

**ECE ECE145A (undergrad) and ECE218A (graduate)**

**Mid-Term Exam. February 11, 2009**

Do not open exam until instructed to.

Open notes, open books, etc

You have 1 hr and 15 minutes.

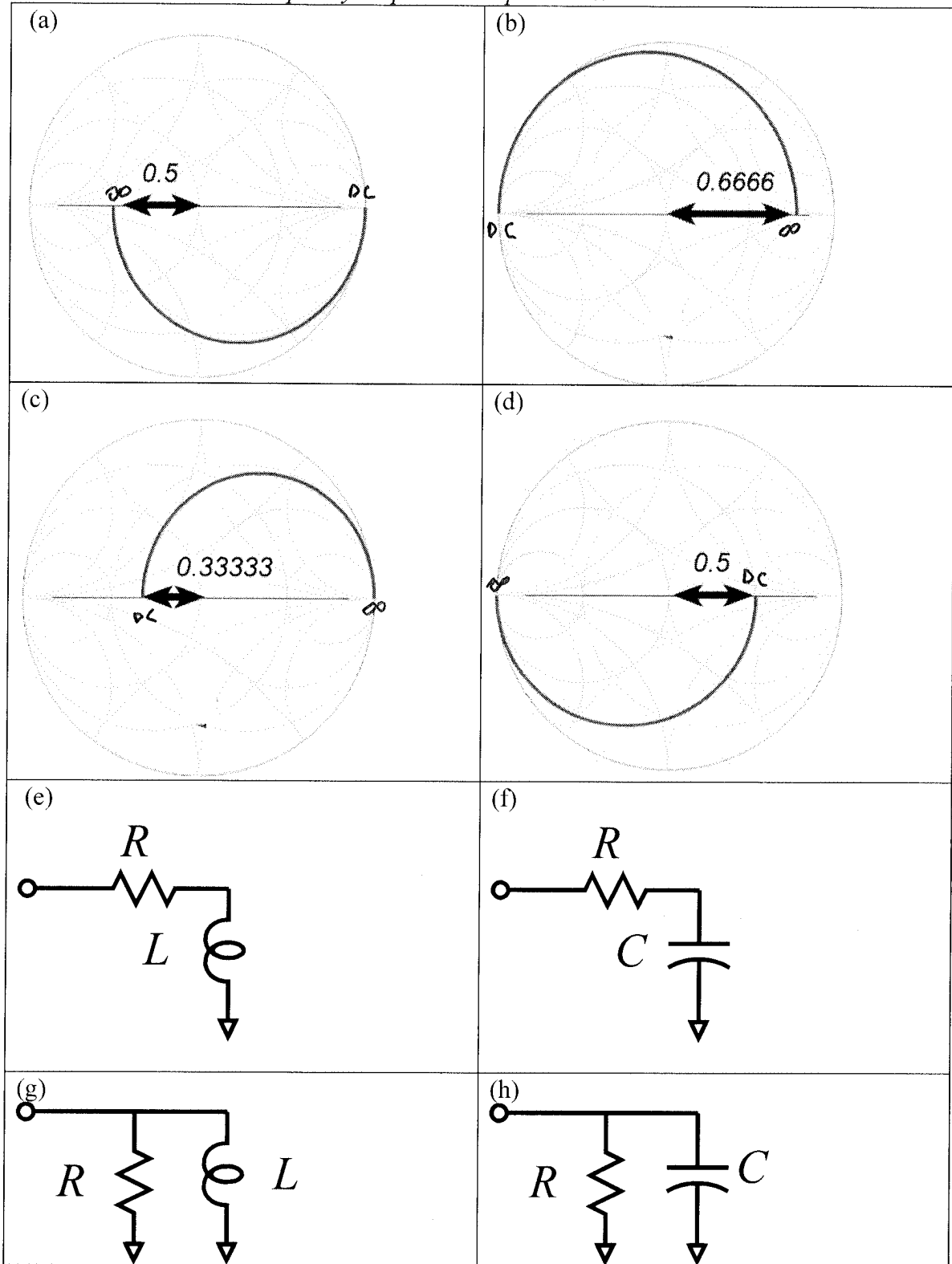
Use any and all reasonable approximations (5% accuracy is fine. ), ***AFTER STATING THEM.***

Problem	Points Received	Points Possible
1		20
2		25
3a		10
3b		10
3c		10
4a		5
4b		20
total		100

Name: Answer key

**Problem 1, 20 points**

*The Smith Chart and Frequency-Dependent Impedances.*



Match each Smith Chart with each circuit, and give all resistor values:

Circuit (e):	Smith chart=	<u>C</u>	R=	<u>25 Ω</u>
Circuit (f):	Smith chart=	<u>A</u>	R=	<u>16.67 Ω</u>
Circuit (g):	Smith chart=	<u>B</u>	R=	<u>250 Ω</u>
Circuit (h):	Smith chart=	<u>D</u>	R=	<u>150 Ω</u>

$$Z = Z_0 \cdot \frac{1 + \Gamma}{1 - \Gamma}$$

E/C

$$\Gamma = \frac{1}{3} \angle 180^\circ = -\frac{1}{3}$$

$$R = 50 \cdot \frac{1 - \frac{1}{3}}{1 + \frac{1}{3}} = 25$$

$$Z = R + j\omega L$$

F/A

$$\Gamma = -0.5$$

$$R = 50 \cdot \frac{1 - 0.5}{1 + 0.5} = 16.67$$

$$Z = R - j/\omega C$$

G/B

$$\Gamma = +\frac{2}{3}$$

$$R = 50 \cdot \frac{1 + \frac{2}{3}}{1 - \frac{2}{3}} = 250$$

$$Y = \frac{1}{R} - j\frac{1}{\omega L}$$

H/D

$$\Gamma = +0.5$$

$$R = 50 \cdot \frac{1 + \frac{1}{2}}{1 - \frac{1}{2}} = 150$$

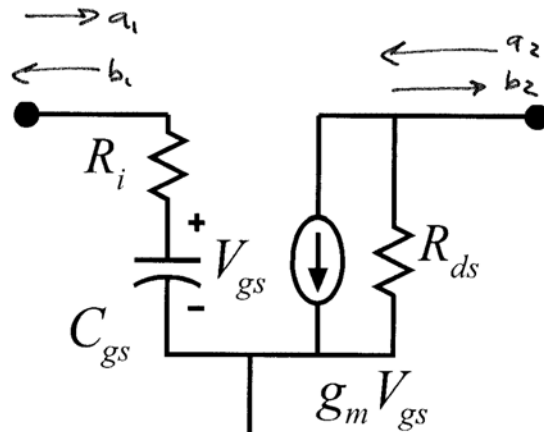
$$Y = \frac{1}{R} + j\omega C$$

**Problem 2, 25 points**

Transistor models and S-parameters.  
To the left is a simplified model of a MOSFET.

With element values as defined, first give algebraic expressions of the four S-parameters as a function of frequency.

Then using  $C_{gs}=31.8$  fF,  $R_i=200$  Ohms,  $g_m=20$  mS,  $R_{ds}=250$  Ohms, give numerical values at  $f=50$  GHz.

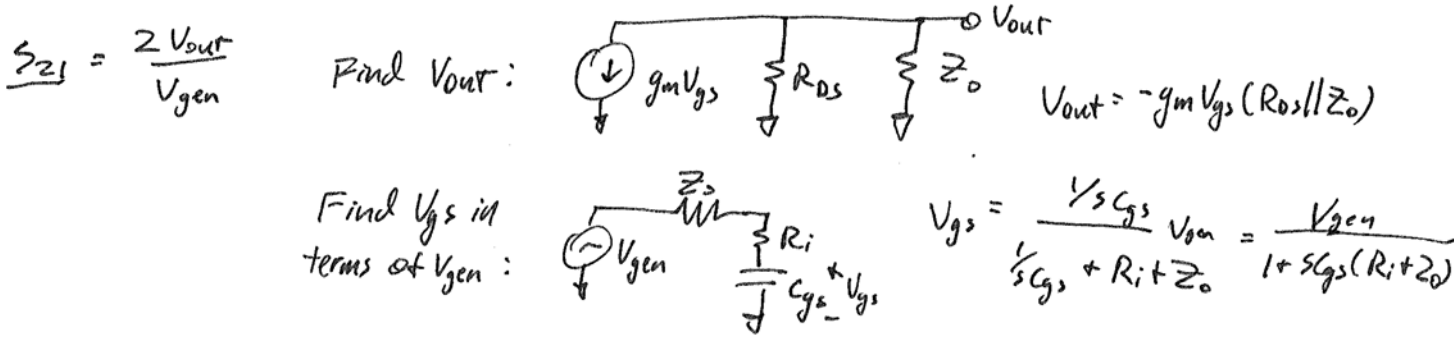


$$S_{11} = \frac{b_1}{a_1} = \Gamma_{in} = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} = \frac{R_i + \frac{1}{j\omega C_{gs}} - Z_0}{R_i + \frac{1}{j\omega C_{gs}} + Z_0} = \frac{j\omega C_{gs}(R_i - Z_0) + 1}{j\omega C_{gs}(R_i + Z_0) + 1} = \frac{j2\pi \cdot 50 \times 10^9 \cdot 31.8 \times 10^{-15} (150) + 1}{j2\pi \cdot 50 \times 10^9 \cdot 31.8 \times 10^{-15} (250) + 1}$$

$$S_{11} = 0.655 - j \cdot 0.130$$

$$S_{22} = \Gamma_{out} = \frac{R_{ds} - Z_0}{R_{ds} + Z_0} = \frac{200}{300} = \frac{2}{3}$$

$S_{12} = 0$  By inspection we see that no signal at Port 2 will couple to Port 1 since  $C_{gd} = 0$



Thus:  $V_{out} = -g_m \cdot \frac{V_{gen}}{1 + s C_{gs} (R_i + Z_0)} \cdot (R_{ds} \parallel Z_0)$

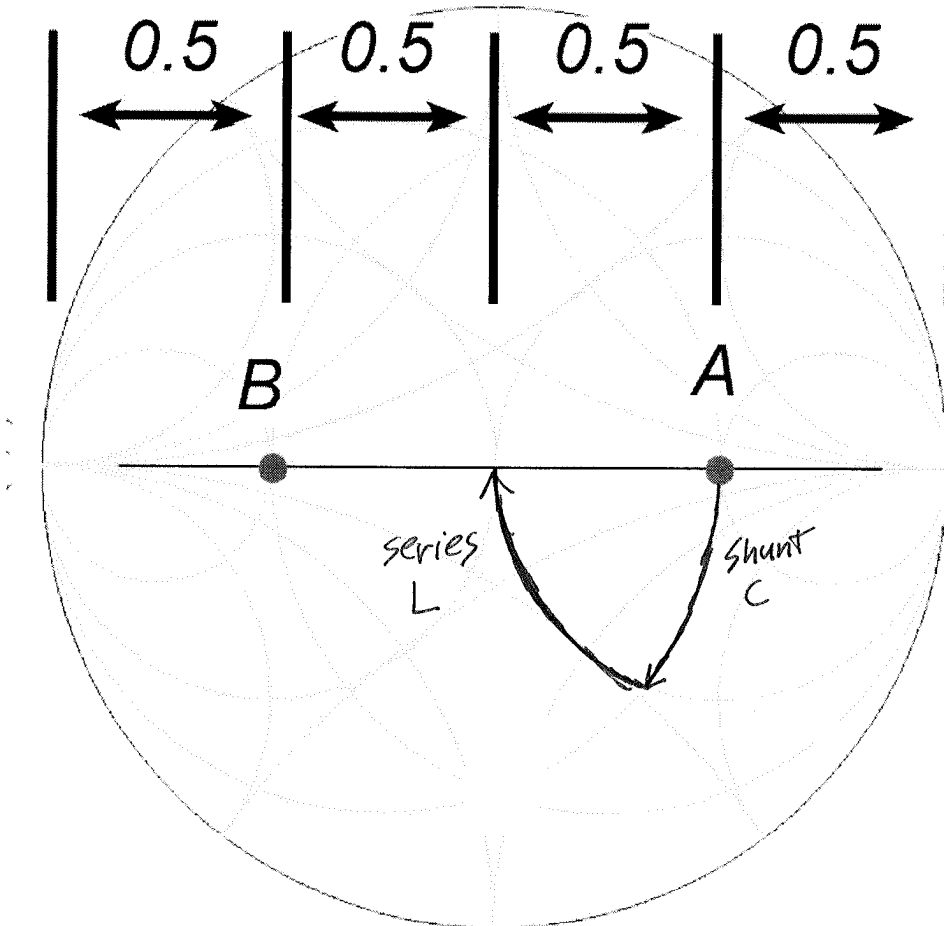
$$S_{21} = \frac{2 V_{out}}{V_{gen}} = \frac{-2 g_m (R_{ds} \parallel Z_0)}{1 + s C_{gs} (R_i + Z_0)} = \frac{-2 \times 0.02 \left(\frac{1}{250} + \frac{1}{50}\right)^{-1}}{1 + j 2\pi \cdot 50 \times 10^9 (250) \cdot 31.8 \times 10^{-15}}$$

$$S_{21} = -0.230 + j \cdot 0.575$$

**Problem 3, 30 points**

*Elementary impedance matching network design.*

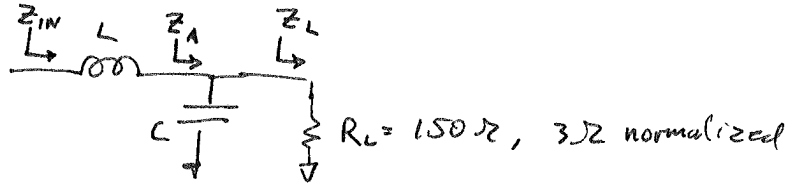
Use the impedance-admittance chart below. Assume a 50 Ohm impedance normalization. To keep the problem simple, if certain Admittance and Impedance coordinate lines *almost* cross, use the approximation that they *exactly* cross.



Part (a), 10 points.

Design a series-L, shunt-C impedance matching network to match impedance "A" to 50 Ohms at 20 GHz. Give the circuit diagram and the element values.

$$Z_L = 50 \cdot \frac{1+0.5}{1-0.5} = 150 \Omega$$



- Use shunt C to bring load to unit resistance circle, i.e. make  $\text{Re}(Z_A) = 1$  (normalized)

$$Z_A = (Y_A)^{-1} = \left( \frac{1}{R_L} + j\omega C \right)^{-1} = \frac{R_L}{1 + j\omega C R_L} = \frac{R_L (1 - j\omega C R_L)}{1 + (\omega C R_L)^2}$$

$$\text{Re}(Z_A) = \frac{R_L}{1 + (\omega C R_L)^2} = 1$$

$$\Rightarrow C (\text{norm.}) = \frac{\sqrt{R_L} - 1}{\omega R_L} = \frac{\sqrt{2} - 1}{2\pi \times 20 \times 10^9 \times 50} = 3.75 \times 10^{-12}$$

$$C = \frac{1}{50} \times 3.75 \times 10^{-12} = \boxed{75 \text{ fF} = C}$$

- Use series L to cancel remaining complex component of  $Z_A$

$$Z_{in} = 50 \Omega = j\omega L + Z_A = 50 + j \left( \omega L - \frac{\omega C R_L^2}{1 + (\omega C R_L)^2} \right)$$

set to 0

$$L = \frac{C R_L^2}{1 + (\omega C R_L)^2} = \frac{75 \text{ fF} \times (150 \Omega)^2}{1 + (2\pi \times 20 \times 10^9 \times 75 \text{ fF} \times 150 \Omega)^2}$$

$$\boxed{L = 563 \text{ pH}}$$

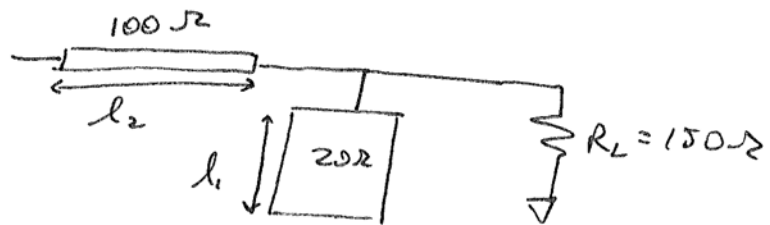
Part (b), 10 points

Ideal inductors are not available to you. Assuming high-impedance lines of 100 Ohm impedance and low-impedance lines of 20 Ohms impedance, give an approximate distributed-element design to this matching network. The lines' effective dielectric constant is 2.0

$$L = \tau Z_0$$

$$C = \tau / Z_0$$

$$V_p = c / \sqrt{\epsilon_r} = 2.12 \times 10^8 \text{ m/s}$$



- High-Z lines are almost like inductors
- Low-Z lines are almost like capacitors

$$\tau_1 = Z_0 C = 20 \Omega \times 75 \text{ fF} = 1.5 \text{ ps}$$

$$l_1 = \tau_1 V_p$$

$$l_1 = 318 \mu\text{m}$$

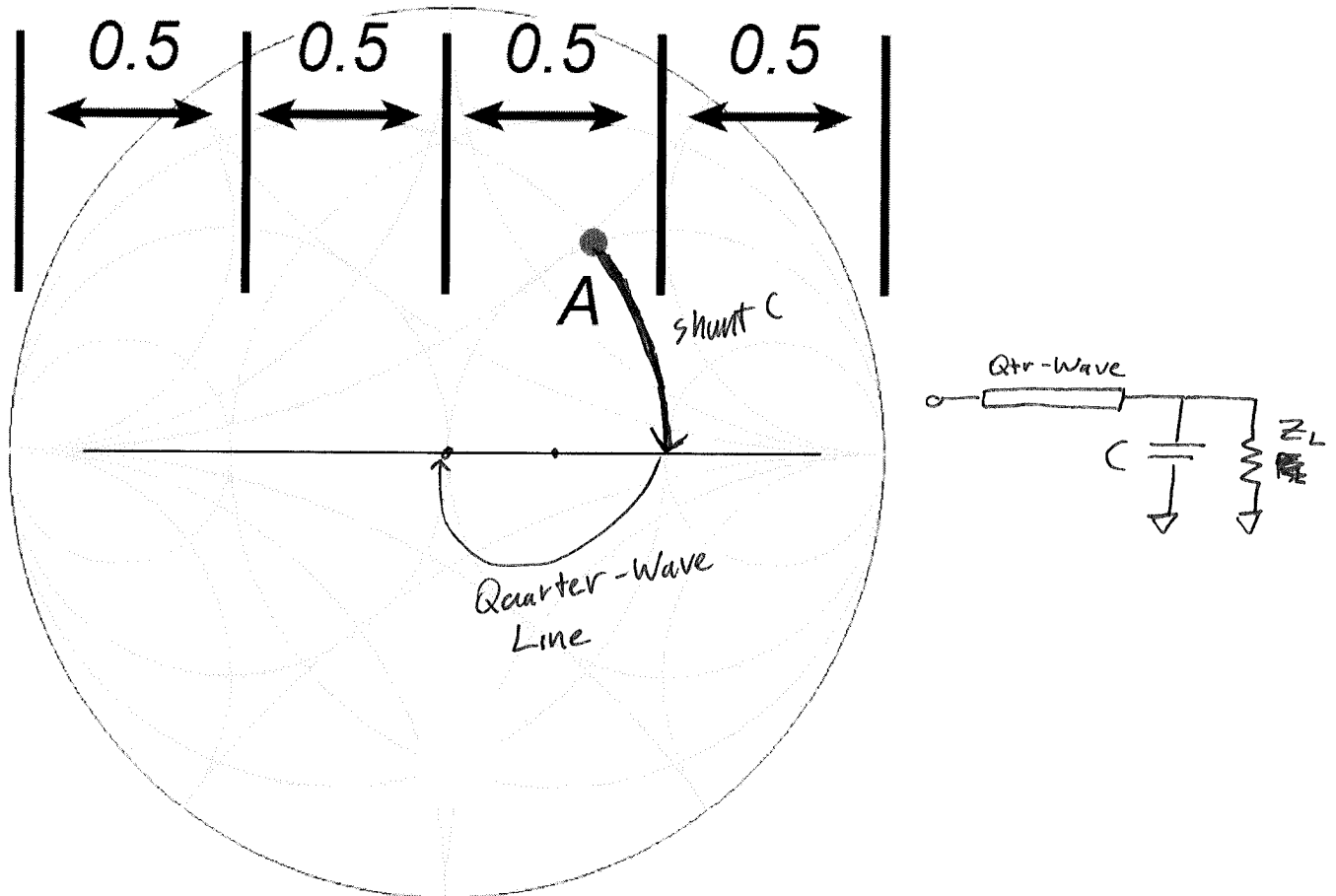
$$\tau_2 = L / Z_0 = 563 \text{ pH} / 100 \Omega = 5.63 \text{ ps}$$

$$l_2 = \tau_2 V_p$$

$$l_2 = 1190 \mu\text{m}$$

Part (c), 10 points

Load impedance "A" is to be matched to  $Z_0=50$  Ohms at 20 GHz (the chart below uses 50 OHms normalization) using a shunt capacitance and a series quarter-wave line. Find the value of the shunt capacitance and the required line impedance.



- From the symmetry with part (A) it is clear we will use the same capacitor  
 $C = 75 \text{ fF}$

- To match the resultant  $150 \Omega$  impedance to  $50 \Omega$  we use a quarter-wave line with impedance:  
 same as load resistor in part A:  $R = 50 \cdot \frac{1+0.5}{1-0.5}$   
 $R = 150 \Omega$

$$Z_0 = \sqrt{Z_L \times Z_{in}} = \sqrt{150 \times 50} = 86.6 \Omega$$

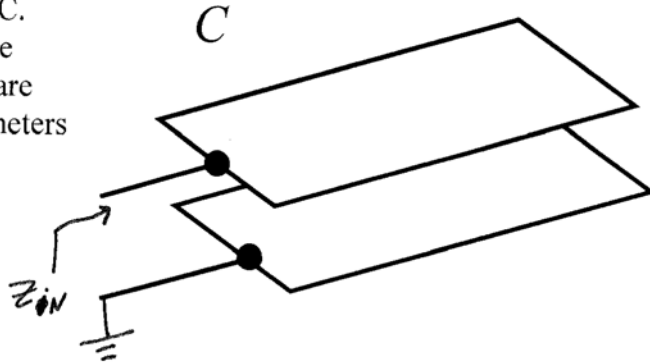
$$Z_0 = 86.6 \Omega$$



**Problem 4, 25 points**

*Lumped vs distributed elements*

We are designing a bypass "capacitor" for use in a 60 GHz wireless transceiver IC. The plate separation is 100 nm, and the dielectric constant is 4.0. The plates are 500 micrometers long and 100 micrometers wide.



Part (a), 5 points

What is the low-frequency capacitance C?


$$C = \frac{\epsilon A}{d} = \frac{4 \times 8.854 \times 10^{-12} \text{ F/m} \times 500 \mu\text{m} \times 100 \mu\text{m}}{100 \text{ nm}} = \boxed{17.7 \text{ pF}}$$

Part (b) 20 points

Using transmission-line relationships, what is the element's impedance at 37.5 GHz and at 75 GHz?

$$v_p = c/\sqrt{\epsilon_r} = 1.5 \times 10^8 \text{ m/s}$$

37.5 GHz:  $\lambda_{37.5 \text{ GHz}} = v_p/f = \frac{1.5 \times 10^8 \text{ m/s}}{37.5 \times 10^9 \text{ Hz}} = 4 \text{ mm}$

$\Rightarrow 37.5 \text{ GHz } L = \lambda/8 \text{ so } Z_{in} = -jZ_0$  \* 

Since this is a low-Z line,  $Z_0 = \sqrt{\epsilon/\mu}$   
 $\epsilon = l/v_p = 500 \mu\text{m} / 1.5 \times 10^8 \text{ m/s} = 3.33 \text{ pF}$   
 so  $Z_0 = 0.188 \Omega$ ,  $Z_{in} = -j \times 0.188$  } or  $Z_0 = \frac{\pi}{\sqrt{\epsilon_r}} \cdot \frac{H}{W}$   
 $Z_0 = 0.188$

75 GHz: Now  $L = \lambda/4$ , so the open circuit ends appear to be short circuit

$$Z_{in} = 0$$

\*  $Z_{in} = -jZ_0$  because  $\Gamma_{in} = \Gamma_L e^{-2j\beta l} = 1 \cdot e^{-2j \frac{2\pi}{\lambda} \frac{\lambda}{8}} = e^{-j\pi/2} = -j$   
 $Z_{in} = Z_0 \cdot \frac{1 + \Gamma_{in}}{1 - \Gamma_{in}} = Z_0 \cdot \frac{1 - j}{1 + j} = -jZ_0$