

Infinite Impulse Response (IIR)

Digital Filters (I)

Mapping analog filters

Yogananda Isukapalli

Design objectives: IIR designs

Given that:

$$H(z) = \sum_{n=0}^{\infty} h[n]z^{-n} = \frac{\sum_{k=0}^M b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}}$$

Or equivalently:

$$\sum_{k=0}^N a_k y[n-k] = \sum_{k=0}^M b_k x[n-k]$$

Require that::

$$h[n] = 0 \quad n < 0$$

$$\sum_{n=0}^{\infty} |h[n]| < \infty$$

Realizable
and stable

General design problem:

Find a_k and b_k 's such that filter responses (time response, frequency response, group delay etc,) approximate the desired responses with some specified error criterion(ex:- MSE)

Design Techniques:

Indirect design:

Mapping analog filters

Direct design:

Direct placement of pole-zeros in the z-plane via closed form solutions.

Optimal designs:

Placement of pole-zeros via computer-aided techniques
open form solutions

Mapping from analog filters:

Given an analog filter:

$$H_a(s) = \frac{\sum_{k=0}^M d_k s^k}{\sum_{k=0}^N c_k s^k}$$

Or equivalently:

$$\sum_{k=0}^N c_k \frac{d^k y_a(t)}{dt^k} = \sum_{k=0}^M d_k \frac{d^k x_a(t)}{dt^k}$$

Use an approximate mapping function to obtain an equivalent digital filter.

Mapping functions:

Mapping differentials

Mapping Integrals

Impulse - Invariant mapping

Bilinear mapping

The matched z-transform

Step-Invariant mapping

others

Mapping differentials:

Backward:

$$\left. \frac{dy_a(t)}{dt} \right|_{t=nT} = \nabla^{(1)}[y[n]] = \frac{y[n] - y[n-1]}{T}$$

Forward:

$$\left. \frac{dy_a(t)}{dt} \right|_{t=nT} = \nabla^{(1)}[y[n]] = \frac{y[n+1] - y[n]}{T}$$

$\nabla^{(1)}$ Backward or forward
difference operator

Generalize:

$$\left. \frac{d^k y_a(t)}{dt^k} \right|_{t=nT} = \frac{d}{dt} \left(\left. \frac{d^{k-1} y_a(t)}{dt^{k-1}} \right|_{t=nT} \right)$$

Also:

$$\nabla^{(k)}[y[n]] = \nabla^{(1)}[\nabla^{(k-1)}[y[n]]]$$

with $\nabla^{(0)}(.) = y[n]$

$$\begin{aligned}
\text{Ex:- } \nabla^{(2)}[y[n]] &= \nabla^{(1)}\left[\frac{y[n] - y[n-1]}{T}\right] \\
&= \frac{1}{T}[\nabla^{(1)}[y[n]] - \nabla^{(1)}[y[n-1]]] \\
&= \frac{1}{T}\left[\frac{1}{T}\{y[n] - y[n-1]\} - \frac{1}{T}\{y[n-1] - y[n-2]\}\right] \\
&= \frac{1}{T^2}[y[n] - 2y[n-1] + y[n-2]]
\end{aligned}$$

Analog filter differential equation becomes:

$$\sum_{k=0}^N c_k \nabla^{(k)}[y[n]] = \sum_{k=0}^M d_k \nabla^{(k)}[x[n]]$$

with
$$\begin{cases} y[n] = y_a(nT) \\ x[n] = x_a(nT) \end{cases}$$

Z-domain function:

Since:
$$Z[\nabla^{(1)}[y[n]]] = \left[\frac{1-z^{-1}}{T}\right]Y(z)$$

then:
$$Z[\nabla^{(k)}[y[n]]] = \left[\frac{1-z^{-1}}{T}\right]^k Y(z)$$

and

$$H(z) = \frac{\sum_{k=0}^M d_k \left[\frac{1-z^{-1}}{T}\right]^k}{\sum_{k=0}^N c_k \left[\frac{1-z^{-1}}{T}\right]^k}$$

is the digital filter function via mapping from the analog filter $H_a(s)$

Compare $H(z)$ with $H_a(s)$

$$H_a(s) = \frac{\sum_{k=0}^M d_k s^k}{\sum_{k=0}^N c_k s^k}$$

Conclusion:

$$s = \frac{1 - z^{-1}}{T} \quad \text{Backward difference mapping}$$

$$s = \frac{z - 1}{T} \quad \text{Forward difference mapping}$$

$$\nabla^{(1)}[y[n]] = \frac{y[n+1] - y[n]}{T}$$

Mapping differentials: A summary

Given a desired analog filter $H_a(s)$, two mapping functions

$$s = \frac{1 - z^{-1}}{T} \quad \text{and} \quad s = \frac{z - 1}{T}$$

may then be substituted to yield a corresponding digital filter $H(z)$. The procedure is simple and straightforward

Desirable properties of mapping functions:

- (a) The $j\omega'$ axis ($s = j\omega'$) in the s-plane should be mapped on to the unit circle in the z-plane. This preserves the frequency selective properties of analog filters.
- (b) Points in the LHS of the s-plane ($\text{Re}(s) < 0$) should be mapped to inside the unit circle ($|z| < 1$). Stability property will be preserved

Evaluation of difference mapping functions:

$$\text{Backward difference: } s = \frac{1 - z^{-1}}{T} \quad \text{or} \quad z = \frac{1}{1 - sT}$$

Now we can show: let $s = j\omega'$

$$(1) \quad z = \frac{1}{1 - j\omega'T} = \frac{1}{2} \left(1 + \frac{1 + j\omega'T}{1 - j\omega'T} \right)$$

$$= \frac{1}{2} (1 + e^{j2 \tan^{-1} \omega'T})$$

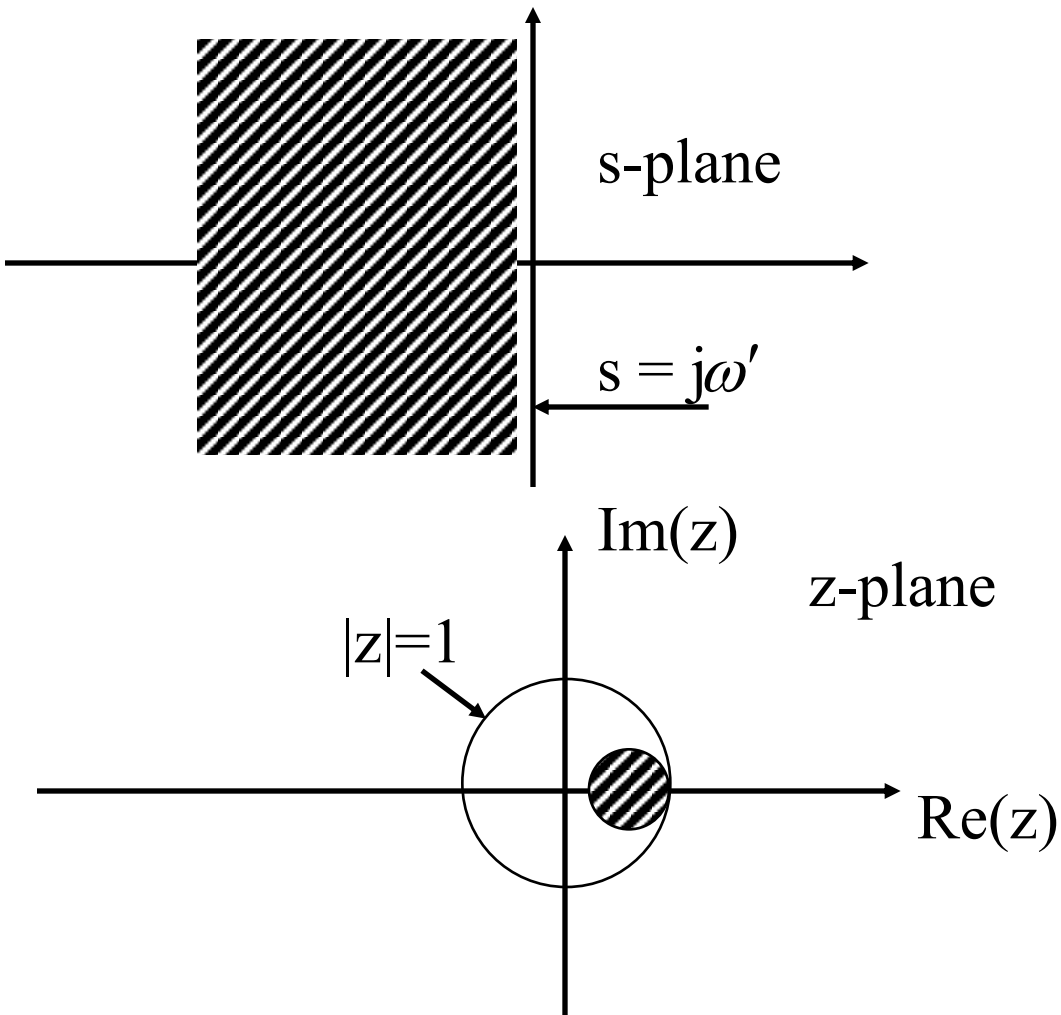
$$(2) \quad \text{Re}(z) = \frac{1}{2} + \frac{\cos(2 \tan^{-1}(\omega'T))}{2}$$

$$(3) \quad \text{Im}(z) = \frac{1}{2} \sin(2 \tan^{-1}(\omega'T))$$

$$(4) \quad \left\{ \text{Re}(z) - \frac{1}{2} \right\}^2 + \{ \text{Im}(z) \}^2 = \left(\frac{1}{2} \right)^2$$

(5) with $sT = \alpha + j\beta$, $\alpha < 0$,

$$|z| = \frac{1}{\sqrt{(1-\alpha)^2 + \beta^2}} < 1$$

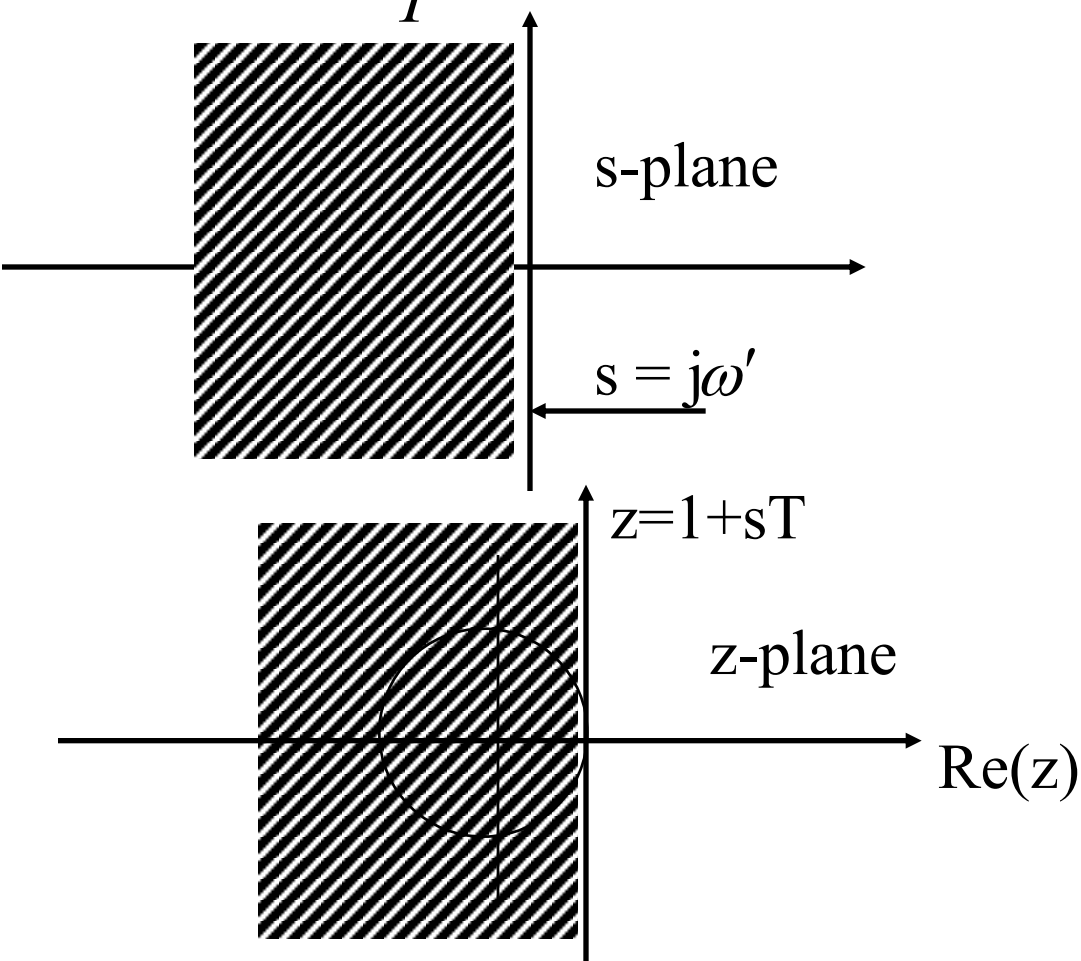


Conclusion: Mapping function does not in general satisfy the desired properties except for extremely small sampling times.

Forward difference operator:

$$s = \frac{z - 1}{T}$$

$$z = 1 + sT$$



Conclusion: Some pole locations in s-plane may be mapped to locations outside the unit circle. Generally this mapping is not recommended. Extremely small sampling times may provide satisfactory results