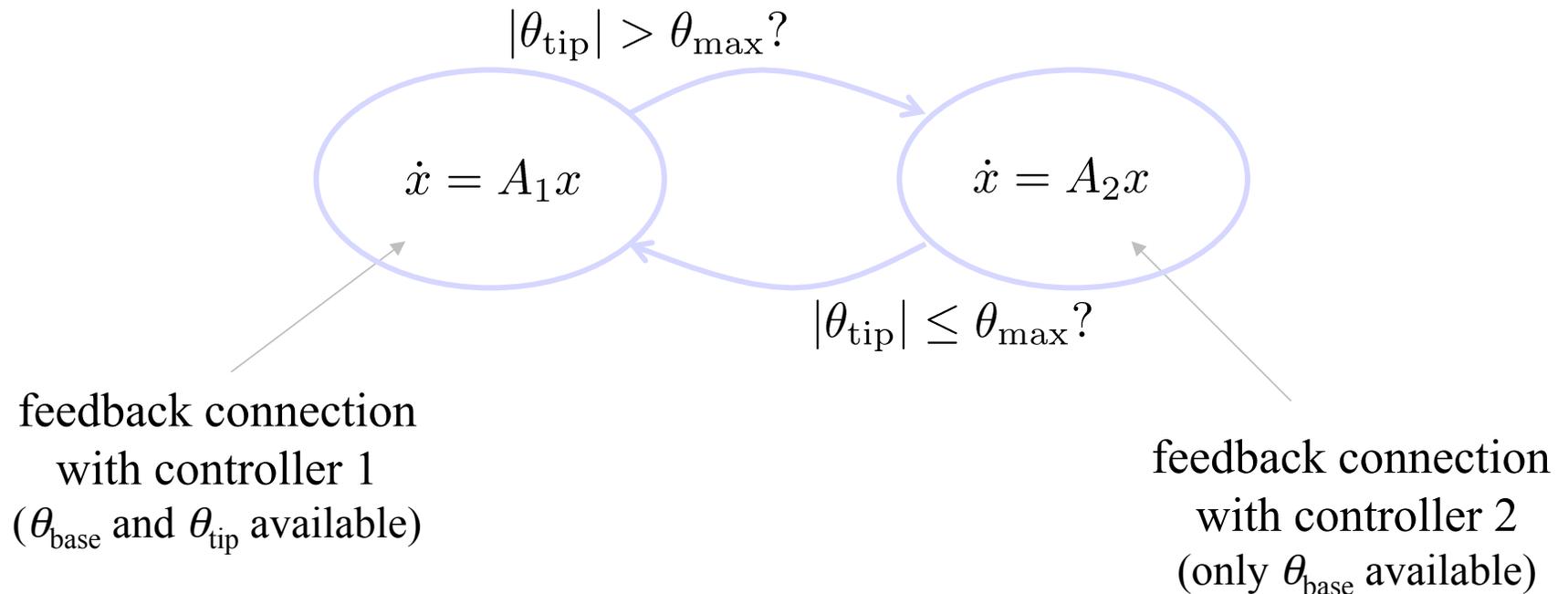
$$\begin{bmatrix} \theta_{\text{base}} & \theta_{\text{tip}} \end{bmatrix}'$$

$$|\theta_{\text{tip}}| \leq \theta_{\text{max}}$$

manipulator

u

y

θ_{base}

$$\left[\theta_{\text{base}} \quad \theta_{\text{tip}}\right]'$$

$$|\theta_{\text{tip}}| \leq \theta_{\text{max}}$$

controller 1

manipulator

y

u

θ_{base}

controller 2

controller 1 optimized for feedback from θ_{base} and θ_{tip}
and
controller 2 optimized for feedback only from θ_{base}

E.g., LQG/LQR controllers that minimize $\displaystyle\lim_{T\to\infty} \frac{1}{T} E\left[\int_0^T \theta_{\text{tip}}^2 + \dot{\theta}_{\text{tip}}^2 + \rho u^2 dt\right]$
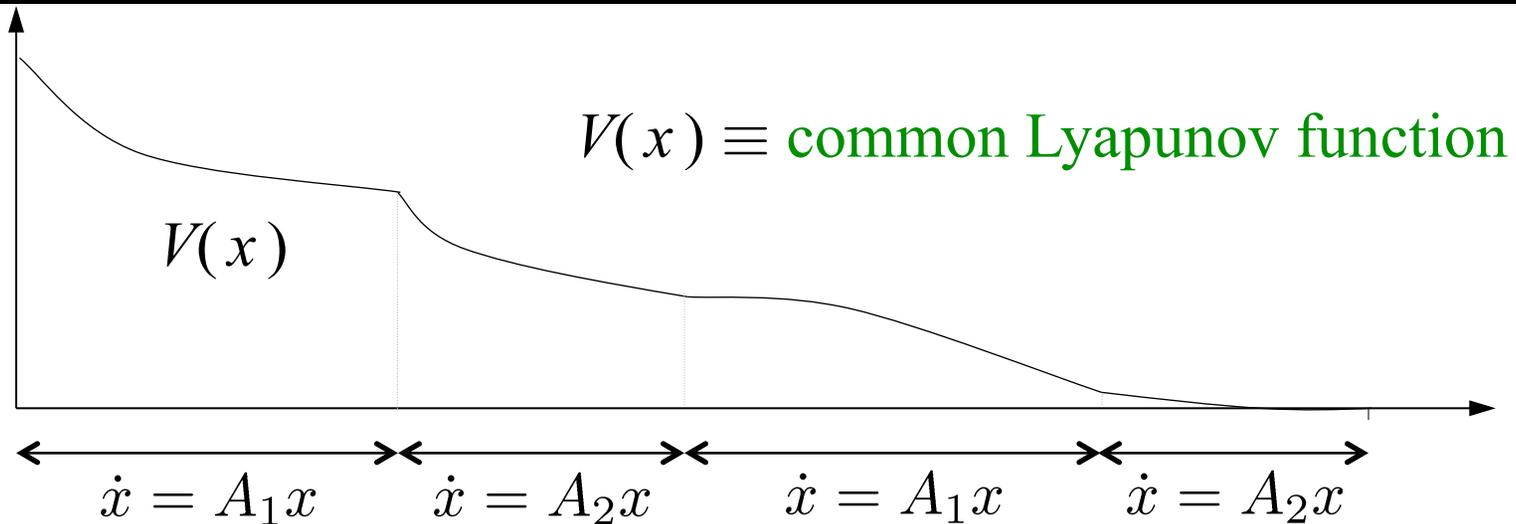
$$|\theta_{\text{tip}}| > \theta_{\text{max}}?$$

$$\dot{x} = A_1 x \qquad \dot{x} = A_2 x$$

$$|\theta_{\text{tip}}| \leq \theta_{\text{max}}?$$

feedback connection
with controller 1
(θ_{base} and θ_{tip} available)

feedback connection
with controller 2
(only θ_{base} available)

How does one check if the overall system is *stable* and that

$$x := \begin{bmatrix} \theta_{\text{tip}} & \dot{\theta}_{\text{tip}} & \theta_{\text{base}} & \dot{\theta}_{\text{base}} & x'_C \end{bmatrix}'$$

eventually *converges to zero* ?

controller's state

$V(x) \equiv$ common Lyapunov function

$V(x)$

$$\dot{x} = A_1 x \qquad \dot{x} = A_2 x \qquad \dot{x} = A_1 x \qquad \dot{x} = A_2 x$$

Suppose that there exists a cont. diff. function $V(x)$ such that

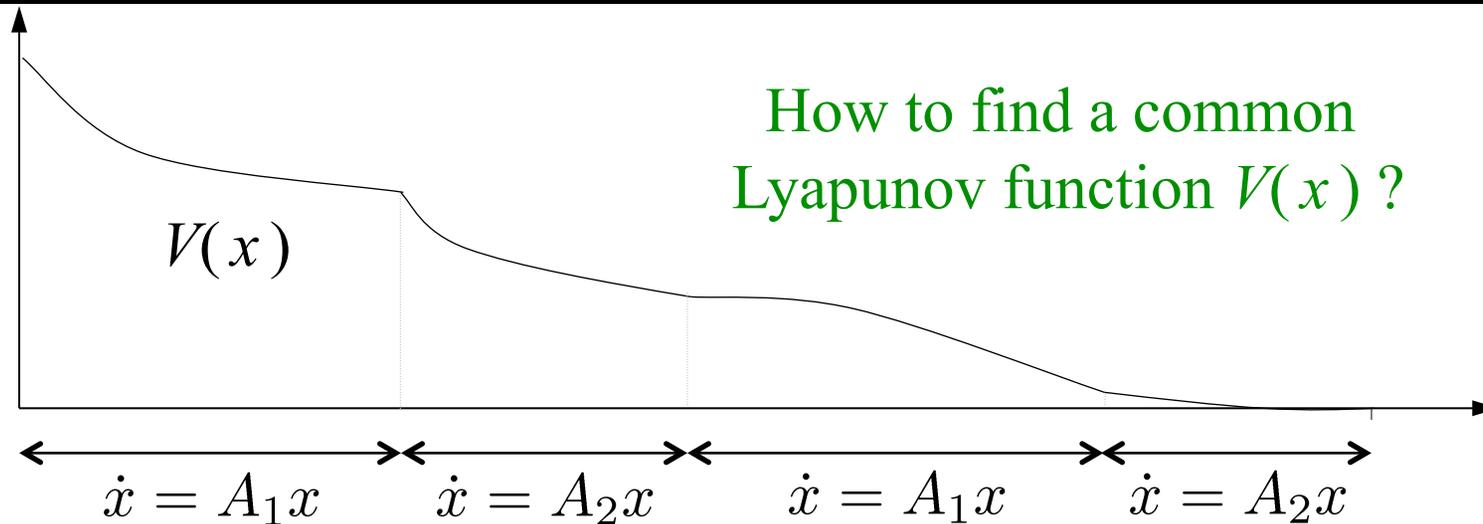$V(x)$ provides a
measure of the size of x:

- positive definite
- radially unbounded

$V(x)$ decreases along
trajectories of both systems:

$$\frac{\partial V}{\partial x} A_i x < 0 \qquad i \in \{1, 2\}, x \neq 0$$

switched system is stable and $x \to 0$ as $t \to \infty$
independently of how switching takes place

How to find a common
Lyapunov function $V(x)$?

$V(x)$

$\dot{x} = A_1 x$ $\dot{x} = A_2 x$ $\dot{x} = A_1 x$ $\dot{x} = A_2 x$
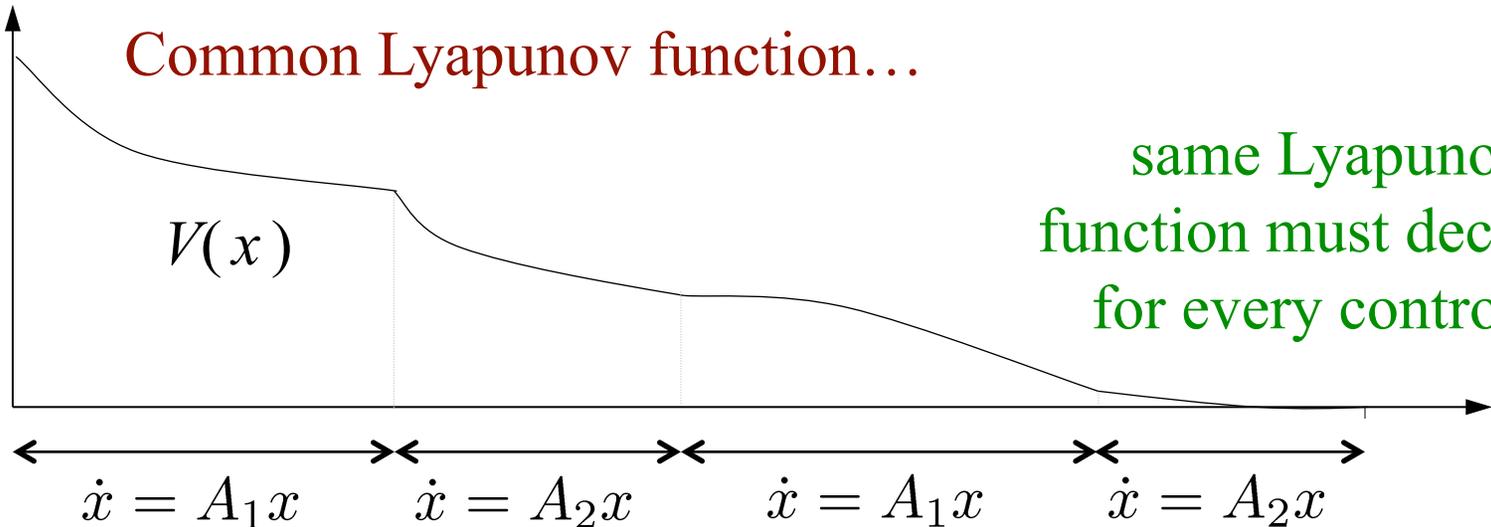
Algebraic conditions for the existence of a common Lyapunov function

- The matrices commute, i.e., $A_1 A_2 = A_2 A_1$ [S1,S2]

- The Lie Algebra generated by $\{A_1, A_2\}$ is solvable

- For all $\lambda \in [0,1]$ the matrices $\lambda A_1 + (1 - \lambda) A_2$ and $\lambda A_1 + (1 - \lambda) A_2^{-1}$ are asymptotically stable (only for 2×2 matrices)

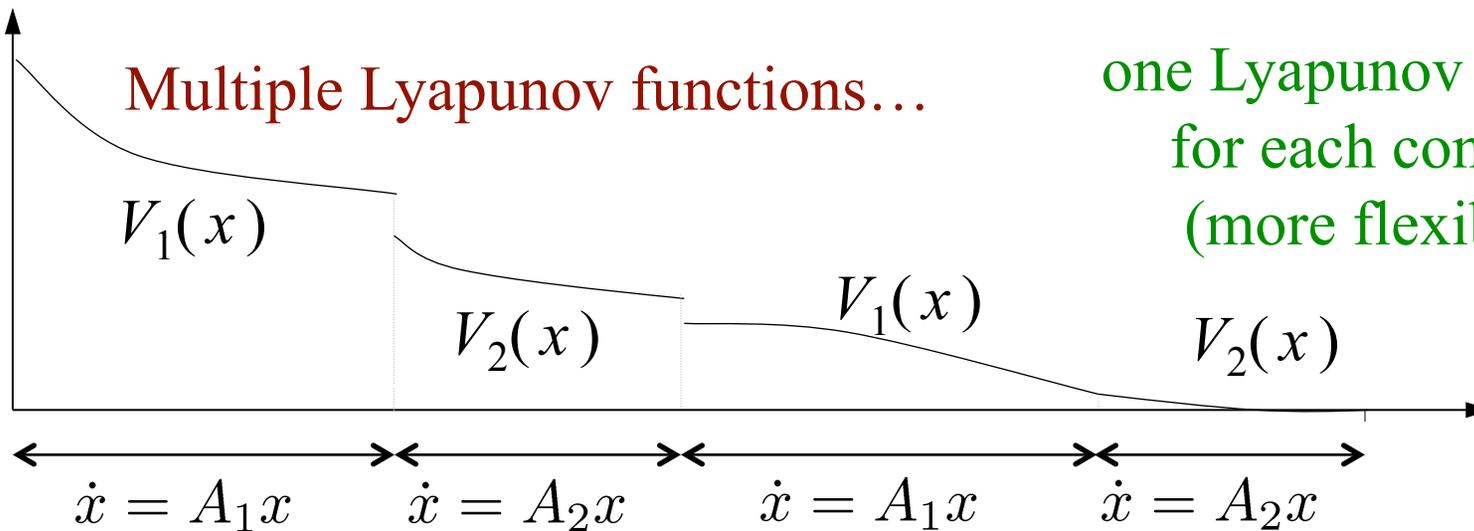But, all these conditions fail for the problem at hand …

Multiple Lyapunov functions

UC SANTA BARBARA
engineering

Common Lyapunov function…

$V(x)$

same Lyapunov
function must decrease
for every controller

$\dot{x} = A_1 x$ $\dot{x} = A_2 x$ $\dot{x} = A_1 x$ $\dot{x} = A_2 x$

Multiple Lyapunov functions…

one Lyapunov function
for each controller
(more flexibility)

$V_2(x)$

$V_1(x)$

$V_1(x)$

$V_2(x)$

$\dot{x} = A_1 x$ $\dot{x} = A_2 x$ $\dot{x} = A_1 x$ $\dot{x} = A_2 x$

[2,3, etc.]

Common Lyapunov function…

$V(x)$

same Lyapunov
function must decrease
for every controller

$$\dot{x} = A_1 x \qquad \dot{x} = A_2 x \qquad \dot{x} = A_1 x \qquad \dot{x} = A_2 x$$

Multiple Lyapunov functions…

$V_1(x)$

$V_2(x)$

$V_1(x)$

$V_2(x)$

one Lyapunov function
for each controller
(more flexibility)

$$\dot{x} = A_1 x \qquad \dot{x} = A_2 x \qquad \dot{x} = A_1 x \qquad \dot{x} = A_2 x$$

[2,3, etc.]

$$V_1(x)$$

$$V_2(x)$$

$$V_1(x)$$

$$V_2(x)$$

$$\dot{x} = A_1 x \qquad \dot{x} = A_2 x \qquad \dot{x} = A_1 x \qquad \dot{x} = A_2 x$$
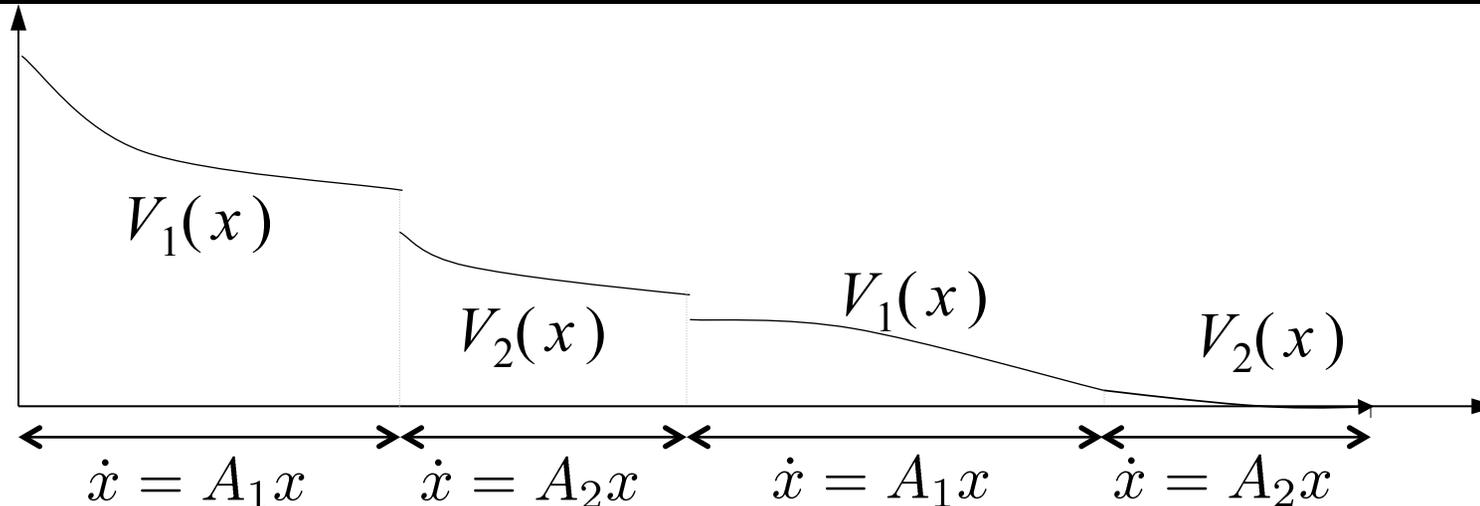
Suppose that exist positive definite, radially unbounded cont. diff. functions $V_1(x)$, $V_2(x)$ such that

$V_i(x)$ decreases along trajectories of A_i:

$$\frac{\partial V_i}{\partial x} A_i x < 0 \quad i \in \{1, 2\}$$
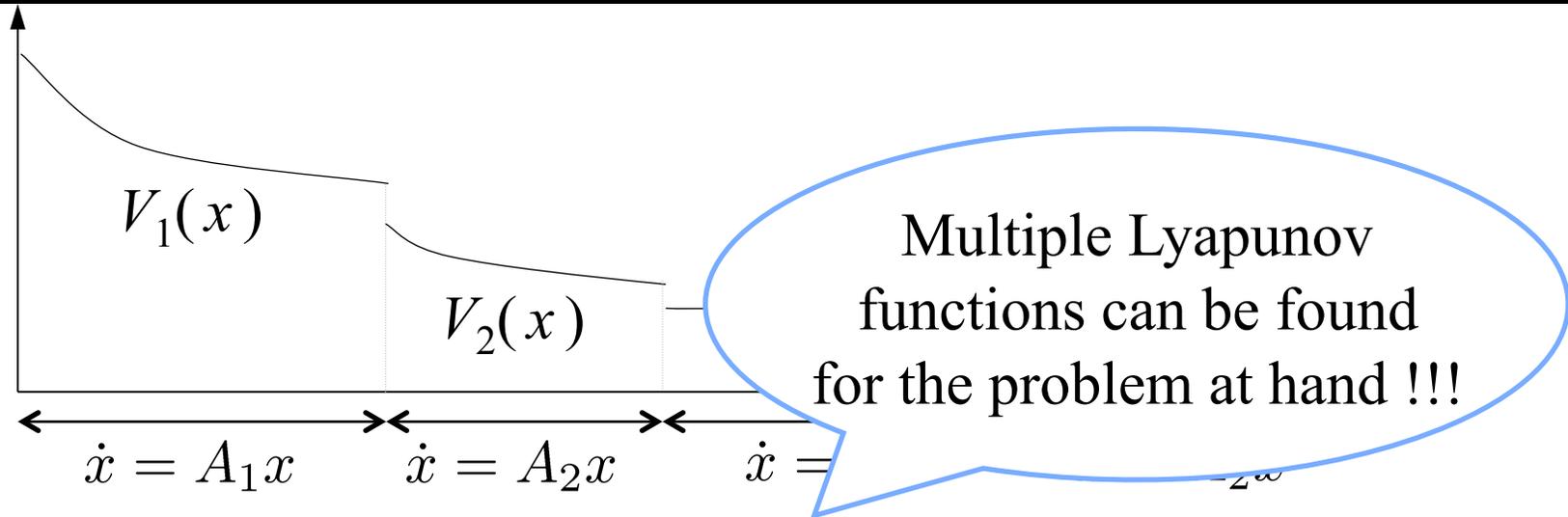
$V_i(x)$ does not increase during transitions:

$$V_i(z) \geq V_j(z)$$

at points z where a switching from i to j can occur

switched system is stable and $x \to 0$ as $t \to \infty$

LaSalle-like versions of this results that only require $\frac{\partial V_i}{\partial x} A_i x \leq 0$, $i \in \{1, 2\}$ are also available [4]

$V_1(x)$

$V_2(x)$

$\dot{x} = A_1 x$ $\quad$ $\dot{x} = A_2 x$ $\quad$ $\dot{x} =$

Multiple Lyapunov
functions can be found
for the problem at hand !!!

Suppose that exist positive definite, radially unbounded cont. diff. functions $V_1(x)$, $V_2(x)$ such that

$V_i(x)$ decreases along trajectories of A_i:

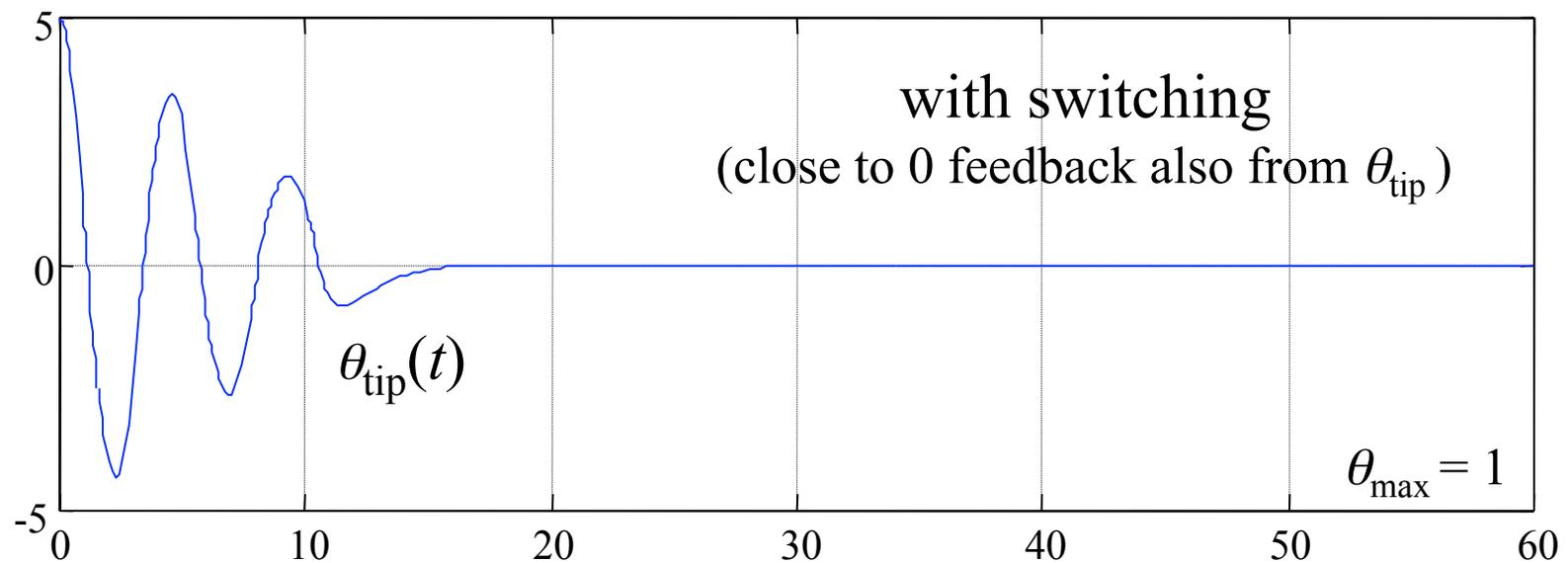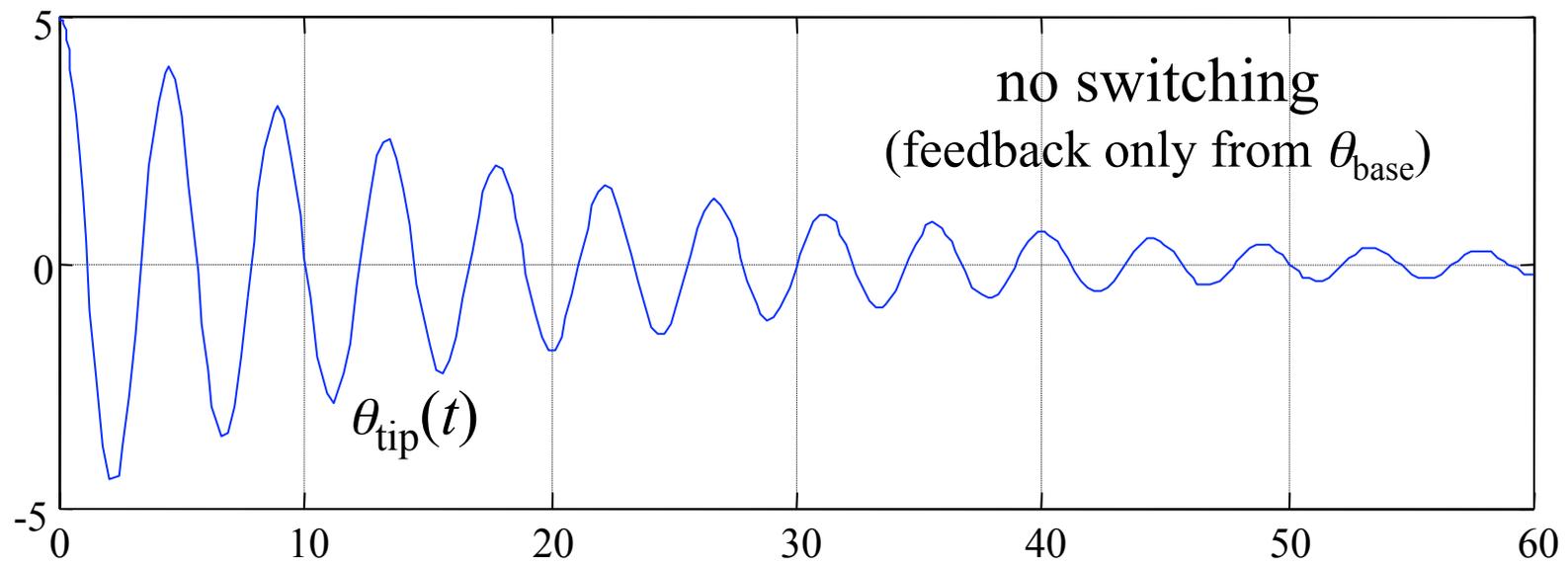$$\frac{\partial V_i}{\partial x} A_i x < 0 \quad i \in \{1, 2\}$$

$V_i(x)$ does not increase during transitions:

$$V_i(z) \geq V_j(z)$$

at points z where a switching from i to j can occur

switched system is stable and $x \to 0$ as $t \to \infty$

[S2]

Closed-loop response

no switching
(feedback only from θ_{base})

$\theta_{\text{tip}}(t)$

with switching
(close to 0 feedback also from θ_{tip})

$\theta_{\text{tip}}(t)$

$\theta_{\text{max}} = 1$

[S2]

*When will a small perturbation in the dynamics result in a
small perturbation in the switched system's trajectory?*

For purely continuous systems (difference or differential equations)
Lyapunov stability automatically provides some degree of robustness

This is not necessarily true for switched systems:
When is this a problem?
Is there a notion of stability that automatically provides robustness?

Important for …
1. numerical **simulation** of switched systems
2. digital **implementation** of switched controllers
3. **analysis** and **design** based on numerical methods

[A. Teel, R. Goebel, R. Sanfelice have important results in this area]

Logic-based switched systems framework

application areas

{ Congestion control in data networks

Vision-based control

Adaptive control }

{ Impact maps

Lyapunov tools

Interconnection of systems }

analytical tools

> process can either be:
> $$\mathbf{P}_1: \quad \dot{x} = A_1 x + b_1 u, \qquad y = c_1 x$$
> or
> $$\mathbf{P}_2: \quad \dot{x} = A_2 x + b_2 u, \qquad y = c_2 x$$

$$u \rightarrow \boxed{\textbf{process}} \rightarrow y$$

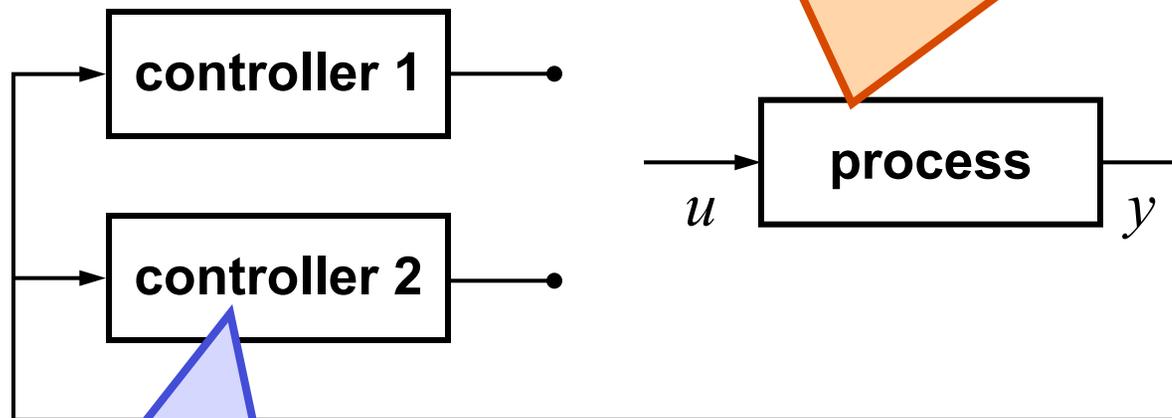***Control objective***: Stabilize process (keep state of the process bounded)

Prototype adaptive control problem

process can either be:
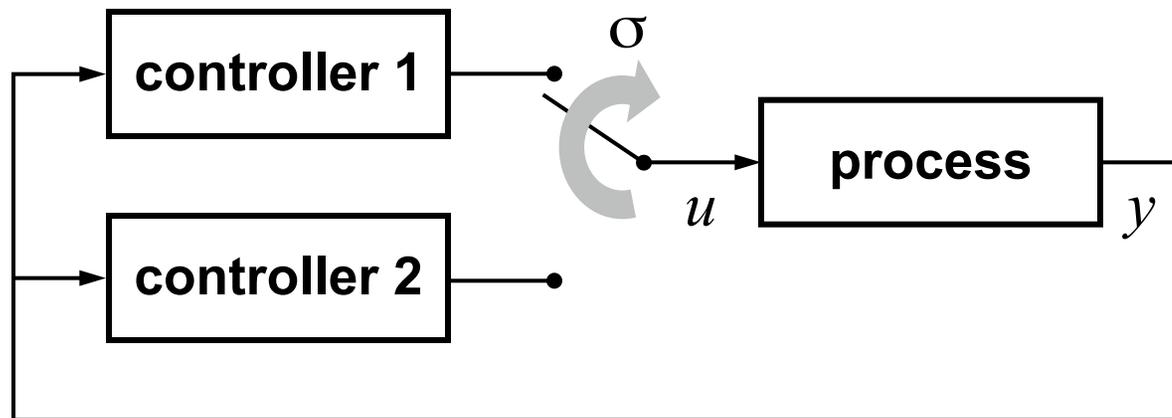$$\mathbf{P}_1: \quad \dot{x} = A_1 x + b_1 u, \qquad y = c_1 x$$
or
$$\mathbf{P}_2: \quad \dot{x} = A_2 x + b_2 u, \quad y = c_2 x$$

controller 1

controller 2

process

u　　　　y

controller 1 stabilizes $\mathbf{P}_1$
and
controller 2 stabilizes $\mathbf{P}_2$

UC SANTA BARBARA
engineering

How to choose online
which controller to use?

$\sigma \equiv$ *switching signal* taking values on the set $\{1,2\}$
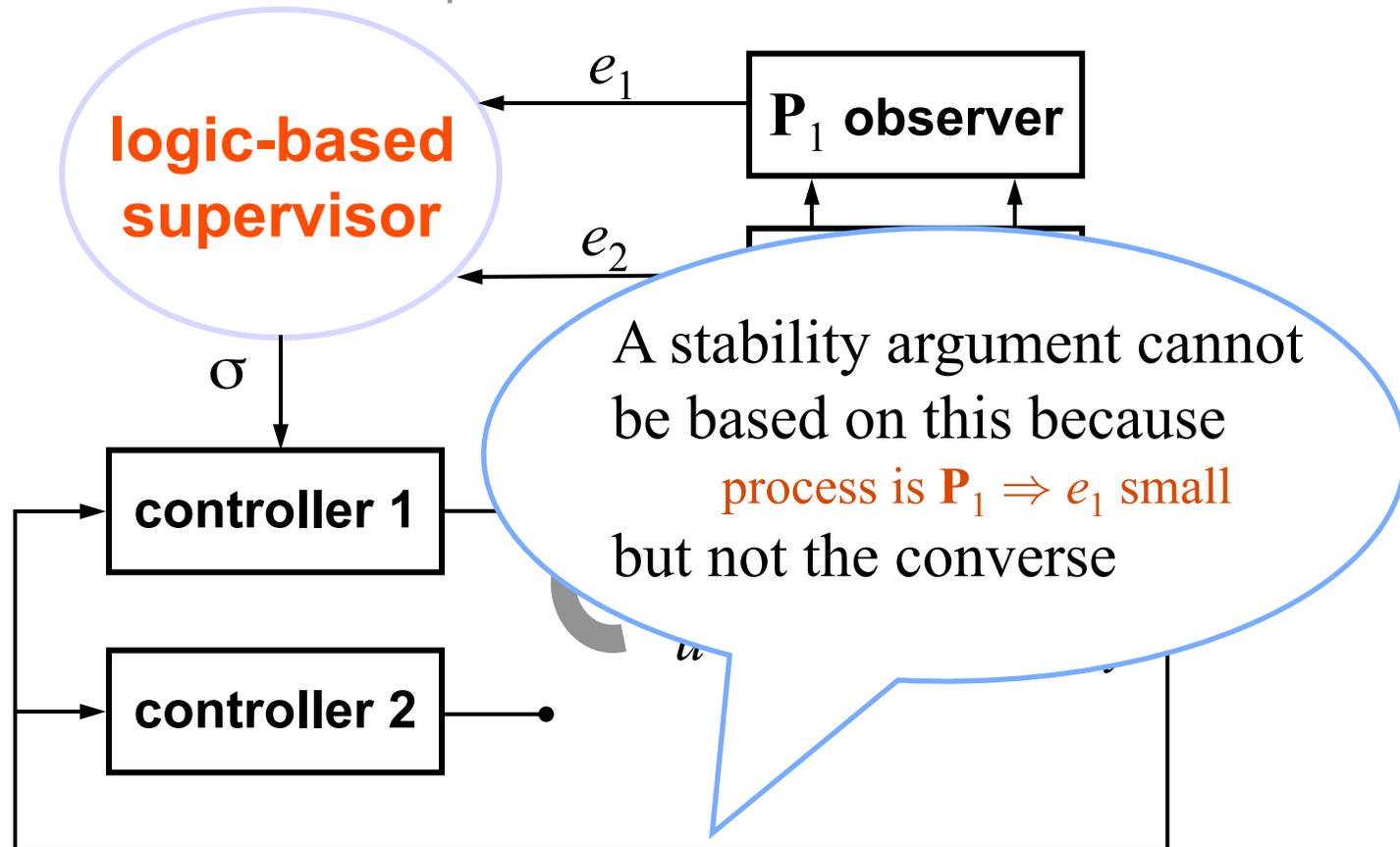
output estimation errors

"likelihood" of process being P_1 is high

e_1 small ⟹ "likelihood" of process being P_1 is high ⟹ should use controller 1

Certainty equivalence inspired

output estimation errors

logic-based
supervisor

e_1

$\mathbf{P}_1$ **observer**

e_2

σ

controller 1

controller 2

A stability argument cannot
be based on this because
process is $\mathbf{P}_1 \Rightarrow e_1$ small
but not the converse

e_1 small ➡ "likelihood" of
process being
$\mathbf{P}_1$ is high ➡ should use
controller 1

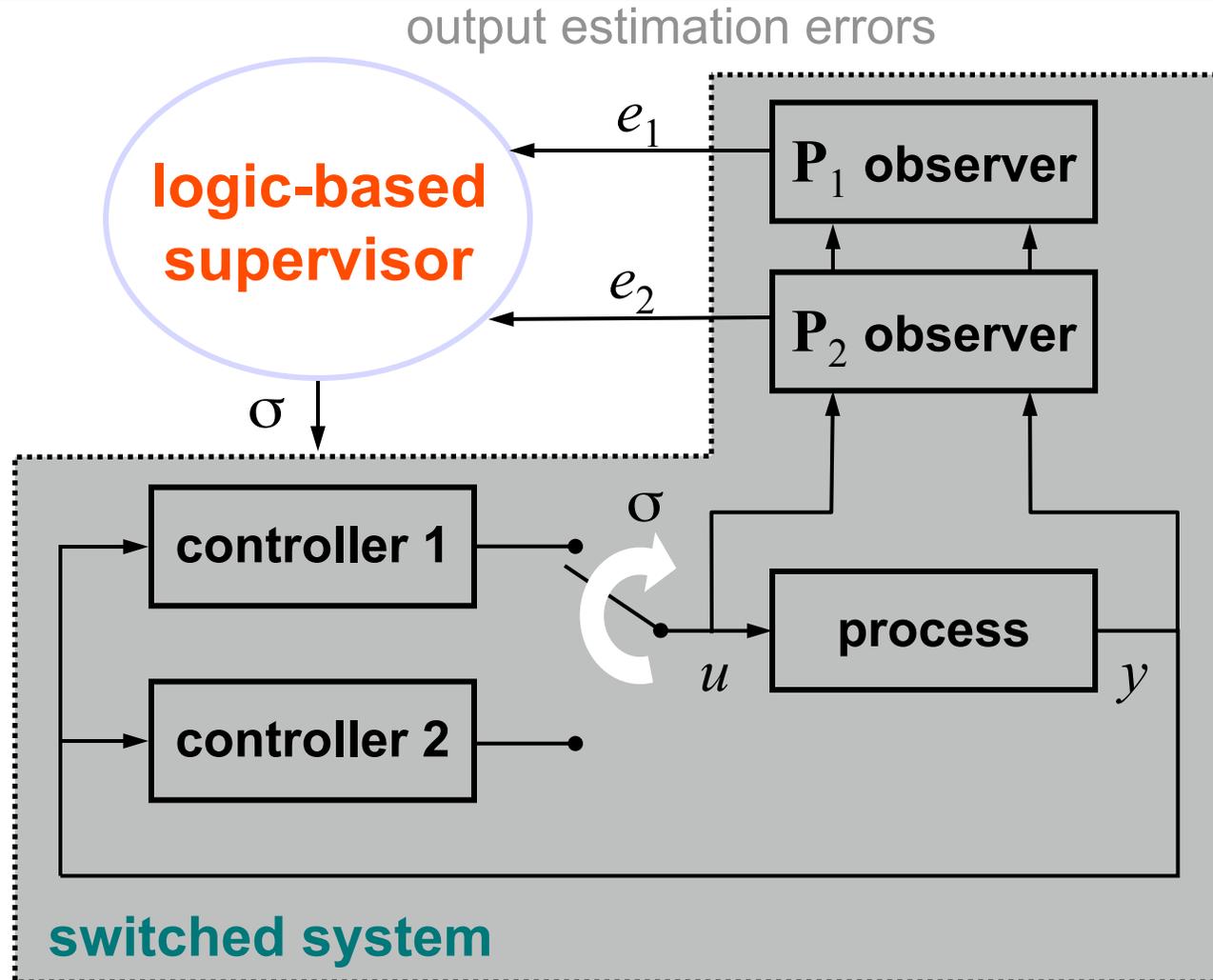Certainty equivalence inspired

Estimator-based architecture

output estimation errors

logic-based supervisor

e_1

$\mathbf{P}_1$ observer

e_2

$\mathbf{P}_2$ observer

σ

controller 1

σ

controller 2

process

u

y

switched system

$$\dot{x} = A_\sigma x \qquad e_p = C_p x \quad p \in \{1, 2\}$$

$$\sigma = 1$$
$$\dot{w}_p = -\lambda w_p + e_p^2$$

$$\pi_1 > \pi_2(1+h)?$$

$$\pi_2 > \pi_1(1+h)?$$
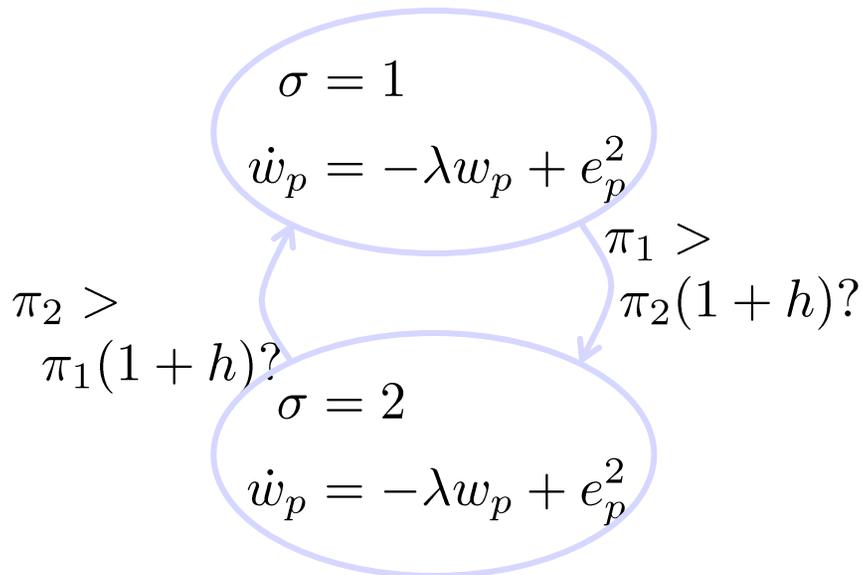
$$\sigma = 2$$
$$\dot{w}_p = -\lambda w_p + e_p^2$$
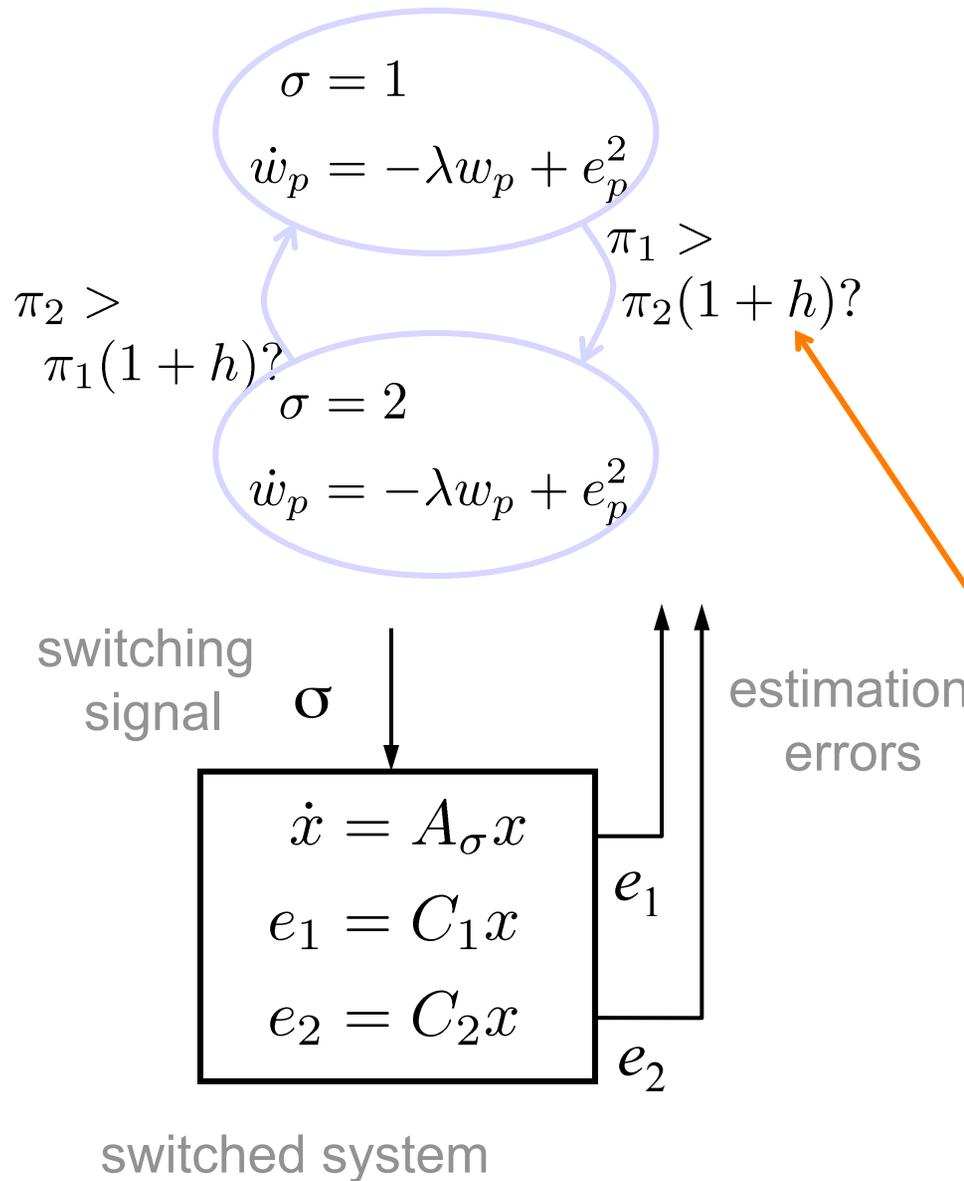
$$\pi_p := w_p + \varepsilon = \int_0^t e^{-\lambda(t-\tau)} e_p^2 \, d\tau + \varepsilon$$

$$\varepsilon > 0, \ \lambda > 0, \ p \in \{1, 2\}$$

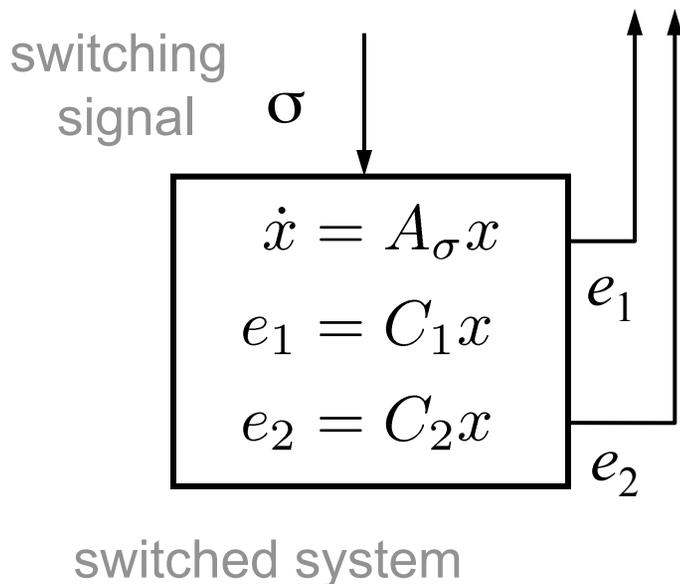***performance signals***
(measure the "size" of
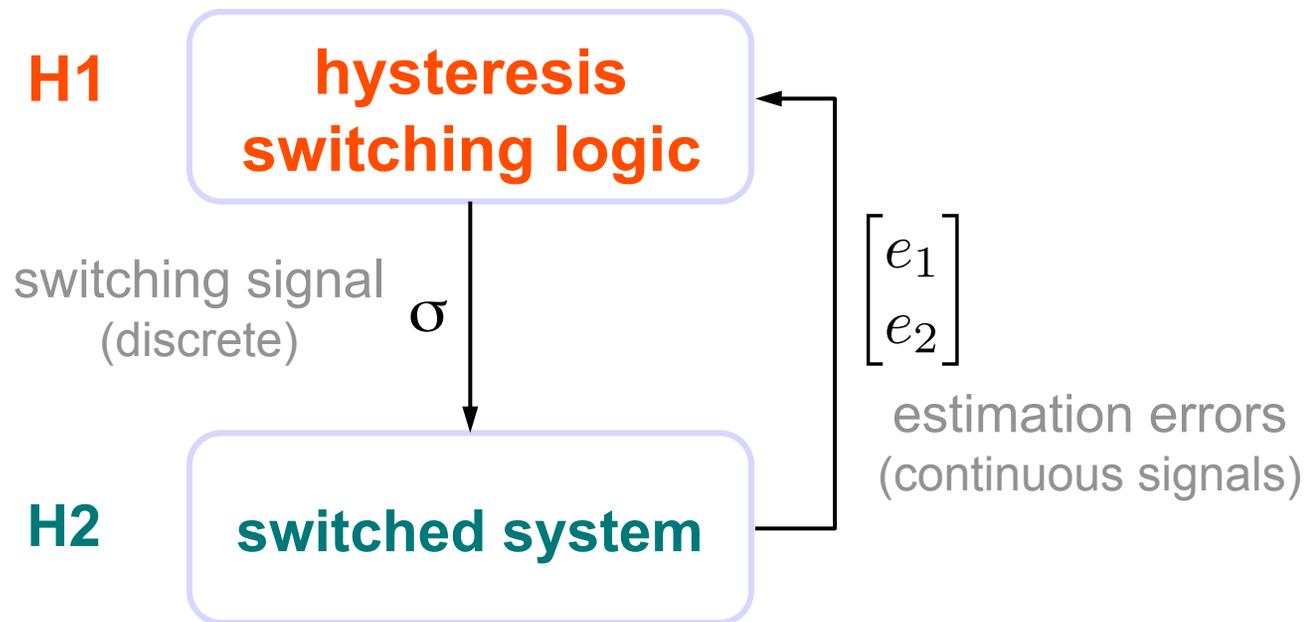the estimation errors)

hysteresis constant (positive)

switching
signal σ

estimation
errors

$$\dot{x} = A_\sigma x$$
$$e_1 = C_1 x$$
$$e_2 = C_2 x$$

e_1

e_2

switched system

$$\sigma = 1$$
$$\dot{w}_p = -\lambda w_p + e_p^2$$

$$\pi_1 > \pi_2(1 + h)?$$

$$\pi_2 > \pi_1(1 + h)?$$

$$\sigma = 2$$
$$\dot{w}_p = -\lambda w_p + e_p^2$$

How does one verify if
x remains bounded along
solutions to the hybrid system?

switching
signal σ

$$\dot{x} = A_\sigma x$$
$$e_1 = C_1 x$$
$$e_2 = C_2 x$$

e_1

e_2

switched system

Analyzing the system as a whole is
too difficult. We need to:

1. *abstract* the complex behavior of
   each subsystem (supervisor &
   switched) to a small set of
   properties
2. *infer* properties of the overall
   system from the properties of the
   interconnected subsystems

UC SANTA BARBARA
engineering

H1

hysteresis switching logic

switching signal
(discrete)

σ

$\begin{bmatrix} e_1 \\ e_2 \end{bmatrix}$

estimation errors
(continuous signals)

H2 switched system

One can show [S3] that…

H1 has the property that

$$\int_0^t e^{\lambda\tau} e_\sigma^2 d\tau \leq \gamma \left(\min_p \int_0^t e^{\lambda\tau} e_p^2 d\tau \right)$$

finite "L_2-induced gain"
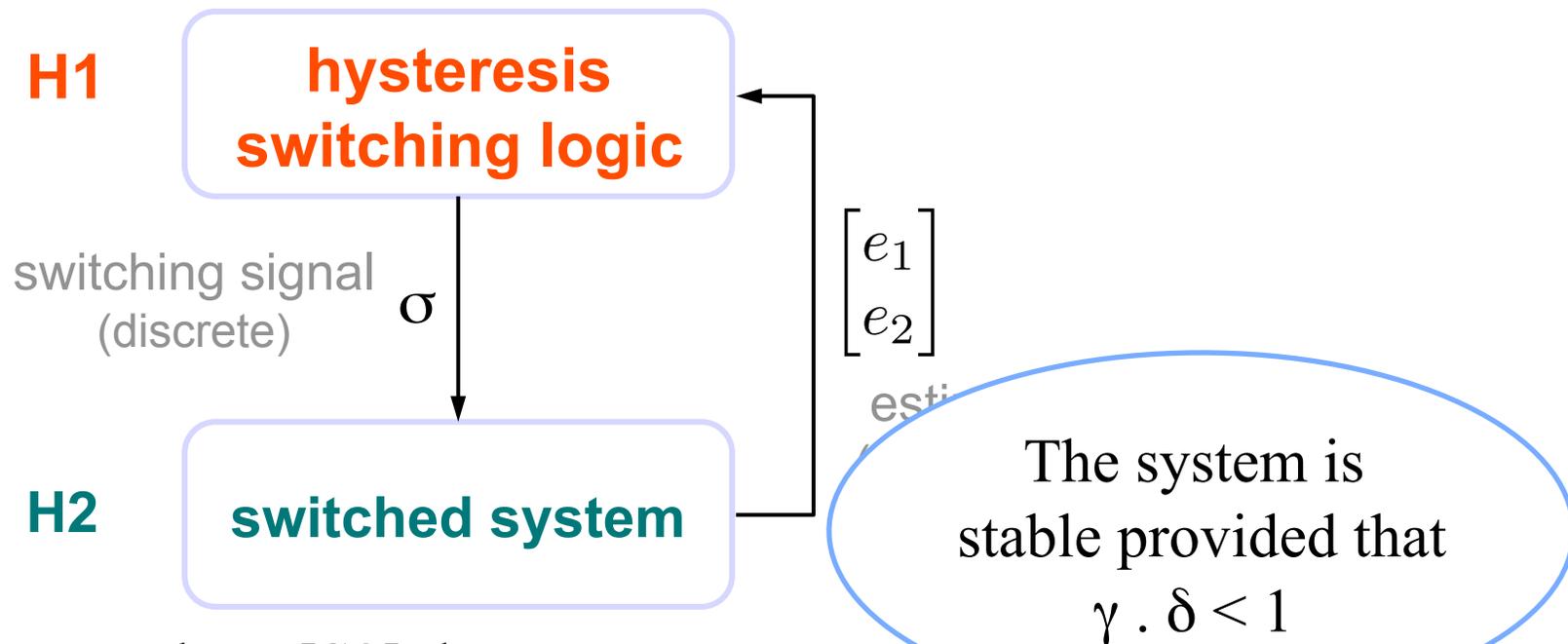from smallest error to
the switched error

H2 has the property that

$$\min_p \int_0^t e^{\lambda\tau} e_p^2 d\tau \leq c_0 + \delta \int_0^t e^{\lambda\tau} e_\sigma^2 d\tau$$

(with $\delta = 0$ when there is no unmodeled dynamics)

vice-versa
("detectability"
through e_σ)

H1

hysteresis switching logic

switching signal (discrete) σ

$\begin{bmatrix} e_1 \\ e_2 \end{bmatrix}$

esti

H2   **switched system**

The system is stable provided that
$$\gamma \cdot \delta < 1$$

One can show [S3] that…

H1 has the property that

$$\int_0^t e^{\lambda\tau} e_\sigma^2 d\tau \leq \gamma \left(\min_p \int_0^t e^{\lambda\tau} e_p^2 d\tau \right)$$

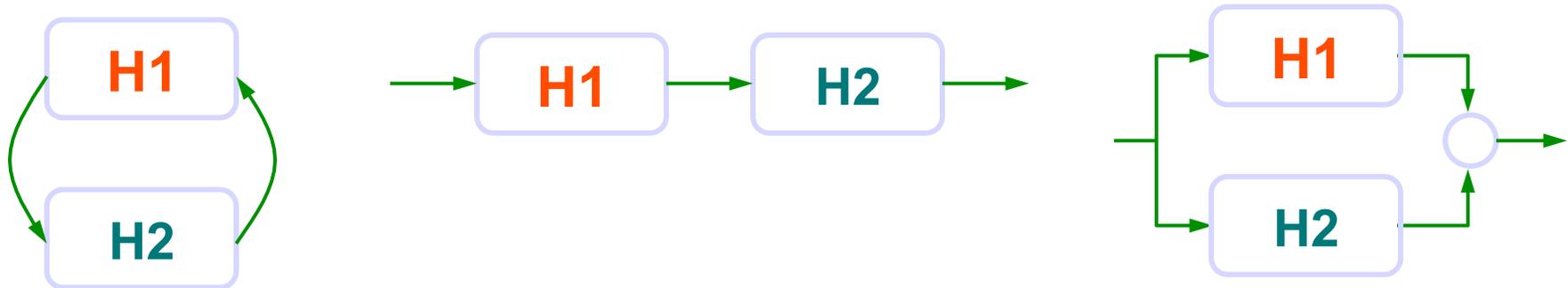finite "L$_2$-induced gain" from smallest error to the switched error

H2 has the property that

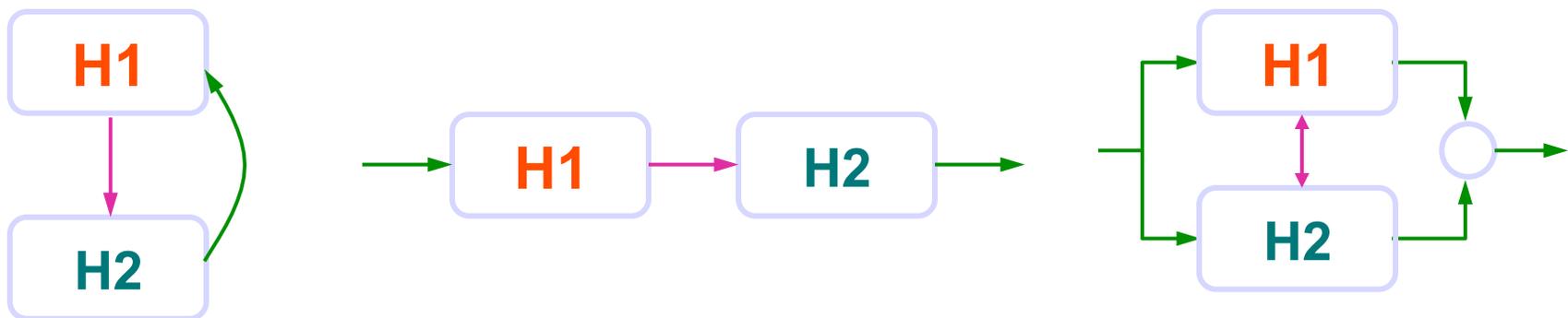$$\min_p \int_0^t e^{\lambda\tau} e_p^2 d\tau \leq c_0 + \delta \int_0^t e^{\lambda\tau} e_\sigma^2 d\tau$$

(with $\delta = 0$ when there is no unmodeled dynamics)

vice-versa ("detectability" through e_s)

UC SANTA BARBARA
engineering

For interconnections through continuous signals, existing tools can be extended to hybrid systems (small gain, passivity, integral quadratic constrains, ISS, etc.) [6,7]

For mixed interconnections new tools need to be developed…

→ continuous signal   → discrete signal

[D. Liberzon & D. Nesic used this to analyze networked control systems with quantization]

application areas

Congestion
control in data
networks

Vision-based
control

Adaptive
control

Impact
maps

Lyapunov
tools

Interconnection
of systems

analytical tools

*Switched systems are
ubiquitous and of significant
practical application*

*A unified theory of
switched systems is starting
to be developed*

References

Background surveys & tutorials:

[S1]   D. Liberzon, A. S. Morse, Basic problems in stability and design of switched systems, In *IEEE Control Systems Magazine*, vol. 19, no. 5, pp. 59-70, Oct. 1999.

[S2]   J. Hespanha. Stabilization Through Hybrid Control. In Encyclopedia of Life Support Systems (EOLSS), volume Control Systems, Robotics, and Automation, 2004

[S3]   J. Hespanha. Tutorial on Supervisory Control. Lecture Notes for the workshop *Control using Logic and Switching* for the 40th Conf. on Decision and Contr., Dec. 2001.

[S4]   R. Goebel, R. Sanfelice, A. Teel. Hybrid dynamical systems. *IEEE Control Systems Magazine* 29:28–93, 2009

Papers referenced specifically in this talk:

[1]   S. Bohacek, J. Hespanha, J. Lee, K. Obraczka. Analysis of a TCP hybrid model. In *Proc. of the 39th Annual Allerton Conference on Communication, Control, and Computing*, Oct. 2001.

[2]   P. Peleties P., R. A. DeCarlo. Asymptotic stability of *m*-switched systems using Lyapunov-like functions. In *Proc. of the 1991 Amer. Contr. Conf.*, pp. 1679–1684, 1991.

[3]   M. S. Branicky. *Studies in Hybrid Systems: Modeling, Analysis, and Control*. Ph.D. thesis, MIT, 1995.

[4]   J. Hespanha. Extending LaSalle's Invariance Principle to Linear Switched Systems. In *Proc. of the 40th Conf. on Decision and Contr.*, Dec. 2001.

[5]   J. Hespanha, A. S. Morse. Certainty Equivalence Implies Detectability. *Syst. & Contr. Lett.*, 36:1-13, Jan. 1999.

[6]   M. Zefran, F. Bullo, M. Stein, A notion of passivity for hybrid systems. In *Proc. of the 40th Conf. on Decision and Contr.*, Dec. 2001.

[7]   J. Hespanha. Root-Mean-Square Gains of Switched Linear Systems. *IEEE Trans. on Automat. Contr.*, 48(11), Nov. 2003.

[8]   J. Grizzle, G. Abba, F. Plestan. Asymptotically Stable Walking for Biped Robots: Analysis via Systems with Impulse Effects. *IEEE Trans. of Autom. Contr.*, 46:1, pp. 51-64, Jan. 2001

[9]   D. Liberzon, D. Nesic. A unified framework for design and analysis of networked and quantized control systems. *IEEE Trans. of Autom. Contr.*, vol. 54, pp. 732-747, Apr. 2009

See also http://www.ece.ucsb.edu/~hespanha/published.html